ANALYSIS OF SPACECRAFT ON-ORBIT ANOMALIES AND LIFETIMES

PRC R-3579 10 FEBRUARY 1983



Prepared for
National Aeronautics and Space Administration
Goddard Space Flight Center

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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

GODDARD SPACE FLIGHT CENTER

under

Contract No. NAS 5-27279

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FOREWORD

This report presents the results of a study of spacecraft on-orbit anomalies and lifetimes. The basic source of information is an update of a data bank of on-orbit spacecraft reliability data compiled by Planning Research Corporation (PRC) for the National Aeronautics and Space Administration and the Navy Space Systems Activity in a series of short term contracts starting in 1966. The update covers spacecraft operating since 1977 under the cognizance of the Goddard Space Flight Center and the Jet Propulsion Laboratory.

Emphasis in this study is on individual spacecraft and their postlaunch performance degradation over time as a function of component failures and other incidents of anomalous behavior. By contrast, earlier studies in this series concentrated on compiling reliability statistics for hardware elements across spacecraft.

The NASA Technical Monitor for this study was Mr. Edward Shockey of the Goddard Space Flight Center, Code 302. The work was performed during the period June 1982 through January 1983, under NASA Contract NAS 5-27279.

The authors of this report are Charles E. Boomquist and Winifred C. Graham. Other members of the PRC study team were Patricia Alverson and Vera Little. Library assistance was provided by Wendy Christensen and report production support by Brenda Healy.

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ABSTRACT

Analyses of the on-orbit performance of forty-four unmanned NASA spacecraft operating in the past five years (1977-1982) are presented. Included are detailed descriptions and classifications of over 600 anomalies - each anomalous incident represents one reported deviation from expected spacecraft performance. Charts depicting satellite lifetimes and the performance of their major subsystems are included. Engineering analyses to further investigate the kinds and frequencies of various classes of anomalies have been conducted. An improved method for charting spacecraft capabilty as a function of time on orbit is explored.

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I. INTRODUCTION

This study has examined the orbital performance records of forty-four unmanned spacecraft under the cognizance of the Goddard Space Flight Center and the Jet Propulsion Laboratory. Particular attention has been given to each recorded incident of anomalous behavior. These incidents, referred to harein as anomalies, range from momentary "glitches" in otherwise normal spacecraft operation to complete spacecraft failure. The basic data have been collected, reduced, analyzed and reported in formats consistent with those in the existing data bank, developed by Planning Research Corporation (PRC). These earlier data were collected on 350 spacecraft under several discrete contracts awarded to PRC between 1966 and 1979.

A. Study Objectives and Scope

One of NASA's primary concerns is to improve the performance of its spacecraft, both manned and unmanned. For unmanned spacecraft, longevity is a key parameter. Generic approaches to improving longevity are of continuing interest to NASA; the search for such approaches is the motivation for this study. There are two study objectives. The first is to establish a current data base of on-orbit spacecraft anomalies and performance summaries following previous PRC work in this area but extending it somewhat to support the second study objective. The second objective is to develop a method for quantifying spacecraft performance as a function of time on orbit which extends and improves upon an existing methodology, previously developed by PRC and applied to other spacecraft in the data bank.

Augmentation of the data base is limited to spacecraft launched under the auspices of the Goddard Space Flight Center (GSFC) or the Jet Propulsion Laboratory (JPL) and which have been operational since the last general update of the space data bank in 1977-1978.

B. Background

The first 15 references at the end of this report trace the complilation and utilization of the PRC data bank. Reference 1 was the result of an initial study undertaken in 1966 to respond to the need for more accurate and detailed spacecraft reliability data than were available in the mid-sixties. On-orbit data from 225 spacecraft were compiled and analyzed. The resultant report was well received and widely distributed. Subsequently, several specific analyses of these data were conducted and reported on (see References 2-6). Reference 7 was an extensive update of Reference 1; the size of the data base essentially doubled. Reference 9 added still more data resulting from a modest collection effort in 1972. References 8 and 10 through 14 reported on various special-purpose analyses of the data bank. Reference 15 reported on another comprehensive update and consolidation of the data bank conducted in 1978. At the conclusion of that study, the PRC data bank included on-orbit performance data on some 350 different spacecraft. All basic spacecraft data collected from the beginning of these efforts were included in the Reference 15 study report. Reference 16 analyzed and interpreted orbital reliability data for U.S. meteorological satellites in the data bank.

C. Organization of the Report

Section II briefly describes the data base and the updating of it for purposes of this study. It includes a description of collection and reduction procedures and baseline data on all spacecraft included in the update. Section III classifies the anomaly data. First, the categories established in the earlier efforts are utilized. They are reported separately for purposes of consistency. Then, added classifications developed specifically for this study are applied and reported. Section IV presents performance summaries by spacecraft and by major subsystems. It also provides engineering analyses of the anomaly data regarding trends, persistent problem areas, test-related anomalies and other areas of interest. Section V treats the question of measuring on-orbit spacecraft capability over time. It includes consideration of the effect of anomalies on (1) the basic spacecraft, (2) its scientific or applications payload, and (3) its overall mission objectives. A methodology for possible future application is suggested. Three appendices provide (1) an indication of the adequacy of the data base coverage for this update, (2) basic anomaly data tabulations including anomaly codes for purposes of classification, and (3) detailed spacecraft and subsystem performance summaries in graphical form.

II. DATA BASE

This report documents a continuing examination of spacecraft on-orbit reliability that PRC began in 1966. Four earlier studies collected and analyzed data on 350 spacecraft from 52 space programs. Results from these four studies are integrated and reported in Reference 15.

This present study is a contractually limited update to Reference

15. It covers only GSFC and JPL spacecraft which were operational between

1977 and 1982. Several of the analyses integral to the earlier studies are

missing here, notably those relating to failure rates and probabilities of

failure during launch. Furthermore, no systematic effort has been devoted

to reporting the totality of the earlier data here or to relating the

earlier study results to those found in this update. Selected comparisons

have been made, but if the reader is interested in the entire collection of

data and information contained in the PRC space data bank it is necessary to

have both Reference 15 and this report.

A. General

In addition to the published reports, an unpublished file of engineering analysis reports (EARs) are maintained for each spacecraft in the data base.

The ERAs are maintained at NASA and at PRC. (1)

The EARs are the basic data collection. They contain:

- General descriptive and operational data on each spacecraft.
- A detailed breakdown of the spacecraft assemblies, components,
 and piece parts.

The NASA contact is Edward Shockey, GSFC Code 302, Telephone (301) 344-5628. The PRC contact is Charles Bloomquist, PRC Systems Services, 10960 Wilshire Boulevard, Suite 2320, Los Angeles, California 90024. Telephone (213) 477-8278.

- Operating (and dormant) time accumulated by each hardware element.
- Descriptions of all anomalies and failures recorded against the spacecraft, together with information on the known or probable causes of many anomalies.
- Background information regarding manufacture, test, and launch.

The information contained in each EAR, as summarized above, is organized into three categories, namely, (1) general information, (2) reliability data, and (3) development and prelaunch information. General information includes launch data, launch vehicle, launch site, intended mission, orbital parameters, spacecraft description, and a general performance assessment over the time period covered by the data bank.

The reliability data elements, to the extent possible, break the spacecraft down into its major components (receivers, tape recorders, digital decoders, etc.), accumulate the survival hours in space for each (including length of time on standby and number of times cycled), give in a further breakdown the piece parts in each component, and finally, provide a rather detailed description of each anomaly recorded during the mission.

Development and prelaunch information includes, as available, the prelaunch test and checkout routines and experience, and brief descriptions of developmental testing, part selection procedures, and quality assurance provisions.

The subject study is an exception in that it correlates specific anomalies with particular spacecraft; previously published reports an papers do not. This correlation is always possible, however, by returning to the EARs.

The same data collection and reduction procedures and reporting formats are used in each study, including the current one. This uniformity allows ready combination of the data herein with any or all of the previous data sets.

B. Update For This Study

Exhibit 1 depicts the five on-orbit reliability studies, including the current one, in terms of the programs and numbers of spacecraft considered. This update includes 44 spacecraft from 19 programs. Nineteen of these spacecraft were covered in the previous study and continued to operate into this study period. As mentioned previously, access to the total data base (62 programs, 375 spacecraft) requires both this document and Reference 15 since previous data are not, for the most part, repeated here.

As in the previous studies, the basic data sources were the Product Assurance Divisions at the NASA Centers (GSFC and JPL in this study), cognizant spacecraft program offices, and open literature. Of particular help in this update were the Mission Operations Managers for the various Goddard programs.

The two major types of data sought for this study, as in earlier studies, are: (1) an engineering report of the final design of the space-craft, and (2) a flight analysis for individual spacecraft from which operating histories and all known anomalous behaviors can be obtained. From this information Engineering Analysis Reports (EARs) are generated for each spacecraft. The EAR is tailored to provide the information content required to meet the study objectives and provides a uniform base for each spacecraft of the study.

The EARs contain a complete list of references used, by spacecraft. The number of citations for this update is in excess of 250.

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	Original Study, 1707 (mission of		30 = 41:X	Program	Kumber of	Program	Number of
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AFFIX	,	200	-	CEOS	-	ATS (1)	•
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		Designation	Spacecraft				
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(1) includes update(3) of spacecraft analyzed in previous data bank studies. (2) Wiking Program includes 2 Orbiters and 2 Landers.

In the EARs the treatment of standby and redundant units is consistent for all data samples and emphasizes the utilization of only known values. Operational hours in the EARs were recorded as "powered" and "unpowered" where such information was known. For much of the equipment, however, the information available only indicates that at a given time the equipment was known to be operational. For this reason the nominal unit of measure in this report is survival time.

The authors believe that the crux of studies of this nature is the provision of a large amount of data in a readily usable form. For this reason, as well as the fact that the information from the documentation does not warrant application of highly sophisticated techniques, the methods of analysis are simple and straightforward.

Classification and summarization, using simple, readable tables, are the primary presentation techniques. In general, statistical inferences are not drawn from these efforts. Conclusions have been drawn where appropriate, but the emphasis is placed on presenting data in such a form that readers may easily draw their own conclusions in areas of their special interest.

Documentation for the spacecraft in this study was generally of sufficient detail and of high quality. Appendix A indicates the quality of data bank coverage for each spacecraft in the update as a function of the four major tables in the Engineering Analysis Reports.

C. Baseline Data

Exhibit 2 provides a complete list of spacecraft in the update, together with several key data elements. The first four items, space-

EMIBIT 2 - SPACECRAFT BASELINE DATA

SPACETORARY DESIGNATION	STATUS.	OPERATING LIFE (Months)	LIFE, ING LIFE ache)	STNOPSIS OF MERITACE/MATURITY	SYNOPSIS OF COPPLEXITY PACTORS	COPPLEXITY
ATOS PRESE ECPLORER, AL-3	11/20/75 Reentered 6/10/81	21	5	identical to AE-D except for pay- load. First spacecraft to use a central computer and data base.	Twelve straightforward ecientific instruments. Three axis stabilization with wheels and megactic torquers. Hydraxine orbit adjust; straightforward telemetry; commend and power subsystem. Has a solar pointing platform.	*
APPLICATIONS ESPLONER HISSIGN, ABP-A (MEAT CAPACITY NAPTING HISSIGN), (MCOC)	4/27/78 Descrivated 9/30/80	77		First in a series of low cost modular speceraft. Bull: by Besing. Based on a speceraft bullt for URAF. Magnetic acquisition and in-orbit control had mayer been actempted before. Bedinmeter was a modified HIMMUM-5 unit.	Spin stabilised; used augmentic control loop for both acquisition and in-orbit centrol; had wheels and hydraxime orbit adjust system. He tape recorder. Straightforward telematry, commend, and power subsystems. Had three deployables and one poyload instrument.	a
AMB-B (STRATOSPHERIC) 2/18/79 AEROPOL AMB CAS Patiod EXPERIMENT, SACE) 1/7/82	2/18/79 Palled 1/7/82	2	ž	Same besic speceraft so MCGM but had two tape recorders instead of arbit adjust system: Radiometer wes similar to SAM II on NIMBUR-7.	Same as NCOM sampt for tape recorders and orbit adjust system difference.	2
APLICATIONS TECHNOLOGY SATBLITS ATS-1	12/7/66 Partially Operational 12/82	*	6	Less outgrowth from the Syncon progres, but due to the tech- melegical evaluation nature of the ATS progres, speceraft hard- were primarily involved now developments.	Extensive communications subsystems, electronically desput antenna utilising considerable elecutry; extralphiforward telematry, commune, possi; sophisticated applications poyload; opis stabilised; straightforward propulator; bad appear engine.	
A78-3	11/5/67 Partially Operational 8/1/82	*	79	1== as ATF-1	Datic operated came as ATD-1 except ATD-3 has machanically instead of electrosically degram entones; increasing complexity very elightly; has ancombat informat paylead from ATD-1 but equally cophisticated.	~
\$ - #\$	8/12/69 Partially Operational 12/80	*	191	See as ATP-1	Same comments as ATP-1 and-3 except ATP-5 was gravity gredient stabilized and therefore did not need a gaspun antenna or spin centrel propulsion; did require deployable gravity gradient booms.	2
74	5/30/74 Dectivated 8/3/79	*	3	New programmany "firsts", s.g., 30-feet reflector, stringest ACS requirements, heat pipes, stc. Little "heritage."	Bringent three-axis central requirements; deployable reflectors and solar arrays; complen- extensive communications systems; on-beard computer with plated wire mensy. One of the most complex unmanned specestaft ever flows.	2
Private Estada	6/3/81 Operational 7/31/82	.	21	Outgrawth of the AE's. MASA- standard tape recordsts and transponder. Amaleg/digital multiplexing based on TIMG-H design. Bus sensor adms as	Spin stabilised; two booms; tape Tecofdors, augments terrests. No wheels, no prepalsion. Straightforward telemetry, commend, power and commitations. No mitroprocessor, two tape recorders. Nos six straightforward estentific lastrumants; 200 meter tip-to-tip ervenses.	2
ĩ	8/3/81 Operational 7/31/82	2	2	Outgrowth of the AE's. MASA- standard tape recorders and transponders. Sum esteor similar to IUE's. Amalog/ digital multiplaning based on TING-H design.	Three-axis stabilized; uses wheels and torquere. Command system rather complex because many functions implemented. Straightforward power system and communications. He sufcreprocessor; two tape recorders, scan platform and augmenter boom. He propulsion. Fairly straightforward extending interments (mine). Hen two	a

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SPACECHAPT DESTONATION	LAUNCH DATE, STATUS, STATUS DATE	OPERATION LIFE OPERATION LIFE (Marchs)	M. 1.1FF. Mr. 1.1FF. (ths)	SYMMESTS OF TEMPETAM/ 4-DK LEWITH	SYNOPSIS OF COMPLEXITY PACTORS	COMPLEXITY RATING
: <u>इ</u>	SC and by 95 (10) 16/75	£	*	The SMS/COBS hardware utilized technology and designs developed on the ATS 1 through 5 program.	Straightforward basic subsystems; spiratabilized; semewhat complex radiometer. Has apogee boost motor and hydratice system.	**
	6/16/77 Partially Operational 4/30/82	£	\$	Same as COES-1	Same as GOES-1	*
	6/16/78 St.andby 3/81	×	E	Third spacecraft in the Ford Acrospace-CDES series.	Hay Apogee Boost Motor, hydraxine system, electronically despun antenna. Straightforward command, telemetry, cummunications and power. Fairly complex radiometer. Spin stabilised; hydraxine system. No tape recorders.	5 *
	9/9/80 Operational 7/31/82	*	2	First spacecraft in Nughes Aircraft-GOES series; outgrowth of ATS and other MAC spacecraft. Same space-craft bus as HAC GAS. Carried new type of radiometer; new S-band equipment; extensive use of microwave integrated circuits and aurface acoustic wave (SAW) devices. New telementy and command design. Used advanced K-7 solar cells.	Spin stabilized; has hydrazine system, apogee boost motor. No tape recorders. Nas mechanically despun platform. Array divided into five sections. Complex rediometer. Uses microprocessors for telemetry control. Fairly complex S-band equipment.	8
	5/22/81 Operational 7/31/82	ž	=	Second in MAC-GOES series; same spacecraft as GOES-4.	Same as G0ES-4	2
INTERPLANETARY MONITORING PLATFORM (INP-8)	5 10/26/73 Operational 7/31/82	*	105	Based on earlier IMP's/Explorers.	Straightforward Explorer-type spacecraft; spin stabilized; has cold gas system; two deployables; straightforward scientific payload.	=
INTERNATIONAL SUN- EARTH EXPLORER ISEE-1	10/22/77 Operational 7/31/82	2	\$	Same cold-gas system as 198's. Same hardware was IUE spares; based on IUE designs.	Mas cold-gas system; simple attitude control. Straightforward power system, data handling and communications. Uses microprocessor for command control. Mas thirteen rather atraightforward scientific instruments; eight deployables.	4
	10/22/7; Operat ional 7/31/82	*	57	New design, built by the European Space Agency.	Mas cold-gas system; simple spin stabilised attitude control. Straightforward power, data handling and communications. Eight experiments; seven deployables.	12
	8/12/78 Operational 7/31/82	2	8	Same as ISEE-1	Same as ISEE-1 except has hydratine system (orbit adjust) instead of cold-gas.	±
EXPLORER	1/26/78 Operational 7/31/62	3	*	Cyro-sheving approach to attitude control represents a new development. Panoramic Attitude sensor originally developed for RAE-B. Analog sun sensors sidentical to those on OAO and ATS. Digital sun straor similar to that on OAO-C. Spin mode aun sensor similar to the one on MAMEYE. Reaction wheels identical to yaw wheel on NIMBUS-D. Wheel drive designed especially for IUE. Data Multiplexer based on GSPC standard design. On-board computer has been used on neweral GSPC missions. Prover subsystem supplied by the European Space Agency.	Some observations require that 3-axis stabilization be maintained for up to fourteen hours. Has complex attitude control system to achieve this (Ayros, digital and analog sun sensors, spin mode sun sensor, PAS). Has hydratine system, wheels. Straightforward communications and compand subsystems. Complex data handling - has computer, extensive multi- plexing, has Apogee hoost motor, heat pipes and two deployables. Complex telescope control/ electronics. No tape recorders.	÷.

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	LAUNCH DATE, STATUS,	DESIGN LIFE, OPERATING LIFE (Months)	, E	SYNOPSIS OF MEDITAGE/MATURITY	STMOPSIS OF COMPLEXITY PACTORS	RELATIVE COPPLEXITY PATING
LAIDSAT-2		12	8	Similar to LANDSAT-1, and based on technology from the NIMBUS program.	Complex cormand/clock subsystem with memory; complex power and power distribution system; complex ACS with wheels, gives, Freen and hydraxine system; also megnetic torquer; fairly complex telemetry and communications; complex payload.	\$
LANDSAT-3	3/5/78 Operational 7/33/82	*	23	Outgrowth of LANDSAT-1 and -2; uses improved return beam vidicon and multispectral scanner.	Essentially the same as LAMDEAT 2.	s
4-TASSAT-4	7/16/82 Operational 7/31/82	*	-	Outgrowth of previous LAMDSAT's; new Thematic mapper. Intended for shuttle retrieval/refurbishment.	Thematic mapper much more complex than previous MSS's; has no tape recorders, will utilise TDESS; basic spacecraft is MASA/Pairchild multi-mission bus; has Ku, X- and S-band communications; required pointing accuracy is 0.010.	Ş
HACS A T	10/30/79 Been to red 6/11/80	•	^	Some MACSAT hardware originally built for SAS-3. At the time, MACSAT was the most complex space-craft ever built at APL. Uses recorder/transponders interface new on MACSAT. Payload magnetometers an outgrowth of the designs used on the OGO's, also, vector magnetometer an outgrowth of Voyager magnetic fields experiments.	Uses wheels and magnetic torquers; has gyros, microprocessor, extendable trim boom; straight-forward power subsystem; has stray dilly; fairly complex telecommodications system with microprocessors, tape recorders. Pairly complex structure; fairly straightforward payload.	:
4-27 8 03	4/8/70 Descrivated 4/80	2	2 2	Image Dissector Cemera seme as on MINBUS-1, otherwise payload up- dated versions of MINBUS-3 pay- loads. Mad new Versatils Infor- mation Processing System; had upgraded ACS.	Three-axis stabilized to one degree. Two-hundred watts of power supplied by two SMAP-19 generators. Two tape recorders. Extensive command and telementy subsystems. Several deployables. Four new experiments the series.	\$
8-20 0 (1)	12/11/72 Partially Operational 7/31/82	u	116	Med first deployable and retroctable scanning sicrowave rediometer; had five new pay- load instruments; designs based or earlier HIMMUS' basic space- craft.	Uses wheels, magnetic torquers, and pneumatics has gives, extensive clock/timing subsystem; has solar arrey drive; extensive power and information handling subsystems; complex and extensive psyload (seven instruments).	2
4-83 6 011	6/12/75 Partially Operational 7/31/82	12	*	Outgrowth of earlier NINBUS space- craft but incorporated improve- ments in many basic spacecraft subsystems.	Essentially the same as WIMMS-5 but had mine payload instruments.	*
и 17 805- 7	10/24/78 Operational 7/31/82	17	\$	MCS essentially the same as on MINBUS-6; some changes in the command/clock subsystem from MINBUS-6; almost all new Filght Data Manding Equipment; same power system design as MINBUS-6 but different vendors; of the eight payloads, alx were new to NIMBUS-7.	Uses wheels, torquers and Preon pauseatics; has solar array drive, gyros; complex commend/ clock subsystem; stratghtforward but extensive filtht dats and VIP's subsystems; straight- forward power subsystem; complex and extensive payload (eight instruments).	*

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MOLITARIO PRACTICAN	LAUNCH DATE, STATUS, STATUS DATE	DESIGN LIFE, OPERATING LIFE (Numths)	.1FE.	SYNOPSIS OF HERITACE/NATURITY	STWOPSIS OF COMPLEXITY PACTORS	COPLEXITY
HDAA-4	11/15/74 Deactivated 11/78	*		Long heritage in ESSA/TIROS/TUSS series of spacecraft.	Uses wheels and magnetic torquing; has deployable arrays; straightforward power and communications subsystems; straightforward but extensive command/timing subsystem; fairly complex psyloads (four).	*
8-79°	1/29/76 Descrivated 6/80	77	;	See HOAA 4	Same spececraft on MOMA 4.	*
9-FECH	6/27/79 Operational 7/31/82	5	25	Pirst operational apacecraft of the TIMOS-N series; essentially same apacecraft as TIMOS-N except for a few design changes due to problems identified on TIMOS-N	Uses wheels and magnetic torquing; has gyros, solar array drive, hydratis, and mitrogen system; fairly complex power system; has apogee boost motor; straightforward but extensive comment, data handling and communications. Nuderately complex payload.	3
e-wega	5/29/80 Umauccessful le	4	1			•
1 - 4 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	6/23/81 Operational 7/31/82	**	2	Second operational spacecraft of the TIMOS-M series.	Same as MOAA-6.	3
SOLAE INATINEN HUSSION	2/14/80 Failed 1/15/81	*	=	Pirst of the modular specerraft built for shuttle retrieval and first use of multi-mission space-craft bus approach. One of the unmanned spacecraft. Ned first madular power supply ever flow. Nest experiments had predecessors on the OSO's.	Unes wheels, magnetic torquers, and a wide variety of sum seasors; has gyros, deployable array; fairly straightforward power system; has atterable antenna, on-board computer, tape recorders; straightforward command, communications, telemetry and acleutific payload.	z.
STREET NET BELLECICAL	3					;
1-986-1 286-1	5/17/74 Deect twated 1/29/81	*	8	First of the SME/COES series; see COES-1.	Some as 0065-1.	₹ ;
~ 8	2/6/75 Standby 2/25/82	2	*	Same as 0005-1.	Same as 00ES-1.	ર :
11908-8	10/13/78 Failed 2/27/81	*	2	"Protefilght" spacecraft for the third generation of WOAA's; See MOAA 4-7.	Same as MOAA-6.	
\$\$A\$AT	6/26/78 Failed 10/9/78	21	•	Used standard Agens bus equipment for basic spacecraft functions. Payload a moutdwestowner except acaming multichemeal alcromave Radiometer may as on NINBUS-7.	Uses wheels, has hydrasise orbit adjust, retaiing solar array. Overall, very straightforward besit spacecraft subsystems. Fairly complex perioed with a double-deployment antenna array.	
SOLA MESSENIES EPLONER	10/6/81 Operational 12/20/82	*	2	A low budget explorer; all hard- were well within the state of the art.	Spin stabilized, uses ampatic torquers; has no propulation or pyrotechnics equipment. Very simple speceraft; only unique feature is disk mounted array on booster-end of speceraft. Straightforward scientific payload.	2

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		ដ	EXMIBIT 2 - SPACECRAFT BASELINE DATA (Continued)	(fined)	RELATIVE
	LAUNCH DATE. STATUS.	DESIGN LIFE, OFERATING LIFE (Months)	STMOPSIS OF HERITACE/MATURITY	STHOPSIS OF COMPLEXITY FACTORS	COPPLEXITY
VIKING ORBITER I	\$/20/75 Deactivated 7/80	15 58	Outgrowth of earlier JPL Mariner spacecraft; new developments required to accommodate LANDER	Mad very extensive communications, telemetry and command equipment; general purpose computer, tape recorders, memories; extensive pyrotechnics and deployments; complex propulaton; fairly straightforward power tubsystem.	&
VIKING LANDER 1	8/20/75 Operational 12/2/82	15 87	Mew development overall; also all individual hardware represented new developments to accomplish Mars landing, sampling and environmental	Mad highly sophisticated payloads; de-orbit and Mars landing equipment; used radioisotope thermoelectric generators; fairly straight- forward communications and data handling.	:
VIKIMC	9/9/75 Peace lyane	15 44	sensing. See VIKING ORBITER 1.	SAME AS VIKING ORBITER 1.	\$6
VIKING	9/9/78	25	See VIKING LANDER 1.	SAME AS VIKING LANDER 1.	19
UMBER 2 VOTACER 1	9/5/17 9/5/17 Operational 12/82		Outgrowth of previous JPL space- craft but required many new developments to support interplanetary mission.	Mas three on-board computers; sophisticated scan platform and atticulation costrol; uses radio- isotope generators for power; extensive communications equipment for 5- and X-band. Mas hydratine system, gyros, extensive command and control system; has separate propulation	861
WOT AGER 2	8/20/77 Operational 12/82	64 49	Same as VOTACER 1.	module (solid rocket motor) for Jupiter trajectory injection. SAME AS VOTAGER 1.	90

craft designation, launch date, spacecraft status and status date, are self-explanatory. The next column gives the design life (1) and the operating life, calculated as the difference between launch and status dates. If the spacecraft is still operational this figure is, of course, only tentative.

The next two columns attempt to place the individual spacecraft in the context of the larger U.S. space program by giving brief synopses of its heritage/maturity and factors determining its relative complexity. Attempts to tabulate such quantitative factors as pointing accuracy, voltage regulation, data rates, etc., were unsuccessful in that for many spacecraft the requisite data points were unavailable and the others required so many qualifications or explanations that the quantitative nature of the entry was effectively obscured. Thus, our reliance on more qualitative factors.

The final column is our attempt, nevertheless, to quantify relative complexity. The numbers were read from Exhibit 3 which, in turn, represents our best engineering judgment of relative spacecraft complexity. Exhibit 3 is the end result of an iterative, assessment process designed to place all 43 spacecraft in the update (which successfully attained orbit) in relation to each other in terms of complexity. The most complex was then assigned a complexity rating of 100 and the least complex a rating of 10, there being in our judgment about an order of magnitude difference in complexity between the SME and the Voyagers.

⁽¹⁾ Spacecraft design life is a rather nebulous parameter. It sometimes is not specified at all in the documentation available to us; in other cases multiple design lives are referenced. We have, therefore, selected one design life for each spacecraft that seems most reasonable to us on the basis of all available information.

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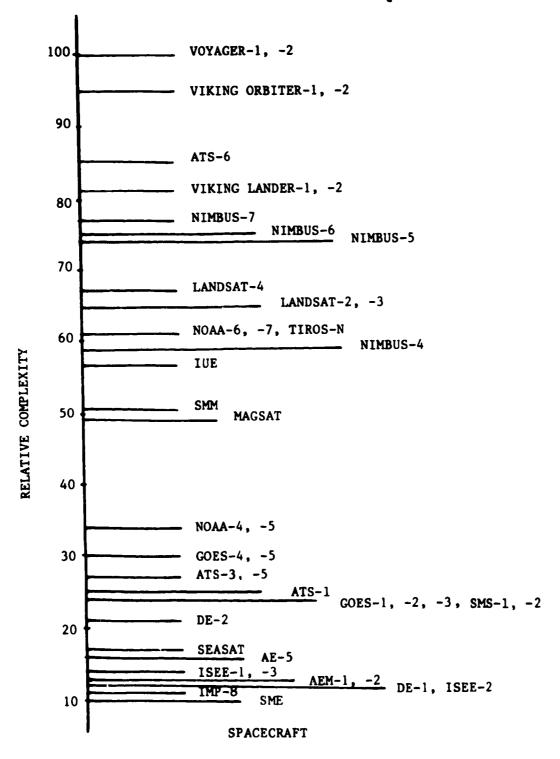


EXHIBIT 3 - RELATIVE SPACECRAFT COMPLEXITY

III. ANOMALY CLASSIFICATIONS

Because of the large number of anomalous incidents in this sample (and in previous samples) classification and summarization procedures are mandatory to extract readily useable information. From the relevant spacecraft EARs, a summary of each anomalous incident in this sample has been prepared. The summary is found in Appendix B-1 in the same format as the corresponding data for the earlier comprehensive studies. Appendix B-1 lists, by spacecraft, every anomalous incident recorded in the EARs subsequent to a successful launch. Each anomalous incident contains the following information:

- . An anomaly index relating the incident, unambiguously, to the information in the EAR.
- 2. Time the incident occurred. An entry of ε indicates that the incident occurred between the end of countdown and the establishment of the initial orbit. An entry of indicates that the anomaly cannot be pinpointed in time since it was intermittent, gradual, or unknown. All other entries are in hours.
- Three short statements giving a description of the incident,
 its cause, and its effect on the mission as a whole.
- 4. Any known corrective action taken to prevent occurrence of the incident on future flights or to obviate its effect on the flight under consideration.
- Other clarifying remarks required to put the incident in the proper context.

In addition to this summarization, two kinds of anomaly classifications were accomplished: (1) compilations by the classification codes used in all previous studies (the standard approach), and (2) compilations by a set of additional classification codes designed to more fully describe the characteristics of the observed anomalies.

Complete compilations are presented in Appendices B-2 and B-3, respectively, in the same order and using the same anomaly index as the summaries of Appendix B-1. The two sets of classifications and their results are discussed in the following subsections.

A. The Standard Approach

In the standard approach, there are nine characteristics for which each anomalous incident is coded. Some of the information needed to select a particular code for a given entry may occur only in the EAR so that, in a sense, the classification codes carry more information than that provided in the entries of Appendix B-1. The complete standard approach coding of each entry is given in Appendix B-2. Unsuccessful launches are not included in these appendices.

Fxhibit 4 defines the categories and codes for eight of the classifications used. The ninth classification, Subsystem Function is defined in Subsection III.A.8 below. Definitions of the terms, the results of classifying the 606¹ anomalies of this study and the 2,096¹ anomalies of Reference 15 are given in the following subsections.

These totals do not include unsuccessful launches.

EXHIBIT 4 - ANOMALOUS INCIDENT CLASSIFICATION CODES, STANDARD APPROACH

I. Mission Subset

- U. Unsuccessful Launch
- S. Spacecraft with No Anomalies Reported

Spacecraft with Anomalies Reported

II. Mission Term

- L. Long Term
- S. Short Term

III. Mission Phase

- L. Launch and Acquisition
- O. Orbital (Steady-State)
- Q. Unknown

IV. Mission Effect

- 1. Negligible
- 2. Non-Negligible but Small
- 3. 1/3 to 2/3 Mission Loss
- 4. 2/3 to Nearly Total Mission Loss
- 5. Essentially Total Mission Loss
- U. Unknown

V. Spacecraft Subsystem

- a. Timing, Control and Command
- b. Telemetry and Data Handling

- c. Power Supply
- d. Attitude Control and Stabilization
- d* Propulsion
- e. Environmental Control
- f. Structure
- g. Payload (Experimental and Scientific)
- h. Unknown

VI. A. Incident Type

- E. Electrical
- M. Mechanical
- O. Other
- U. Unknown

VI. B. Incident Type

- C. Catastrophic Part Failure
- O. Other Part-Related Incident
- N. Non-Part-Related Incident
- U. Unknown

VII. Incident Cause

- A. Assignable
- N. Non-Assignable
- U. Unknown

Roman numerals following the paragraph headings refer to the Roman numerals in Exhibit 4.

1. Mission Subset (I)

This code simply identifies the unsuccessful launches (U) and those spacecraft for which there are no reported anomalies (S).

For this study, one of the 44 spacecraft launches (NOAA-B) was unsuccessful; there were no spacecraft that experienced zero anomalies. The breakdown by number of spacecraft and percentage is as follows:

		Nu	mber	Pe	rcent
		This Study	Reference 15	This Study	Reference 15
Mis	sion Subset				
v.	Unsuccessful Launch	1	43	2.3	12.3
s.	Spacecraft With No Anomalies Reported	0	40	0	11.4
	Spacecraft with Anomalies Reported	43	267	97.7	76.3

2. Mission Term (II)

The code identifies long-term (L) or short-term (S) missions. If a mission is anticipated to be longer than 60 days it is classified long-term. All spacecraft in this data sample are long-term missions.

The breakdown, by number of anomalies and percentages, is as follows:

	Nu	mber	Per	cent
	This Study	Reference 15	This Study	Reference 15
Mission Term				
L. Long Term	606	1,695	100	80.9
S. Short Term	0	401	0	19.1

3. Mission Phase (III)

A spacecraft mission can be thought of as consisting of two distinct phases: launch and acquisition (L) and the orbital or steady-state phase (0). An anomaly occurring during launch and acquisition is classified L; if it occurs during steady-state operation it is classified 0. A third category, Q, is provided for those instances where the dichotomy cannot be made due to insufficient information. The distinction is made on the best judgment available based on the engineering analysis reports. Generally, those incidents indicating an ε , or very few hours of elapsed time at occurrence, are classified as L, all others as 0.

The breakdown of anomalies occurring in each category and the associated percentages is as follows:

		Nu	mber	Per	rcent
		This Study	Reference 15	This Study	Reference 15
Mis	sion Phase				
L.	Launch and Acquisition	61	480	10.1	22.9
0.	Orbital (Steady-State)	545	1,608	89.9	76.7
Q.	Unknown	0	8	0	0.4

4. Mission Effect (IV)

The five groups included in this classification indicate the severity of the anomalous incident in terms of its effect on the overall mission had it occurred in isolation. The definition of each class 1, 2, 3, 4, and 5 should be self-evident from the classification names given in Exhibit 4. Thus, in column IV of the tables in Appendix B-2 all incidents coded 1 have essentially negligible effect on mission performance; those coded 5 are essentially catastrophic to the mission. The code U indicates there was insufficient information on which to assign a mission effect code.

The breakdown of these groups, by number and percent of anomalies, is as follows:

		Nur	mber	Percent	
		This Study	Reference 15	This Study	Reference 15
Mis	sion Effect				
1.	Negligible	447	1,330	73.8	63.4
2.	Non-Negligible but Small	117	579	19.3	27.6
3.	1/3 to 2/3 Mission Loss	32	93	5.3	4.7
4.	2/3 to Nearly Total Mission Loss	5	20	0.8	0.9
5.		4	44	0.7	2.1
υ.	_	1	25	0.2	1.2

5. Spacecraf Subsystem (V)

Each anomalous incident is coded according to which of eight major spacecraft subsystems is most closely related to the incident.

An unknown category is included for those cases where a relationship does not exist or cannot be determined from the available information. The subsystems used for this classification are meant to define broad functional operations found to one extent or another in all spacecraft. The functional definition for subsystems was chosen rather than a definition based on hardware for two reasons. First, subsystem definitions vary among organizations and among program offices of the same organization. The data analysis requires a grouping that can be applied to all spacecraft of the collective data sample. The second and more important reason for using a functional definition is that, in the predesign stages of fu'ure programs, the program management will know what functions the planned spacecraft is expected to perform with more certainty than the actual hardware configuration that will be used to perform the desired functions. The comparisons at the subsystem level as defined in this report would be useful in the predesign phase of program development. For example, one would be interested to know, based on past experience of other programs, with what certainty a spacecraft would deploy its structural elements (structure subsystem) or supply power to the other planned functions (power supply subsystem). In the later stages of development of a projected program, when more is known about the hardware configuration, the interest would shift to the equipment group/component level of analysis which is hardware oriented.

The following list defines the subsystems and indicates the types of equipment that are considered to be a part of each subsystem.

Command receivers, decoders, timers, programmers, sequencers, command distribution equipment

b. Telemetry and Data Handling

Encoders, D/A converters, A/D converters, tape recorders, signal conditioners, telemetry transmitters, tracking transmitters, antennas

c. Power

Batteries, solar arrays, fuel cells, converters, inverters, regulators, protective devices, charge regulators

d. Attitude Control and Stabilization

Gyros, spin control, magnetometers, sun aspect indicators, eddy current dampers, horizon scanners, ster trackers, dynamic control

d* Propulsion

Coding this subsystem with a d* indicates that the propulsion subsystem considered here is more closely related to the attitude control subsystem of the spacecraft than to the launch vehicle. Included are hydrazine thrusters, tanks, valves, etc.

e. Environmental Control

Both passive and active thermal control devices, life support systems, etc.

f. Structure

Basic structure, booms, solar paddles separation.

g. Payload (Experimental and Scientific)

Wide-band communications (for spacecraft where this equipment was considered experimental), microwave

equipment (cavities, TWTs, etc., flown for assessment purposes), university experiments, particle detectors, mass spectrometers, plasma analyzers, infrared radiometers, ultraviolet radiometers.

Although it is felt that these groupings are essentially self-explanatory, checking a few of the codes in Appendix B-2 with their corresponding entries in Appendix B-1 should dispel confusion. This procedure is applicable to most of the other classifications as well.

The breakdown, in terms of number of anomalies and their associated percentages, to each of the subsystem categories is as follows:

		Num	Number		cent
		This Study	Reference 15	This Study	Reference 15
Spa	cecraft Subsystem				
a .	Timing, Control and Command	55	290	9.1	13.8
ъ.	Telemetry and Data Handling	116	599	19.1	28.6
c.	Power Supply	56	199	9.2	9.5
d.	Attitude Control and Stabilization	123	287	20.3	13.7
ď.	Propulsion	26	62	4.3	2.9
e.	Environmental Control	16	36	2.6	1.7
f.	Structure	6	47	1.0	2.2
8.	Payload (Experimental and Scientific)	208	540	34.3	25.8
h.	Unknown	0	36	0	1.7

6. Incident Type (VI)

a. <u>Incident Type</u> (VI.A)

one of four mutually exclusive groups: electrical (E), mechanical (M), other (O), and unknown (U). Those entries in Appendix B coded with an E in the VI.A column indicate that anomalous behavior is exhibited by electrical or electronic parts, components, subsystems, or functions. Those anomalies coded M are similarly defined for mechanical parts, components, subsystems, or functions. An O indicates behavior of equipment that cannot be classified electrical or mechanical: propellant degradation, for example. A U indicates insufficient information to assign the entry to any of the other three categories.

The breakdown of anomalies and percentages in this classification group is as follows:

		Number		Percent		
		This Study	Reference 15	This Study	Reference 15	
Inc	ident Type					
E.	Electrical	329	1,538	54.3	73.4	
M.	Mechanical	64	192	10.6	9.2	
٥.	Other	197	158	32.5	7.5	
v.	Unknown	16	208	2.6	9.9	

b. Incident Type (VI.B)

The classification of column VI.B in Appendix B attempts to divide incidents into those that are part related and those that are non-part related. A code of C indicates those incidents arising

from a catastrophic part failure. An O indicates that the anomalous incident is related to behavior of a part (or parts) that has not failed catastrophically (degraded, intermittent, etc.). An N indicates an anomalous incident not related to any part misbehavior. A U indicates that insufficient information exists to determine whether part behavior was involved or not.

The breakdown by number and percentage of anomalies for these categories is as follows:

		Number		Perc	entage
		This Study	Reference 15	This Study	Reference 15
Incident Type					
c.	Catastrophic Part Failure	21	225	3.5	10.7
ο.	Other Part- Related Incident	52	242	8.6	11.5
N.	Non-Part- Related Incident	277	727	45.7	34.7
υ.	Unknown	256	902	42.2	43.0

7. Incident Cause (VII)

Three broad groups are defined for incident cause in column VII of the tables in Appendix B: assignable causes (A), non-assignable causes (N), and unknown (U).

An assignable cause is attributed to an anomalous incident if the incident could have been prevented by taking some action well within the

The term "catastrophic" here is defined to mean "catastrophic" to the part and not necessarily to the larger component system. Typical types of catastrophic part failures include a transistor or diode shorting for no known reason. This definition is consistent with that used in the negative exponential distribution for modelling failure probability.

state-of-the-art prior to launch. If the incident could not have been prevented in this manner, it is classified nonassignable (N). If insufficient information exists to make a judgment, the anomaly is classified unknown (U).

The breakdown for these categories is as follows:

		Number		Percent		
		This Study	Reference 15	This Study	Reference 15	
Inc	ident Cause					
A.	Assignable	251	732	41.4	34.9	
N.	Non-Assignable	83	264	13.7	12.6	
U.	Unknown	272	1,100	44.9	52.5	

Further discussion of the assignable cause category is given in Subsection III.B, below.

8. Subsystem Function (VIII)

This classification is a secondary breakdown of spacecraft subsystem .

The assignment of anomalies to the subsystems (characteristic V) is helpful in narrowing down the functional aspects of spacecraft which are the most troublesome. A further step in this direction is justified to isolate more precisely the location of anomalous incidents. To do this a number of subfunctions (characteristic VIII) are defined for each previously defined spacecraft subsystem. The subfunctions for each subsystem are defined so that they are mutually exclusive and exhaustive, i.e., they do not overlap and they do cover the entire subsystem. In determining the quantities of the subfunctions and their associated anomalies, only data that specifically identifies the subfunction is considered. For instance,

ment is made to that category. Each anomalous incident carries, therefore, two codes relating the incident to functional location within the spacecraft. The subsystems, subfunctions, and codes used for each are tabulated in Exhibits 5 and 6. Exhibit 5 gives the total number of functions in this sample, the total number of anomalies observed, and the anomalies per function for this study. Exhibit 6 presents the same information for data previously available in the PRC data bank and reported in Reference 15.

EXHIBIT 5 - DETAILED CLASSIFICATION OF ANOMALOUS INCIDENTS BY SPACECRAFT SUBSYSTEM AND FUNCTION, THIS STUDY

-	Subsystem Function	Number of Functions in Sample	Number of Reported Anomalies by Function	Anomalies per Function
a.	TIMING, CONTROL,			
	AND COMMAND	43	55	1.28
	1. Receiving	43	21	0.49
	2. Decoding	43	3	0.07
	3. Command Distribution	25	17	0.68
	4. Sequencing and			
	Programming	27	5	0.19
	5. Timing	28	9	0.32
	6. Manual Control	-	-	-
	7. Unknown	-	-	-
	8. Unassignable	-	-	-
ъ.	TELEMETRY AND			
	DATA HANDLING	43	116	2.70
	1. Data Point Sensing			
	and Monitoring	43	13	0.30
	Signal Conditioning	8	1	0.12
	3. Encoding, Formatting	43	2	0.05
	4. Data Storage	27	43	1.59
	5. Transmission	43	56	1.30
	6. Unknown	-	-	-
	7. Unassignable	-	~	-
c.	POWER	43	56	1.30
	1. Conversion	43	4	0.09
	2. Storage	41	3	0.07
	3. Power Control	42	45	1.07
	4. Power Distribution	17	2	0.12
	5. Unknown	-	2	-
	6. Unassignable	-	-	-
đ.	ATTITUDE CONTROL			
	AND STABILIZATION	40	123	3.08
	1. Orientation Sensing	40	90	2.25
	2. Active Attitude			
	Correction	22	19	0.86

EXHIBIT 5 - (Continued)

-	Subs	ystem Function	Numbe Funct in Sa	ions	Numbe Repor Anoma by Fun	ted lies	Anoma per Fi	lies metion
	3. P	assive Stabilization		8		3		0.38
	4. U	nknown		_		1		-
	5. U	massignable		-		10		-
d*.	PROPU	ILS ION	37		26		0.70	
	1. N	avigation		4		4		1.00
	2. P	ropulsion		33		22		0.67
	3. U	inknown		-		-		-
	4. U	Inassignable		-		-		-
e.	ENVIR	CONMENTAL CONTROL	43		16		0.37	
	1. A	Active Thermal Control		23		15		0.65
	2. L	ife Support		-		-		-
		Inknown		-		-		-
	4. t	Jnassignable		-		1		-
f.	STRUC	CTURE	43		6		0.14	
	1. I	Basic Structure		43		5		0.12
	2. I	Deployable Structure		33		1		0.03
	3. 9	Separation		43		0		0.00
		Unknown		-		-		-
	5. 1	Unassignable		-		-		-
g.	PAYLO	DADS	256		208		0.81	
	1. :	Scientific		230		205		0.89
	2.	Technical		26		1		0.04
		Unknown		-		1		-
	4.	Unassignable		-		1		-
h.	UNKN	<u>own</u>	-		-		-	

EXHIBIT 6 - DETAILED CLASSIFICATION OF ANOMALOUS INCIDENTS BY SPACECRAFT SUBSYSTEM AND FUNCTION, REFERENCE 15

	Subsystem Function	Number of Functions in Sample	Number of Reported Anomalies by Function	Anomalies per Function
a .	TIMING, CONTROL, AND COMMAND	265	290	1.09
	1. Receiving	261	103	0.39
	2. Decoding	251	23	0.092
	3. Command Distribution	72	30	0.42
	4. Sequencing and	7-		• • • •
	Programming	188	63	0.33
	5. Timing	133	30	0.22
	6. Manual Control	11		
	7. Unknown		29	
	8. Unassignable		12	
ъ.	TELEMETRY AND			0.13
	DATA HANDLING	277	601	2.17
	1. Data Point Sensing		•••	1.06
	and Monitoring	164	206	1.26
	Signal Conditioning	46	3	0.065
	3. Encoding, Formatting	264	63	0.24 1.20
	4. Data Storage	126	151	0.56
	5. Transmission	270	151	0.30
	6. Unknown		14 12	
	7. Unassignable		12	
с.	POWER	282	199	0.70
	1. Conversion	175	40	0.23
	2. Storage	271	77	0.28
	Power Control	247	50	0.20
	4. Power Distribution	179	12	0.067
	5. Unknown		18	
	6. Unassignable		2	
d.	ATTITUDE CONTROL		205	. 17
	AND STABILIZATION	244	285	1.17
	1. Orientation Sensing	226	131	0.58
	Active Attitude Correction	209	250	1.20

EXHIBIT 6 - (Continued)

	Subsystem Function	Number of Functions in Sample	Number of Reported Anomalies by Function	Anomalies per Function
	3. Passive Stabilization	69	11	0.16
	4. Unknown		16	
	5. Unassignable	n=	8	
d∗.	PROPULSION	121	62	0.51
	1. Navigation	108	11	0.10
	2. Propulsion	121	37	0.30
	3. Unknown		4	
	4. Unassignable		10	
e.	ENVIRONMENTAL CONTROL	80	36	0.45
	l. Active Thermal Control	1 63	24	0.38
	2. Life Support	12	13	1.08
	3. Unknown		2	
	4. Unassignable		5	
f.	STRUCTURE	272	47	0.17
	1. Basic Structure	267	2	0.0075
	2. Deployable Structure	89	33	0.37
	3. Separation	256	11	0.043
	4. Unknown		1	••
	5. Unassignable			
g.	PAYLOADS	809	544	0.67
	1. Scientific	711	423	0.59
	2. Technical	98	120	1.22
	3. Unknown		1	
	4. Unassignable		- t,	
h.	UNKNOWN		36	

B. Additional Categories

anomaly data were considered. These included additional treatment of anomaly causes, anomaly type, history, test background, level of space-craft breakdown giving rise to the anomaly, the heritage of anomalous hardware, etc. Many of these considerations are reflected qualitatively in the engineering analysis of Section IV.B. Quantitatively, four characteristics were found to have sufficient information to provide additional useful categorization. These are cause, type, testability, and source. Exhibit 7 defines the categories and codes for these additional classifications. It also provides the number and percentage of the 606 anomalies assigned to each category. Definitions of the terms and notes on classifying the 606 anomalies of this study are given in the following subsections.

Roman numerals following the paragraph headings refer to the Roman numerals in Exhibit 7. A complete tabulation of these codes, by anomaly, is given in Appendix B-2.

1. Anomaly Cause (X)

Anomaly cause is treated in the standard approach but only to the extent of determining if the anomaly has an assignable cause or not. While the previous studies in this series further analyzed the anomalies with assignable causes, no formal coding was reported. This categorization remedies that situation and also defines a new set of "causes" more in keeping with recent data. The first three categories all represent design problems. The first, Space Environment, is invoked when the design provides an inadequate response to the environmental stresses of space.

EXHIBIT 7 - ANOMALOUS INCIDENT CLASSIFICATION CODES, ADDED CHARACTERISTICS

X.	Anomaly Cause		Number	Percent
	-	vironment	56	9.2
		Software	21	3.5
	c. Design,		90	14.9
		Control/Workmanship	25	4.1
	e. Contamin		21	3.5
		phic Part Failure	40	6.6
		phic Circuit Failure	25	4.1
		phic Component Failure	28	4.6
		phic Black Box Failure	33	5.4
	j Unknown		267	44.1
	TOTAL		606	100.0
XI.	Anomaly Type			
	S. Systemat	ic	216	35.6
	W. Wearout/	Aging/Depletion	44	7.3
	C. Chance		20	3.3
	G. Glitch		52	8.6
	U. Unknown		274	45.2
	TOTAL		606	100.0
XII.	Testability			
	Y. Yes		95	15.7
	N. No		90	14.9
	M. Maybe		116	19.1
	U. Unknown		305	50.3
	TOTAL		606	100.0
XIII.	Source			
	1. Part		68	11.2
	2. Circuit/	Subassembly	66	10.9
	3. Componen	-	117	19.3
	4. Black Bo	x	97	16.0
	5. Subsyste	m/Interface	15	2.5
	6. Interact		153	25.2
	7. Unknown		90	14.9
	TOTAL		606	100.0

The second, On-Board Software, covers anomalous behavior attributable to errors in software or to software which is inadequate for actual operational procedures. The third category, Design, Other, covers all other anomalies attributed to design deficiencies. Anomalies are categorized as Quality/ Workmanship if, and only if, the source documentation so specifies. Thus, there may be more of these anomalies than appear in the Exhibit 7 tabulation. Contamination includes all reports of any kind of foreign matter in or on the spacecraft hardware. Catastrophic failure occurs when a particular level of hardware (Part, Circuit, Component, Black Box) fails completely for none of the previously listed causes. Parts are single integrated circuits, valves, motors, etc. Circuits are actual electrical circuits (oscillators, amplifiers, etc.) or small collections of parts (gear assemblies, for example). Components are sets of "stand-alone" hardware, typically: tape drives, power converters, gyro electronics. Black Boxes are complete functional units, e.g., tape recorders, batteries, solar arrays, or command decoders. The Unknown category is reserved for those anomalies for which there is insufficient information to make any other assignment.

2. Anomaly Type (XI)

The standard approach treats anomaly type in two dimensions.

The first distinguishes between electrical, mechanical, or other (chemical, etc.) type of anomaly and the second the relationship of the anomaly to piece part behavior. This categorization examines whether the anomalies are deterministic or not. Thus, the category Systematic includes anomalies that would recur if identical hardware were operated under identical conditions. Wearout, Aging, and Depletion are special cases of systematic anomalies and have been

broken out separately. Two kinds of "random" anomalies have also been included. The first, Chance, represents significant anomalies that would not necessarily occur if identical hardware were operated under identical conditions. These anomalies are almost always reported in the source documentation as random failures. Glitches are also randomly occuring anomalies. They are usually insignificant in terms or mission effect, occur at most a very few times then disappear requiring no corrective action other than perhaps a command to restore proper status. Again, nearly half of the anomalies cannot be assigned to the above categories.

3. Testability (XII)

This categorization answers the question, "Could prelaunch testing have revealed the anomaly?" A "Yes" was assigned if it was reasonably clear that some type of testing would have produced the anomaly. A "Yes" was not assigned if the required testing was beyond a reasonable definition of the state of the art or would have required testing of excessive duration.

A "No" was assigned if no test would have a reasonable expectation of producing the anomaly (a random part failure, for example). A "No" was also assigned if a test could be conceived but was clearly impractical (requiring zero gravity, for example) or would have been prohibitively expensive. An assignment of "Maybe" covers the situation in which test expense or sophistication while not clearly out of the question are approaching that situation. This category is also assignmed when a clear distinction between "Yes" and "No" is not possible based on available data. The "Unknown" category represents the case where there is not enough information available to make any other assignment.

4. Source (XIII)

This classification has been constructed to reveal where the anomalies originate. The first four categories are simply hardware items of increasing levels of complexity. The hardware levels are defined as in the Anomaly Cause classification. In each case, the lowest applicable level was assigned that the available information would support. A few anomalies could not be isolated below the Subsystem/Interface level. These are mostly incorrect wiring harnesses. A much more frequently occurring source is "Interaction." This covers all anomalies where incorrect responses occur between groups of hardware or between the hardware and its operating environment. Typical anomalies in this category are wheel unloading when the tape recorder stops, RF1, turn-on transients, and contamination of one set of hardware due to outgassing from another. The "Unknown" category is assigned where insufficient information is available to make any other assignment.

IV. ANALYSIS

For this study, two types of analyses of the basic anomaly and spacecraft survival data were conducted. The first deals with spacecraft and spacecraft subsystem performance over their observed lifetimes. The second is an engineering analysis of several special factors.

A. Performance Summaries

The performance of each spacecraft considered in this update is indicated on a separate bar chart in Appendix C-1. The survival time for each subsystem (as defined in the documentation for that spacecraft) is presented as are the survival times for all anomalous components. Survival times are also indicated for the redundant units of anomalous components whether or not they themselves had anomalies. Each and every anomaly is charted at the time it occurred and against the component or subsystem in which it occurred. A distinction is made on the charts between failing components (totally unusable) and less serious anomalies.

For those spacecraft that were considered in previous studies, all anomalies from launch have been included even though these anomalies do not otherwise form part of the update data base. They are treated in Reference 15.

A second set of charts indicates the performance of major spacecraft subsystems. These are collected in Apendix C-2. Since each spacecraft has a somewhat different breakout of subsystems, we have standardized on the eight defined in subsection III.A.5. For the major

subsystems (Timing, Control and Command; Telemetry and Data Handling;
Power Supply; Attitude Control and Stabilization, and Payload) an entry is
made for each spacecraft whether or not it had significant anomalies in
the subject subsystem. If it had significant anomalies, the anomalous
components (and their redundant units, if any) are also listed. The
Structure subsystem does not appear since there were no significant
anomalies in this subsystem in this update. Since so few anomalies
occurred in the Propulsion and the Environmental Control subsystems, only
those spacecraft are listed which suffered significant anomalies in these
areas.

In addition to being ordered by subsystem rather than space-craft, this set of charts differs from the spacecraft charts in two ways. First, only "significant" anomalies are included. These are generally those categorized as having a mission effect code of 2 or greater (see subsection III.A.4) although all anomalies in redundant units, whose mission effect is negligible because of the redundancy, are also included. The second major difference is that time, rather than being plotted in hours, is plotted in units of spacecraft design life. Thus, an operating time of 67 months for an AE-5 subsystem is plotted as 67/12 = 5.6 since its design life is one year (see Exhibit 2). Similarly, an operating time of 62 months for an ATS-6 subsystem is plotted as 62/24 = 2.6 since the ATS-6 design life is two years.

B. Engineering Analyses

Engineering analyses were conducted to provide further insights into the nature of the anomalies that have occurred on the satellites in this update. The analyses covered seven areas ranging from persistent problems and test-related anomalies to black box failures and RFI/EMI. Each of the seven areas is discussed below in a separate subsection.

1. Persistent Problems

In an earlier analysis of the data bank, it was found that over 80 percent of all anomalies fell into 30 categories of leading problem areas (Reference 14). It was also noted that these categories represented "persistent" problems in that the anomalies occurring on the more recently launched spacecraft were of the same types as the anomalies on earlier spacecraft. Since a significant amount of new data were collected on this data bank update, it was deemed desirable to reexamine these persistency trends.

Once again it was found that approximately 80 percent of the anomalies "fit" the 30 problem areas. Exhibit 8 depicts the rank order of these problem areas for this update, for the 1978 update and for the pre-1978 data bank. The three-part exhibit illustrates the persistency of the problem areas over time as well as the shifts in their ranks.

A number of interesting observations can be made from the exhibit. For example, as time passes fewer problem areas account for 50 percent of the anomalies. This implies that by addressing the five upper-ranking problem areas in this update one would in fact be addressing forty percent of the observed anomalies. In the pre-1978 era, nine problems would have had to be addressed to achieve similar coverage.

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EXHIBIT 8 - RAW ONDER OF PROBLEM AREAS

(Note: Ranking is in descending order by number of anomalies, i.e., \$1 had the most securation)

THIS UPDATE	1. Scientific Instruments 2. Propulaton (Constal) 3. RT/OH 4. Talemery Sending 5. Tage Incorders 6. Thermal Control 7. (Command 6 Centrol (Ingic)	9. Command & Control (Registers, Masseises) 9. Deployable Structures 10. Violentry Receding 10. Violentry Receding	Solar Arroy, Commer (4) [Commerce & Concret [Timers, Sequencers) [Timers, Sequencers) [Timers Conditioning [Northern Sensors [2] Sun Sensors	13. (Sperious Comments 14. (Start Mulpum) 15. (Star Trechers 20ler Arrey Dagredeties 15. (Mathemat, M-lock On 15. (Ma	(Commend, EP-Other (2) 16. Thelemetry, BF (Mideband, Other (3) 17. Solar Array Brives
1978 UPDATE	1. Scientific Instruments 2. NT/DNI 3. Tope Becorders 4. Camers Equipment 5. Propulsion (Chemical) 6. Stortunes 7. Wideband Transmitters 7. Wideband Transmitters	8. Deployable Structures 9. Telemetry Seming 10. Solar Array, Other (4) Telemetry, RF 11. Command & Control	(Timers, Sequencers) 12. Sum Semoors 13. Power Conditioning 14. Command & Control (Logic) 15. Telemetry Eccoding (Sepertons Commandes		21. Underson mediate 22. Syron 24. (Solar Array Drives 25. Commond, NP-Other (2)
21v04n 9/61-384	1. Scientific Instruments 2. Taye Bacorders 3. Camera Equipment 4. Batterion 5. WI/UII 6. Camend 6 Castrol (Logic) 7. Telementry, WF	9. Sperious Comments 10. Talemetry Secoding 11. Commend & Control (Timers, Sequencers)	12. Command, EF-Lock On 13. Command & Control (1) (Inglators, Manorites) (2) Star Trackers 14. Telemetry Sensing	Underson Franchiters 13. [Section Meals 16. Comment (7. Other (2) 17. Thereal Central 18. Employable Structure 19. Employable Structure 19. Employable Structure	11. Solar Array Degradation 22. Solar Array, Other (s) 23. Oyras 24. Solar Array Brives 25. Hidahand Deceivers 26. Hidahand Transparders

MOTES: (1) Brachets indicate a "tia" for the bracheted rank (2) Other than Command, ED-Lock Co. (3) Other than Array degradation (4) Other than Array degradation (5) Brached line indicates the "madian." i.e., the categories above and below the line each represent approximately half of the total anomaly count.

The rank of tape recorders as a problem area has dropped steadily from the first sample to the last while remaining a significant problem area.

Note that this drop in rank could mean either that tape recorders are getting better or other problems are getting worse. RFI/EMI also continues to be a significant problem.

Chemical propulsion now ranks second only to scientific instruments as a problem area. It's ranking in the pre-1978 sample was 15 and in the 1978 sample it was 5. Part of the reason for the rank increase in this study is the large number of propulsion problems on ATS-6. However, many other spacecraft suffered from 1 to 3 propulsion problems, indicating that anomalous behavior in chemical propulsion systems is a general and increasingly severe problem. Another interesting increase is observed in the gyro category. The ranks are 23, 23, 8 from the earliest to the most recent sample.

This is due in part to several gyro problems on IUE, TIROS-N, and NOAA-6 but again it seems to be a more general problem as well and a definite cause for concern.

The RF Telemetry category ranking dropped from 7 to 11 to 16 in the most recent sample. A major reason for this is that spacecraft now rely extensively on S-band equipment for telemetry, and S-band anomalies are included in the Wideband categories.

2. Test-Related Anomalies

Anomalies in the update sample were classified according to whether they might have been eliminated through some type of testing (See Section III.B). Anomalies known to be related in some fashion to the testing program were also identified. Twenty seven such anomalies were found and although there are undoubtedly others, specific information is available only for these 27.

Seven anomalous incidents were reported that were known to exist as anomalies prior to launch. One typical anomaly of this type involved a memory halt on LANDSAT-3 when an S-band timer reset was commanded. This abnormal response had occurred occasionally prior to launch. On SEASAT, a 21 GHz electrical temperature monitor was reported as failed prior to launch, then returned to normal operation, but failed again about 300 hours into the mission. Another typical anomaly involves payload data interference over the South Atlantic Anomaly on NIMBUS-7; this was expected due to the type of data channel detectors utilized.

Ten anomalies were of a type noted prior to launch but not then considered to be an anomaly. For instance, on NOAA-6 a ceramic capacitor had been identified as a problem component before launch, and was replaced with specially screened items. Nevertheless, problems with this capacitor recurred and caused significant losses of instrument data. In another case, a tape recorder on SME did not respond to playback commands when the unit was cold; symptoms of this anomaly had been noted in prelaunch tests

Two anomalies -- both on NIMBUS 7 -- were specifically reported as having not been revealed in testing. One of these involved interference with the scanning of one instrument by the scanning of another instrument. It was reported that this was possibly due to structural resonance or structural transmission, and that the test fixture could have masked structural effects. The other anomaly of this kind involved unexpectedly high temperatures of the cooler door and cone on the Coastal Zone Color Scanner. It was reported that this possibly occurred because of higher earth albedo in orbit than was simulated in thermal-vacuum testing.

Four anomalies existed prior to launch but went undetected, including a wiring error in a thruster control harness on AE-5.

Four anomalies were reported that involved settings or procedures based on test data that were later found to be inadequate. For instance, on Viking Lander 2 battery temperatures increased significantly higher than predicted. It was reported that the temperature predictive model was based on data from preproduction, prototype batteries rather than flight batteries, and was in error.

3. Environmental Effects

Of the 606 update anomalies, 56 (or slightly over 9 percent) were caused by some type of environmental effect. Since this is a rather significant proportion of the anomalies, and particularly since many of these anomalies could possibly have been prevented by more adequate design or testing provisions, the anomalies were further investigated in terms of hardware and functional areas.

In this investigation, environmental effects were broadly defined as those originating external to the spacecraft itself. It was found that ten categories encompassed these effects:

- (1) Effects of orbit: Determined by orbital characteristics such as eclipse and solstice, sun angle, day/night and night/day transitions, orbital location, etc.
- (2) Temperature effects: Created by the space thermal environment and the reactions of the spacecraft to this environment.

- (3) Sun effects: Resulted from the sun's visible spectrum.
- (4) Moon effects: Resulted from lunar gravitation and reflected light.
- (5) Atmospheric noise: Associated with the atmospheric RF spectrum.
- (6) Effects of vacuum: Associated with the space vacuum.
- (7) Earth effects: Resulted from albedo and the earth's magnetic field.
- (8) Radiation effects: Associated with space radiation.
- (9) Effects of launch: Created by the launch environment.
- (10) Other: Environmental effects not encompassed by the other categories.

From the above, it can be seen that "overlap" between the categories can occur. For instance, an excessive spacecraft temperature might be due to either the space thermal environment or the sun angle as determined by the spacecraft's orbital characteristics. In assigning anomalies to the environmental effects categories in this investigation, such possible overlaps were handled by basing the assignment on the primary environmental effect leading to the the anomaly as given in the data. That is, if the primary cause of spacecraft overheating was the sun angle, the anomaly was assigned to the orbital effects category rather than the temperature effects category. It is felt that assigning the anomalies in this manner provides a clearer indication of where more emphasis would be warranted during design and test.

Exhibit 9 depicts in matrix format the distribution of anomalies by hardware/functional area and the various environmental effects leading to them. Typical examples of anomalies assigned to each category are as follows:

- (1) In the "Effects of Orbit" category, anomalies include the GOES-4 loss of RF power from a UHF transmitter pre- and post-eclipse, and the MAGSAT anomaly involving sun interference in the star camera in the Southern hemisphere. Another example is the array "notching" that occurred on NIMBUS-7 at night/day transitions.
- (2) In the "Temperature Effects" category, anomalies include the deployment problem on SAGE attributed to a stiff cable due to low temperature. Also, the ATS-6 parabolic reflector antenna anomaly consisting of distortions due to diurnal thermal gradients was assigned to this category.
- (3) In the "Sun Effects" category, three of the anomalies involve abnormal operation of horizon scanners/earth sensors due to sun interference (SAGE, NOAA-7 and SEASAT). This category also includes erratic operation of NIMBUS-7 sun sensor at some sun angles.
- (4) All of the anomalies attributed to "Moon Effects" are associated with lunar illumination. Twice it interfered with earth sensor operation (GOES-3 and TIROS-N); it also interfered with the operation of a radiometer on TIROS-N.

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EXHIBIT 9 - AMMALIES ATTRIBUTED TO ENVIRONMENTAL EPPECTS

					Environmental Effect	Effect					
			Sub	Moon	Atmospheric	Lifects of	Larth	Radiation	Launch	Other	TOTAL
Spacecraft Mardware/Punction	Effects of	Effects	Effects	Effects	No.1 34	Vacuus	ET TOCK				.
Incurring Amonaly								•			^
	2				•			-			•
ALC BY B					7						~
Clocks					7				•		7
Commend Beceivers								-	•		
Computers/Mtcroprocessors		•									٠.
Deployables		-						-			٠.
Cyro electronics								-			→ •
Maat Pipes		•	-	7			-				
Mortzon Scamers/Larth Sensors		-	•	1				-			-
Hemories						,		-			•
Meteorological Payloads,			-	7				•			
Radiometers					•	•	-				•
Meteorological Payloads, Mos-Radiometers	-				7	, -	•		-		8
Propulaton		,				1					-4
heflectors (Antenne)		-					-			-	n (
Scientific Instruments		•				-		-		~	n ·
Spacecraft/System Lavel		-				-		~			-
Star Trachers/Star Cameras	-						•		-		•
Sun Semeors/Solar Aspect	7						-				-
Thermal Control					-						
Transmitters, S-band						ı	ı	١	•	ı	-1
Transmitters, UNF	- 1	i	1	ı ·	۱ -	•	•	=	•	•	*
TOTAL	•	•	•	•	•	•					

- Noise" were associated with the South Atlantic Anomaly; when the respective spacecraft were over this location, RFI caused a clock jump on SMM and interfered with a payload instrument on NIMBUS-7. LANDSAT-3 also experienced RFI over magnetic anomalies, although the data does not specify which ones. Also assigned to this category was a TIROS-N anomaly involving spurious command verifications; this was attributed to the receiver's frequency being in the neighborhood of amateur radio and television traffic.
- (6) Two of the anomalies assigned to "Effects of Vacuum" were caused by outgassing (LANDSAT 3 and Voyager 2). A third anomaly -- the star tracker on Voyager 2 tracking bright particles just after launch -- was also judged to be due to outgassing.
- (7) In the "Earth Effects" category, one of the anomalies includes a spectrometer on SME breaking-limits due to the effects of a "bright earth." On SEASAT, a horizon scanner tracked cold clouds, and on SMM earth albedo entered a sun sensor's field of view.
- (8) "Radiation Effects" includes three instances of array damage, one due to a large solar flare (ATS-6) and two due to the same large solar particle event (GOES-4 and GOES-5).

 Three other anomalies involve Jovian radiation effects on the Voyagers. Also, a radiation "hit" on DE-1 wiped out a microprocessor chip.

- (9) Three anomalies were caused by the "Effects of Launch".

 On MAGSAT, there were indications that a thermal panel came off during launch. On TIROS-N, propulsion problems were attributed to a nut relaxing due to launch shock.

 On Voyager 2, a computer became "confused" by the high boost rates and issued commands to counteract them.
- (10) Four anomalies were assigned to the "Other" category.

 On ATS-6, intermittent array thermistor operation was attributed cryptically to "the long term effects of cycling in orbit." The detector window of a scientific instrument on ISEE-3 was punctured by a micrometeorite.

 NOAA-7 experienced higher solar pressure torques than expected, and the Viking Orbiter 1 experienced a strong gravity gradient torque at periapsis.

4. Black Box Failures

As is evident from discussions elsewhere in this report, a large number of data bank anomalies involve intermittents (some of which "go away"), degraded performance that does not significantly impact the mission, or other types of anomalous behaviors that do not render the associated hardware useless. It seemed, therefore, that it would be of interest to identify and tabulate the anomalies where a significant piece of hardware became useless due to some type of problem.

These "significant pieces of hardware" are referred to herein as "black boxes," and include batteries, tape recorders, gyros, receivers, radiometers, and the like. The black boxes are generally elements of the basic spacecraft subsystems; experiments were specifically excluded from consideration in this analysis.

The data were then searched to identify those anomalies associated with the failures of black boxes. The definition of "failure" was that the black box was rendered useless by the anomaly. In some cases, this implies that the black box ceased to function; in others that the anomaly caused such degraded or erratic operation that the black box could not provide its intended function.

In the update sample, 65 such black box failures were found representing approximately 11% of all anomalies. The failures occurred on 17 types of black boxes. These data are depicted in Exhibit 10.

The quantities shown in the left-most column indicate the number of black box failures where redundancy was both provided and operable. In the next column, the number of failures shown are those where redundancy was provided but had previously failed. The next column indicates the rumber of failures where no redundancy had been provided.

is, the failures are not broken down to indicate redundancy provisions. This was done because batteries are seldom truly redundant since a remaining battery can carry only some portion of the load that could be handled by the original, non-failed complement of batteries.

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EXHIBIT 10 - BLACK BOX FAILURES

		Number of Pailures		
	Redundancy Provided	Redundancy Provided Bur Not Operable	No Redundancy Provided	TOTAL
BLACK BOX TYPE	And operative			
			-	-
Array Silp King Assemblies	•			-
Attitude Control Electronics	-			=
Batteries (only total number				•
	•			-
Command/Clock Power Supplies	-		•	7
Computers (on-board)	1		•	
Gyros/IMU's	7			٠ ،
IMU Power Supplies	-4	-		,
N CONTRACTOR OF THE CONTRACTOR	2			7
arcare, etc.				-
Panoranic Attitude Sensors	1 +	-	~	1
Radiometers	-			9
Radiometer Encoders	•	•	r	•
Reaction Wheel Power Supplies			•	, ,
Receivers, Wideband	2			• -
Receivers, UHF		•	•	• =
Tape Recorders	Φ	n	-4	. "
Telemetry Encoders	m			, ,
Transferers, Wideband	1		1	• 1
	1	1 (=	65
TOTAL	34	Φ.	11	}

In the update sample, there were 34 black box failures (not including batteries) where redundancy was available and operable. The major impact of these failures is therefore loss of redundancy protection. On twelve spacecraft, however, black box failures resulted in severe mission impacts. There are as follows:

- o Termination of the SAGE mission due to battery failure
- o Termination of the Viking Lander 2 mission due to computer failure
- o Loss of the SEASAT mission due to failure in the array slip ring assembly
- o loss of the SMM mission due to consecutive failures in all three reaction wheel power supplies
- o Loss of the TIROS-N mission due to failures in both redundant IMU power supplies.
- o Loss of primary payload data on SMS-1 due to failure of both S-band transmitters
- o Loss of primary payload data due to failure of both VISSR encoders on SMS-2, GOES-2, and GOES-3
- o Restriction of primary payload data gathering to realtime only due to failure of both primary and redundant tape recorders on LANDSAT 2, NIMBUS-5, and NIMBUS-6.

The impacts of the remainder of the black box failures tabulated in Exhibit 10 fall somewhere between the severe ones and loss of redundancy protection. Two of these remaining black box failures involve loss of a battery; the other 6 loss of a radiometer.

5. RFI/EMI

As indicated above, RFI/EMI ranks as an especially prevalent and persistent problem area. Of the 43 operating satellites in the update sample, 22 had RFI/EMI anomalies. The lack of such anomalies on the other 21 spacecraft may reflect lack of reporting rather than lack of such incidents. Overall, sixty-three anomalies caused by RFI/EMI were identified in the update sample, and they are distributed among various hardware areas as follows:

Scientific Instruments	11
Radiometers	8
Cabling/harness (cross-talk,	
coupling, etc.	8
Telemetry Transitters	3
Telemetry Monitors	3
UHF Receivers	2
Command Receivers	2
Battery Chargers	2
Attitude Sensors	2
Attitude Control Electronics	2
Spacecraft Clock	1
Command Decoder	1
Memory	1
Power Control Electronics	1
Thermal Control Electronics	1
S-band Transponders	1
Unknown	14

The anomalies represented above include cases of "internal" RFI where the extent and effects of the RFI were limited to the "black box" that generated it, and "external" RFI where the RFI generated in one area affected equipment in another area.

In making the above allocation of anomalies to equipment areas, the anomaly was charged to the offending equipment wherever there were sufficient data to make this assignment. This was clear-cut in cases of internal RFI. For external RFI, the equipment that was susceptible to RFI

was charged with the anomaly if it appeared that the equipment would not have been susceptible had more adequate RFI protection been provided. The equipment generating the RFI was charged when it appeared that the magnitude of the RFI was sufficiently high to penetrate normally adequate RFI protection in other equipment. The "Unknown" category includes anomalies where this distinction could not be made. Making these assignments required assumptions when the data did not specifically identify the offending equipment. These assumptions were based on engineering judgment using the descriptions of the anomalies.

Many of the RFI/EMI anomalies did not significantly affect space-craft performance. Some, however, were serious. In several instances, RFI/EMI caused significant losses of payload data. Also, in at least two instances the offending equipment had to be turned off and the back-up units selected, which resulted in loss of redundancy. Thus, it appears that in design and testing, the generation of, and susceptibility to, RFI/EMI warrants special consideration.

6. Deployments

On the spacecraft launches covered in this study sample, but not including spacecraft already covered in previous studies and updated in this sample, there were at least 71 deployment events. These events ranged from solar paddle and boom deployments to extensions of long antennas, but do not include separation or deployments involving simply the "spring-out" of short stub antennas and the like.

For these 71 deployment events, eight anomalies were reported.

Of these eight, only one involved a deployment failure, namely, the deployment failure of the 10 meter, Z axis Vector Electric Field Instrument boom on DE-2. This anomaly was attributed to an open in the power circuit.

The remaining 7 deployment anomalies are summarized as follows:

- o The SAGE S-band antenna required 40 minutes to deploy; attributed to low temperature stiffness of a coaxial cable;
- o The LANDSAT-3 left solar paddle did not slew as expected at deployment, possibly due to shadowing of a sun sensor;
- o LANDSAT-4 was initially unsuccessful in deploying the Ku-band antenna;
- o On MAGSAT, only 1 of the 2 despin timers functioned; timer #2 never became armed, possibly due to higher than expected thermal resistance between the fourth stage and the timer;
- o On NIMBUS-7, several squibs on instruments did not fire until the firing commands were repeated;
- o On NOAA-7, an instrument earth shield door was slow to deploy, possibly due to a mechanical hang-up;
- o The Voyager 2 Science Boom deployed to within 0.060 of the correct position and did not latch; the two most likely causes reported are debris in the folding strut hinge or insufficient drive in the folding strut;
- o On Voyager 2, telemetry indicated that the RTG Boom Release pyro-amplifiers "A" activated; but not the "B" set of amplifiers; there was some evidence that a transistor in the output switching portion of the pyro switching unit failed.

7. Miscellaneous

This subsection discusses four additional observations of interest.

- (1) Self Healing: The apparent self-healing capability which has been noted in previous data bank studies was again observed. In the update sample, there were 14 instances of anomalous behavior that cleared up without any type of intervention. These instances do not include "glitches" that occur once or a few times and then go away.
- (2) Array Temperature Sensors: During the course of this study, it appeared that a large number of array temperature sensor failures were reported. Further analysis revealed that six such sensors had failed catastrophically, and that these failures had occurred on HCCM, ATS-6, GOES-1, GOES-3, IUE, and SMS-2.
- Plume Impingement: On previous data bank studies, anomalies were occasionally noted involving impingement of the propulsion plume on some spacecraft surface. Four such instances were noted during this study; one each on GOES-4, GOES-5, Voyager 1, and Voyager 2. On the Voyagers, this caused 20% less ΔV than was expected, and subsequently more hydrazine use. It was reported that post-launch analyses based on more sophisticated techniques than had been applied earlier produced results agreeing with the observed phenomena.

(4) Problems Corrected/Mitigated from the Ground: On all previous data bank studies, instances were frequently noted where the anomaly was corrected or mitigated by some action taken on the ground. During this update, 75 such instances were identified. These instances include only those where the anomaly was actually corrected or the anomalous hardware restored to acceptable status from the ground. They do not include commanding-in a redundant unit, commanding the spacecraft back to the proper configuration following spurious turn-ons/turn-offs by "glitches," nor establishing procedures to allow some unit to warm-up before use. Even with such exceptions, the number of anomalies corrected or mitigated from the ground in this sample is significantly larger than the numbers noted in the past. There appear to be several reasons for this, one of them being the more extensive use of on-board computers.

This more extensive use of on-board computers presents more opportunities for correcting anomalous behavior via on-board software modifications that change operating points or procedures. It also increases the likelihood of anomalous behavior due to software errors. Of the 75 cases where anomalies were corrected or mitigated from the ground, roughly 20% involved corrections to on-board software discrepancies.

V. PERFORMANCE EVALUATION

Typically, spacecraft performance begins at (or near) its design capability immediately after a successful launch and then degrades over time as it incurs a wide variety of anomalies. A procedure to quantify spacecraft performance, or capability, over time using the PRC space data base was derived in Reference 11.

Each spacecraft anomaly in the data base is assigned to one of five mission effect categories as described in Section III. The procedure to quantify spacecraft capability begins by assigning a single numeric to represent "average" spacecraft degradation in each category as shown below:

	Mission Effect	Degradation
1.	Negligible	0.025
2.	Non-Negligible but Small	0.20
3.	1/3 to 2/3 Mission Lost	0.50
4.	2/3 to Nearly Total Mission Lost	0.80
5.	Essentially Total Mission Lost	0.975

Thus, spacecraft capability starts at 1.0 and remains there until occurrence of of the first anomaly, when it is assumed to degrade by exactly the percentage assigned to its mission effect category. If this value is designated D_1 , then at this point in time spacecraft capability is given by $(1 - D_1)$. Spacecraft capability is assumed to remain at this value until occurrence of the second anomaly with degradation D_2 . Spacecraft capability is then assumed to be given by the product $(1 - D_1)$ $(1 - D_2)$. In general, spacecraft capability

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upon the occurrence of the nth anomaly and remains at this level until the occurrence of anomaly n + 1. Plotting these results provides a highly visual indication of the degradation in spacecraft capability over time.

Integrating the resultant curve over the spacecraft's operating (or design) life and normalizing provides a single numeric representing average capability.

The procedure, while being easy to apply and useful in some applications, may not always provide an accurate portrayal of space-craft performance. It is the purpose of this subsection to examine four specific reasons why this might be so and to suggest an improved procedure suitable for general application.

(1) The criticality categories permit the possibility of large accumulated errors in the capability estimate particularly for accumulations of trivial anomalies.

This criticism is particularly apropos for complex, well-documented spacecraft. A case in point is NIMBUS-7, reported herein. It has accumulated 53 category 1 anomalies and 8 category 2 anomalies for a current estimated capability, using the current procedure, of

$$C = (0.975)^{53} (0.8)^8 = 0.044.$$

The spacecraft in fact is operating quite well in spite of its 61 anomalies, much better than the capability figures of 4.4 percent would imply. The solution to this problem lies in making a more accurate assessment of the mission impact of each anomaly and carefully tracking the cumulative impact of all anomalies. The latter is a good deal easier than the former. That is, determining the impact of each of the first ten NIMBUS-7 anomalies is probably at least ten times as difficult as

determining the state of NIMBUS-7 after the tenth anomaly. Careful application of these two approaches, however should adequately overcome this drawback.

(2) Assignment of anomalies to the categories is highly judgmental with no formal rules for making these assignments.

The informal rule for assigning anomalies to categories is to establish the overall effect on the mission as if the anomaly had occurred in isolation and at the beginning of the mission. Anomalies in redundant units take into account the degree of redundancy available upon their occurrence. Otherwise this approach does not include cumulative or cancelling effects of anomalies. While the assignments are judgmental, it is fairly easy to make the right assignment because the five categories are fairly broad and are tailored to the actual results observed in practice. Furthermore, there is no totally objective way to determine the impact of most anomalies. TV pictures or communications links that are degraded or fuzzy or intermittent, etc., are common anomalies for which this is true. Furthermore, the apparent objectivity inherent in "40 frames of data lost" or "2 transponders failed," etc., may be more illusory than real, requiring agreement that all frames/transponders are equal and so on. The impact of anomalies on scientific missions is generally even more subjective.

One approach to this problem might be to have an expert (or experts) assign the anomalies to their mission effect categories and justify each assignment, in writing, on the basis of all available information. It might also be possible for the expert(s) to prepare ground rules for anomaly classification and then to review the results for realism.

(3) The method for combining the effects of anomalies (i.e., as products), while mathematically advantageous, appears deficient in describing the performance.

The best way to determine how deficient this method is, is to compare its application with the actual curve. But if one had the actual curve there would be no need to apply the method at all. Thus, deriving an actual curve, or at least one approaching as closely as possible to the actual, would obviate this problem.

(4) No distinction is made between engineering performance and science performance.

Assume that each spacecraft can be rather neatly divided into two parts. One is the basic bus; the structure, power supply, attitude control, communications, thermal control, etc.; and the other is the payload, e.g., multi-spectral sensor, TV cameras, magnetometers, etc. Given this division, it would be of interest to know how well the bus was performing (engineering performance) and how well the payload was performing (science performance). It is entirely possible, of course, that under particular scenarios of redundancy, load sharing, and work-arounds that both bus and payload could be doing rather poorly while the mission itself was being accomplished quite satisfactorily. Thus, the distinction between engineering and science performance might best be drawn by making three evaluations upon the occurrence of each anomaly, i.e., its mission effect, its payload effect, and its effect on the bus.

An Improved Procedure

Combining these responses into an overall procedure would not only avoid the four drawbacks discussed above, but would also provide a generally superior way to assess spacecraft capability as a function of time. Specifically, the new procedure might consist of the following steps. (1) Assign "experts" to implement the procedure for each spacecraft or to review the results of more general practitioners. (2) Have the experts and/or practitioners gain familiarity with the total spacecraft design, mission, results, and anomalies. (3) Assign to each anomaly three cumulative degradation factors to the nearest percentage point, one for the mission, one for the payload, and one for the bus.* Since some anomalies have a degradation effect over time it will probably be useful in most cases to also assign cumulative degradation factors at some convenient time intervals such as every 1000 hours or every quarter. These assignments would be an evaluation by experts or practitioners of the cumulative capability lost at a given point in time for the total spacecraft, the bus, and the payload. (4) Provide a written justification for each assignment. (5) Plot the resultant curves and normalize as before.

^{*}Note that it may also be necessary to introduce a factor to account for self-healing and hence improvements in capability.

We, as practitioners, attempted to apply the procedures to SAGE (AEM-2), a fairly simple spacecraft with a fairly straightforward mission profile. The results were not encouraging. Estimating the actual impact of each anomaly has proven to be time consuming, difficult, and ultimately arbitrary in large part. This may be due simply to our lack of in-depth familiarity with the system and its mission. Real experts operating more nearly in real time might ease the process considerably and provide more accurate results.

Our attempt to implement the procedure is documented in Exhibit 11. The results for the mission are plotted in Exhibit 12 together with the results of applying the current methodology. It is assumed in both exhibits that the mission degradation is linear, going from 50 percent after the battery anomaly (2050 hours) to zero at the end of the mission (25,270 hours).

The proposed method gives an average capability over the space-craft's operating life of 54 percent; the current method yields 18 percent. The design life for SAGE is 12 months. Average capability over this period is 76% using the suggested method and 28% using the current method. The differences are clearly significant. How general this phenomenon is with respect to other spacecraft is unknown.

The improved procedure is obviously a good deal more time consuming than the current one. The difference is almost totally in the derivation of the three cumulative degradation factors together with the written justifications required by the improved procedure. In the current procedure this is a simple exercise in multiplication. While it will take some experience in the application of the improved method to

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<u> </u>	Time of Occurrence	Estimate of	Extinct of Cumulative Degradation (X)	RPURMANCE EVALUATION (X)	
	(Hours)	Payload	3	Mission	Reserks
	u	0	0	0	A longer than nominal time to deploy the S-band antenna does not degrade bus, psyload, or mission.
	u	0	~	o	Notter than normal base module temperature had no immediate payload or mission effect but contributed to the shortened battery life.
	\$	0	•	0	The higher than predicted scan wheel temperature had no payload or mission effect. Bus drifting further from nominal.
	900	•	•	0	Loss of one memory location has no payload or alssion effect but does further degrade the bus a bit.
	1,295	•	•	•	Initial frequency shifts in the S-band transmitter can be worked around to avoid mission degradation. The bus is again a bit further from mosimal.
	2,050	•	\$	20	The degraded battery capacity precluded many spacecraft operations. Continuing decline in battery capacity leads to complete failure at 25,270 hours.
	2,736	•	\$	25	The failure of the sun edge detector circuit had no mission effect because a suitable work-around was developed. It did not degrade the bus but the psyload is degraded on the order of 5 percent. Additional degradation shown in bus and mission capability is due to the earlier battery anomaly.
	8, 180	•	:	8	The degraded voltage limiter actually improved the bus a percentage point or so by preventing the dumping of excess shunt current into the battery. Continuing battery degradation of about 5 percent results in cumulative bus degradation of 4 percent. This assembly had no payload effect and no added mission effect. The continuing decline in battery capacity caused a further decline of 5 percent in mission capability, housever.
	7,100	~	\$:	Migher than normal attitude errors four passes result in no further degradation of poyload, bus or mission. The continuing battery decline is reflected in the bus and mission degradation factors.
	8 , 8 50	~	02	Ş	Abnormal variations in the horizon scan wheel are senther outgrowth of the battery problem. The bus is judged to be slightly more impacted than the mission.
	25,270	~	901	100	Mission termination is the end result of the battery anomaly (96).

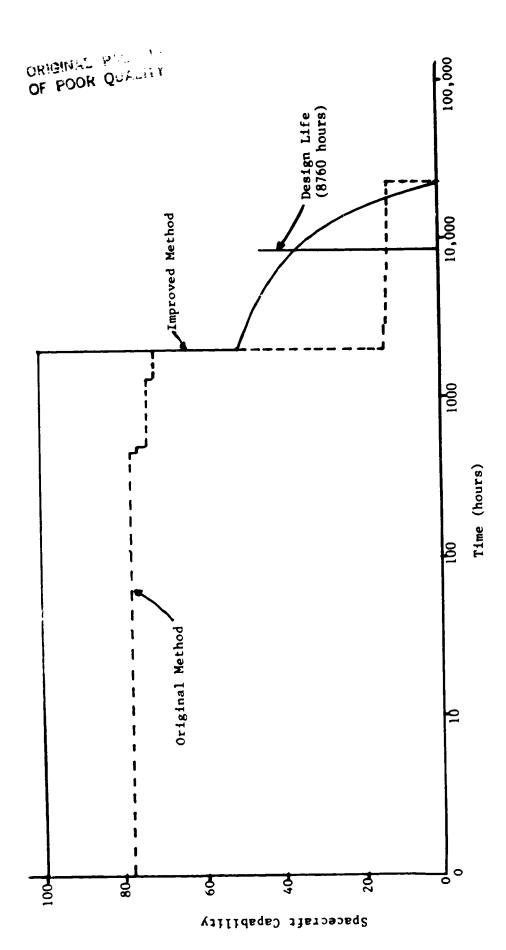


EXHIBIT 12 - SAGE CAPABILITY PLOTS

determine how long it would take, a rough estimate that seems reasonable to the authors is 15-30 minutes per anomaly, if the procedure is implemented at the time the EARs are generated or by someone who is already intimately familiar with the spacecraft, its mission, and its anomalies.

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APPENDIX A

DATA BANK COVERAGE FOR THIS UPDATE

APPENDIX A

DATA BANK COVERAGE FOR THIS UPDATE

The chart in this appendix lists the spacecraft for which information was added to the data bank by this study.

For each spacecraft, the chart shows the number of the engineering analyses report (EAR) that backs up the data in this report and gives an indication of the degree of completeness of the four major tables in the EAR. Information for Table III (parts counts by major components) was not actively sought in this study and that for Tables V and VI (developmental and prelaunch activities) varied from essentially none to fairly comprehsive. Information on developmental activities, however, was not generally available from those sources that provided the spacecraft operational data and a separate collection effort was not undertaken to seek information of this kind.

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MITBUS-7 MOAA-4 MOAA-5 MOAA-5 MOAA-B MOAA-7 SPE SPE-1 SPE-1 Complete Complete Complete Complete Complete SPE-1 SPE-1 Complete VIKING ORBITEN-1 Complete VIKING ORBITEN-1 Complete VIKING LANDER-1 Complete VIKING LANDER-2 Complete VIKING LANDER-2 Complete VIKING LANDER-2 Complete	3	Complete
MOAA-4 Complete MOAA-5 Complete MOAA-5 Complete MOAA-3 Complete MOAA-3 Complete MOAA-3 Complete MOAA-3 Complete MOAA-2 Complete MOAA-2 Complete MOAA-3 M	;	Complete
MOAA-5 MOAA-6 MOAA-8 MOAA-8 MOAA-7 MOAA-7 MOAA-7 MOAA-7 MOAA-7 MOAA-7 MOAA-7 MOAA-7 MOAA-8 MOAA-8 MOAA-8 MOAA-8 MOAA-8 MOAA-8 MOAA-9 MOAA-8 MOAA-8 MOAA-8 MOAA-9 MOAA-8 MOAA-9 MOAB-1 MO	61; 1982 update in this EAR	Complete
MOAA-6 MOAA-7 MOAA-7 MOAA-7 MOAA-7 MOAA-8 MOAA-7 MOAA-8 MOAA-7 MOAA-8 MOAA-8 MOAA-8 MOAA-9 MOAA-9 MOAB-6 MO	61; 1962 update in this EAK	Complete
MOAA-B Complete MOAA-7 Complete SMH Complete SMS-1 Complete SMS-2 Complete SMS-2 Complete SMS-1 Complete VIKING OMBITEN-1 Complete VIKING OMBITEN-1 Complete VIKING OMBITEN-1 Complete VIKING OMBITEN-2 Complete	Complete Not Applicable	Not Applicable
MCAA-7 Complete Spéi Complete SPS-1 Complete SPS-2 Complete SPS-3 Complete SPS-3 Complete SPS-4 Complete SPS-5 Complete VIKING ORBITEN-1 Complete VIKING ORBITEN-1 Complete VIKING ORBITEN-2 Complete	منواسي	
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APPENDIX B

BASIC DATA TABULATIONS

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APPENDIX B

BASIC DATA TABULATIONS

This appendix is divided into three tabulations. Appendix B-1 summarizes each anomaly in the update. Appendix B-2 contains classification codes for each anomaly using the "standard" approach applied to all previous collections. Appendix B-3 contains additional classification codes applied in this study. Sections III.A and III.B in the main body of this report define the various codes and discuss their application to the spacecraft anomalies. For convenience, the identification of the anomaly characteristics and the alpha-numeric codes employed are repeated just prior to the two tabulations of Appendices B-2 and B-3.

Appendix B-1 contains, in tabular form, the primary data upon which this report is based. All 606 satellite anomalies are listed by spacecraft, in order of elapsed time to occurrence and contain these data elements:

- Time-to-occurrence of anomaly in hours. A time t is associated with the launch interval, prior to injection into orbit. The symbol denotes either unknown time or intermittent occurrence.
- o Three short phrases indicating the description of the observed anomaly, its suspected or known cause, and the effect on the mission objective(s).
- o Corrective actions, both in-orbit or for subsequent launches, if known.
- o Brief remarks, if needed to place the anomalous incident in context.

The sequential coding index of column 1 provides a means of crossreferencing to the classification codes of Appendix B-2 and B-3. These two
appendices should facilitate any further classification or analysis the
reader might wish to undertake.

Appendix B-1 begins on Page 83, Appendix B-2 on Page 155, and B-3 on page 175. A list of acronyms used in the anomaly summaries and their definition follows for the convenience of the reader.

ACS Attitude Control System AGC Attitude Gain Control APU Auxiliary Processing Unit **AVHRR** Advanced Very High Resolution Radiometer **BCS** Bent Crystal Spectrometer BOT Beginning of Tape C& DH Command and Data Handling CDA Command and Data Acquisition CDIU Command and Data Interface Unit CIU Controls Interface Unit COMSTOR Command Storage Module C/P Coronagraph/Spectrometer CPU Central Processing Unit CTU Central Telemetry Unit **CZCS** Coastal Zone Color Scanner DAPU Data Acquisition and Processing Unit **DCPR** Data Collection Platform Receiver DCS Data Collection System DDP Digital Data Processor DIP Digital Information Processor DSAS Digital Solar Aspect Sensor DTR Digital Tape Recorder **ECAM** ERTS Command Auxiliary Memory ERB Earth Radiation Budget ESA Earch Sensor Assembly **ESMR** Electrically Scanning Microwave Radiometer **FCS** Flat Crystal Spectrometer **GCMS** Gas Chromatograph Mass Spectrometer **GEODAT** Software HAO High Altitude Observatory **HDRSS** High Data Rate Storage System **HEPAD** High Energy Particle Detector HET High Energy Telescope HIRS High Resolution Infrared Sounder HRIR High Resolution Infrared Radiometer IDC Image Dissector Camera IMU Inertial Measurement Unit LAPI Low Altitude Plasma Experiment LIMS Limb Infrared Monitoring of the Stratosphere LSAD Left Solar Array Drive LVDT Linear Voltage Differential Transformer

Multispectral Scanner

Microwave Scanner Unit

MSS

MSU

NBTR	Narrow Band Tape Recorder
NEMS	Nimbus-E Microwave Spectrometer
OAS	Orbit Adjust System
OBC	On-Board Computer
PAS	Panoramic Altitude Sensor
PCL	Program Control Logic
PCM	Power Control Module
PCS	Pointing Control System
PMT	Photomultiplier Tube
RBV	Return Beam Vidicon
RCS	Reaction Control System
RIU	Remote Interface Units
RM P	Rate Measuring Package
RTG	Radioisotope Thermoelectric Generator
RVDT	Rotary Variable Differential Transformer
SAD	Solar Array Drive
SAM II	Stratospheric Aerosol Measurement II
SAMS	Stratospheric and Mesopheric Sounder
SAR	Synthetic Aperture Radar
SASS	Scatterometer
SBUV	Solar Backscatter Ultraviolet Energy
SEM	Space Environment Monitor
SIRS	Satellite Infrared Spectrometer
SMART	Housekeeping Software Scanning Multichannel Microwave Radiometer
SMMR SNR	Signal to Noise Ratio
SR	Scanning Radiometer
SRR	Scanning Radiometer Recorder
SSCA	Surface Sampler Control Assembly
SSU	Stratospheric Sounding Unit
TCE	Thermal Control Electronics
TED	Total Energy Detector
THIR	Temperature/Humidity Infrared Radiometer
TIP	Tiros Information Processor
TOMS	Total Ozone Mapping Spectrometer
TWERLE	Tropical Winds Energy Conversion Reference Level
	Experiment
TWTA	TWT Amplifier
VAS	Visable Infrared Spin Scan Radiometer Atmospheric
	Sounder
VEFI	Vector Electric Field Instrument
VHRR	Very High Resolution Radiometer
VIP	Versatile Information Processor
VIRR	Visable and Infrared Radiometer
VISSR	Visable Infrared Spin Scan Radiometer Vertical Temperature Profile Radiometer
VTPR	AGILICAL TEMPETATE TINITIE WORTOMETET
WBVTR	Wide Band Video Tape Recorder
WEFAX	A Satellite Weather Facsimile System

APPENDIX B-1

ANOMALY SUMMARIES

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Remarks		ORIGINAL OF POOR	PAGE	111	problem cleared itself and experiment operated normally after about 3% days.	After about 20,000 hours the experiment returned to normal.	Problem went away by itself after about a week.	iroblem resulted from an attempted to pro- long battery life on AR-5 relative to AE-3 and 4.
(orrective Action (if known)		Loaded zeros in memory locations subject to garbling and restricted use of torquer coils to two at any one time.	Changed command routines to obtain compatibility with thrusters.	When the shunt limiter trips, it is commanded back on.				
Mission Effect		Minimal effect due to corrective action.	Minimal effect.	Minimal effect.	Ninmal effect	Some loss of data from one of 12 experiments.	Effect minimal aithough it caused the pitch loop to lose lock and allow the spaceraft body to rotate.	Loss of 4-5 minutes of data out of a 96 minute sequence when the problem occurs.
Cause		Suspect proximity of forquer coils to programmer-to-memory harness qurbles memory address. Exact mechanism unknown.	Quality control.	link nown .	Attributed to temporary short in temporary short in ton extraction lens.	Cause unknown.	Cause urknown.	lestan problem.
Description	AE-5	Memory contents changed after loading and verification. Garbling occurs in both memory units after operation of all four torquer colls.	Thruster control harneys connections in error.	Shint limiter #1 occasionally trips for no apparent reason.	Ion repeller current in neutral atmosphere composition experiment increased slightly and data output counts decreased.	Rackscatter ultraviolet spectrometer ceased operation.	Noisy wheel horizon sensor data occurred intermittently.	Numerous under voltage shifted of the states raft for until an intermittent by.
Time (Nours)			•		۶ ۵ ۰	13,245	41, 760	
Index		~	~	-	•	•	£	•

OF POOR QUALITY

1	Nemal A										
Corrective Action	(1f known)			Design modified for next spacecraft in the series (SAGE).	Design modified for next sparecraft in the series (SAGE).		Operational work-around	rus.	e- Slight doction, inds of mination		not
	Mission Effect		No mission effect.	Minimal impact since spacecraft op- erates in real time.	No effect, possibility of sport rous commands but operational but a sound	developed to	No effect.	Slight impact; oscillator needs to be warmed up before achieving stable status	No effect on space- craft operation. Slight ampart on data reduction, causing brief periods of loss of yaw determination accuracy	A) Blaston offect.	Minimal offect; did not
	(ause)		thereway, but it could be a shift in the set point on the termwetry.	Design problem.	Dealdn problem.		læstyn problem.	Pesign problem.	Possibly due to paor workmanship.	Quality problem. Not a flight worthy device.	spurrous community possibly due to cross talk in the harmws.
	क्षता हिंदी अले	AFM-, (HEFM)	The heat capacity mission radiometer parch remains the controls at 11. K trakend of 115 K	The clock frame count and word count were	cross-talk in harness.		Telemetry frame counter, frame Lough hold register, takes on an arbitrary state when powered.	Stop/abiffs in frequency of s-band transmitter.	Sun sensor reticle loses low sun andles, i.e., loses most significant bits.	The platinum sensor (relemetry point) on the array: x public opens at o 'or	The space tall word not not be recovered and the Sattery over tall to be any control of the sattery over the major of our control of the sattery over the major of our control of the sattery over the sattery over the sattery of the
>	(Sanou)				-					011	ē.
	Index		-	٠.	-		▼	•	Æ	•	2

Anomalaes

Remarks		Similar batteries on SAGE launched subsequent to this anomaly.									
COFFECTIVE ACTION (11 Known)		problem persisted in spite of operational work-arounds, 1.e., cycliffy loa's and the battery, etc.		Attempted work-arounds to no avail.					٠		1011
Mission Effect		Significant reduction in science data collection.	small effect since ground work-around developed to compensate for yaw and servers.	Loss of 8-band and instrument operation.	No mission effect.	No mission effect.		No effect.	contributed to shortened battery life, etc.	No mission effect.	No offect; memory location and used.
-Native		cadmium migration in the battery cells.	Possibly due to foreign matter in the lubricant.	Spacecraft power problems.	Attributed to MFI in some geographical regions.	Unknown.		Coaxial Cable slowed deployment due to low temperature stiffness.	Attributed to design (thermal analysis) but specific ellor unknown.	Design effor in medeling absorbed surlight on panels.	tage design errer.
De service tons	APM-1 (HCCPM)	Battery temperature increased necessitating reduced charge levels.	The momentum compensation major of the heat capacity majorin reli-capacity from the complete to the control of the complete to the control of the complete the co	Long clock stops.	Clock resect counter advances between mome passes.	The heat capacity mapping radiometer croler housing and cone run lest cool with drot closed and heater on.	AEM-2 (SAGE)	S-band antenna required 40 minutes to completely deploy.	Dase module temperature tuns hotter than than predictes.	Scan wheel temperature rose well above predicted.	command stored in memory location and oxecutors when
Anomaly Time (Nours)		0 ! : . 4		14,485	,			-		\$	Çi P
H approximately and the second		,	3		2	ī.		cel	·•	~	•

Remarks					Fortuitous Decause degradation matched the degraded power levels caused by the battery anomaly (it grevented dusping excess shunt current into the battery).		
(orrective Action (if known)				Work-around developed using science detector.			
Mission Effect		No mission effect transmitter commanded on to stabilize before data transmission.	Significant impact. typerating voltage reduced from 30 to 20 volts. Led to command and attifude control problems and increasing loss of experiment data.	No mission c'fect.	No added mission effect.	No mission offect; did not recut.	No stanificant effect.
		Design problem; crystal oscillator requires	Attributed to cadmium migration; exacerbated by thermal control problem.	Due to failure of sun edge detector circuit.	Unknown sause.	law wiltage spikes on the AS power supply for unknown reason.	Combination of Stanceraft when problems and sun interferences.
•	AEM-2 (SAUF)	S-band transmitter frequency shifts after turn on.	Battery capacity degraded; stace- craft went into under voltage condition.	Instrument scan head went into stops instead of reversing scan at sun edge (did not sense sun edge).	Voltage limiter degraded.	Four passes with magicer than mormal artitude crace and wheel activity.	Horizon sensor Scan wheel had absormal speed variations.
	Index (bours)	1,245	o <o':< td=""><td>3,750</td><td>5, 180</td><td>7,100</td><td>850</td></o':<>	3,750	5, 180	7,100	850
	Index	•	٤	•	œ	?	o 1

					O	F POOF	≀ Q	UAL	ITY					
Restarks													End of life tests indicated that the switch might be erratic.	
Carrective Action (if known)														
Mi gon Effect		Institutionant space- craft has been operating off Vapor tressure.	Instagnationants	Instanticant, stationkeeping still possible.	Significant, not enough process to support C-band operations.	Stigntfoenty not enough power to suggest C-band operations.		Small effect.	Small effect.	Stant ant; not enough power to support (-band operations.	Stanificant; not enough jament to support C-band operations.		Stanificants C-band Ismer loss.	Small, are as demand than
a series		Uskraden.	Thik nowin .	Briknown .	Unk namen .	Unk nown .		Unknown,	thik cown .	Unknown .	Unit rown .		Day to design.	Consed by Large of posterior
mole franseag	APS-1	Propellant was lost doring the first echipse.	A number of false ownersted.	Cactinued drop in imported services of stationkeeping system 2.	Some buttery degradation.	Some array degradation.	ATS-1	Some portions of C-band have failed.	Control gas has been depleted.	Some array degradation.	Scale battery degradation.	ATS-5	MF leakage through the cribbon antenna select switch causes M jewer loss.	Array strabily stancest
Time Index (boars)			÷.	17 () Vie	·	,		,		•	,		1,850	26., 3000
Trokes			~,	-	4	∞		*	~	•	7		-	٠.

Resorks			The shutter was not designed for a spinner and its shutter actuator could not overcome the force of the spin.							Anomaly first in a series of propulation/ thruster problems; initially mediatible impacts but later, hackup and work- around approaches luss
(Orrective Action										
Massion Effect		Negligible.	No import; tolevision not used as planned because the spacecraft was symming.	No effect.	No effect.	No effect.	No effect.	Small.	Negligible.	Ned It gible.
Detroit.		linknown,	Due to spin of the spacecraft.	Possibly caused by partial failure of the battery.	Caused by solar array damage from aprige engine elect.	Possibly due to ading.	Unk nown.	Probably due to ayiny.	Unknown.	Due to proprilant ferd blockage.
D. Scrift ion	ATS-5	L-band TMT * (failed.	Television camera vstem sub-shotter not operative.	Undervoltage condition on Battery \$1 during end of life tests.	Telemetry readings from power bus 82 fluctuated during end of life tests.	End of life tests indicated that A to D converter components may have changed values.	End of life tests indicated that array degredation was IM greater than predicted.	Insufficient battery capacity to carry C-band operations through eclipse.	Morth solar array lost 20 watts capability.	Fullure of SPS-c megative yaw jet #11.
Anomaly Time (hours)		34,140	0¥0 **	99,450	44,700	94, 700	44,700	,	08.2,71	21,470
In.		-	7	\$	£	^	70	ø	-	~

									744			
Remarks		See anomaly #2.	See anomaly #2.	See anomaly 62.				See ancealy \$2.	See anomaly #2.	See anomaly 62.	See anomaly 62.	See anomaly #2.
Corrective Action (if known)												
Mission Effect		Negligible.	Negligible.	Negligible.	Loss of a portion of the EME measurements.	Negligible.	Negligible.	Negligible.	Negligible.	Megligible.	Megligible.	Negligible.
Cause		Due to propellant feed blockage.	Due to propellant feed blockage.	Due to propellant feed blockage.	Unknown.	Due to propellant feed blockage.	Unknown.	Due to propellant feed blockage.	Sue to propellant feed blockage.	Due to propellant feed blockage.	Due to propellant feed blockage.	Due to propellant feed blockage.
Description	ATS-6	Failure of SPS-2 negative roll jet 89.	Low initial impulse pulses on positive pitch jet 812 (SPS-2).	SPS-2 negative roll jet #9 leaked for about a day.	Complete failure of Environmental Measurementa Experiment, Auroral Particles.	Less than nominal firing parformance of SPS-2 positive pitch jet #2 and later degraded further.	Unexpected variances in spacecraft IF ACC calibrations.	SPS-1 negative roll jet 81 stuck partially open for about five minutes after it was commanded to close.	SPS-1 positive pitch jet 44 was found to be inoperative.	Less than nominal performance from SPS-2 negative pitch jet 811; later returned to normal.	Lass than nominal performance from SPS-2 positive roll jet #10.	SPS-1 negative yaw jet Me was found to be remainfuly insignation.
Time (hours)		23,880	23,880	24,816	25,920	27, 384	27, 390	30,240	31,704	32,040	32,164	34, 176
Index		•	•	•	•	^	•	•	91	=	21	2

ORIGINAL PRODUCTY

					OR OF	iginal Pool	PA R QI	GE JALI	is ry		
Remarks		See anomaly #2.	See anomaly #2.	See anomaly \$2.				See anomaly #2.			
Corrective Action (if known)											
Mission Effect		Negligible	Negligible.	Negligible.	Some loss of telemetry data.	Some loss of tempera- ture telemetry data.	Negligible.	Negligible.	No impact on mission; mission was over at this point.	Not serious.	Not serious.
Cause		Due to propellant feed blockage.	Due to propellant feed blockage.	Due to propellant feed blockage.	Most likely cause is an intermittent in the multi-layer printed circuit board.	Attributed to long- term cycling in orbit.	Due to propellant feed blockage.	Due to propellant feed blockage.	Unknown.	Attributed to noise transients.	Unknown.
Description	ATS-6	SPS-1 negative roll jet 81 remained firing for about weven times longer than normal.	Degraded thrust level from SPS-2 eastward back-up orbit control jet 016.	Degraded thrust level from SPS-2 eastward prime orbit control jet #15; later failed to fire.	Intermittent telemetry data from DACU-2 analog channels with the number of effected channels progressing with time.	Many external thermistors had become erratic.	SPS-1 negative roll jet 01 failed to fire.	SPS-1 positive yaw jet #5 failed to fire.	One frequency channel of the interferometer failed during end of life tests.	During end of life tests, it was found that the Polaris tracker still inter- fered with the earth sensor.	Slight increase in reaction wheel friction and windage torque were noted during end of life
Anomaly Time (bours)		35,088	37,920	38,256	43, 296	44,232	44,856	44, 856	45,000	45,000	45,000
1		4	15	91		8	61	20	12	≈	ε

Remarks		Caused "squinting" of the RF boresight off the spaceraft	Subsided after the first 24 years in orbit.	ORK OF
Corrective Action (if known)				
Mission Effect		Insignificant.	Insignificant.	Insignificant.
Cpuse		Unknown .	Unknown.	Due to degradation of the second surface mirrors (optical solar reflectors) that cover the reservoir's radiation.
Description	ATS-6	Diurnal variations in reflector temperature gradients produced reflector distortions.	Heat pipe thermal diode exhibited some apparent non-condensible gas generation.	Heat pipe gas reservoir ran hotter than nominal.
Anomaly Time Index (hours)		•	,	•
Index		7	\$	%

Remarks					orig of I	INAL PA	ge is Jality		
Corrective Action (if known)		The horizon scanner "on" command was placed into memory to be executed after transmitter turned off.	Software wes coprogrammed to invert and yet the correct bit pattern.					Work-around developed to reinitialize the memory at each power on.	
Masson Effect		No effect due to work- cround.	Negligible	No impact on mission.	No effect; telemetry data indicated cover did not deploy; experimental data prowed that it did.	No effect; telemetry data indicated loop did not deploy; experimental data proved that it did.	No effect; did not recur.	Negligible.	No mission effect; did not recur.
Cause		Due to coupling between two command lines.	The cause was a design error in that the documentation supplied by the manufacture contained incorrect telemetry format.	Suspected to be due to RFI.	Unk nown.	Unknown.	Unknown, but telemetry data indicate the receiver locked.	Unk nown.	Attributed to bit value change in the stored command,
Description	1-30	Horizon sensor erroneously tuins off when transmitter turns off.	Telemetered data from sun sensor inverted (i.e., l's ind O's interchanged).	Transponder failed to turn off after uplink carrier dropped.	Sensok cover telemetry incorrect.	Plasma wave loop deployment telemetry incorrect.	Transponder down link carrier was on prior to scheduled ground station acquisition (it should have been off).	The memory in the retarding ion mass spectrometer dumped prior to power off. After power off and on again, memory contents had been changed in two positions.	The command in memory location 543 executed 68 minutes early.
Anomaly Time (hours)		u	u	740	364	637	**	O ee ee	1,720
Index		٦	~	m	•	'n	v	r	co

Research K.				The identical power supply also failed on the low altitude plasma indicator of the DE-2 spacecraft.		Drift is 407 milli- seconds per day. DE-2 clock also drifts excessively.	"Mits" seem random geographically. Has happened on eight occasions.
Corrective Action (if known)							. 6.2 0
Mission Effect		Negligible effect; subcarrier returned after some on/off commands transmitted. Problem did not recur.	No effect; command canceled.	Loss of perhaps 10 percent of mission data, and two-thirds of the high altitude plasma data.	Little mission effect; temperatures controlled to within limits by operational work-arounds.	Negligible due to periodic GMT adjustments.	Some lost and incorrect telemetry data.
Cause		Unknown.	Unknown.	Probable cause is voltage break at one or more of several capacitors or an insulation break-	Transistor failure in associated amplifier.	Unknown.	Radiation "hits" impinging space- craft clock, etc.
Description	1-3	Loss of transponder sub- carrier.	A command which is not used in the speceraft was found in memory. No record exists of loading such a command.	The high voltage power supply failed on the high altitude plasma indicator.	The lower of one of six active thermal control units opened fully rather than as required to maintain temperature.	Excessive .ock drift.	Numerous glitches in spacecraft operation. E.g., unexplained 7 to 10 watt power increas, on spacecraft bus; apparent loss of a micro-processor in the command and telemetry processor.
Anomaly Time (bours)		2,075	2,177	2,860	5, 135	9.890	• 000
Index		•	01	ជ	21	13	*

	Remarks								
Corrective Action	(if known)					Work-around developed; either disable ranging or transmit uplink ranging tones.	Conversion algorithm modified. When gain shifted again, horizon sensor data used more extensively for attitude determination.	At each occurrence the damper loop is commanded closed again.	Work-around developed.
	Mission Effect		VEFI is one of 9 experiments on the spacecraft. It suffered significant loss since no direct measurements of eastwest electric field were possible.	Until 840 hours science operation was cut back approximately 10 percent. At 80 hours the problem dis- appeared and did not recur.	Negligible, work-around is straightforward.	Makes command verification difficult.	Negligible.	Causes minor perturbations in attitude.	Not serious.
	Cause		Attributed to an open in the power circuit since no motor current shown on telemetry whereas other parameters were normal.	Caused by short in charge controller summing point to signal ground.	Unknown.	Unk nown .	Unknown.	Noise spikes during on board computation of roll angle adversely influence the pitch control electronics.	Due to noise coupling which causes the ACS to "think" it must correct an ittitude error.
	Description	<u>DE-2</u>	Z-antenna for the vector electric field instrument (VEFI) did not deploy.	One of two battery charges does not correctly control charge; protective circuity disconnects the charges.	Malfunction in one segment of the Retarding Potential Analyzer Memory.	Telemetry downlink noisy when ranging enabled and no uplink ranging tones being sent.	Fine sun sensor beta electronics changed gain and bias setting.	Nutation damper loop opens erratically and recurrently wis automatic disconnect.	Spacecraft body is offset by about 0.4* whenever the trans- pxnder turns on.
Anos + ly Time	(hours)		u	u	02	*	4 50	795	1,430
	Index		~	~	m	•	'n	ø	r

	Remarks			Identical power supply also failed on the high altitude plasma instrument on the DE-1 spacecraft.	DE-1 clock also drifts excessively.		-	Occurred once again two months later.		
Corrective Action	(if known)									Switched to VHF transmitter #2 and used 8-band system as a backup.
	Mission Effect		Significant reduction in low altitude plasma instrument data. Lesser impact on vector electric field instrument. (Two of 9 experiments)	Loss of 4 the experiment's sensors. Not much additional degradation beyond that caused by anomaly 8. LAP1 is one of 9 experiments.	Negligible due to periodic GMT adjustments.		No effect since redundant subsystem used.	Negligible effect.	Loss of perhaps 20 percent of total spacecraft capability.	Command capability lost lost for three days.
	Cause		Unk nown .	Unknown .	Unknown.		Unknown	Unknown	Unknown	Unknown
	Description	<u>DE-2</u>	loss of telemetry enable pulse for encoding and transferring digital data.	High voltage power supply for the low altitude plasma instrument (LAPI) failed.	Excessive clock drift; approximately 130 milliseconds per day.	GOES 1	One side of the telemetry subsystem failed.	Visible/infrared spin scan radiometer hung up temporarily.	Infrared data from the visible/infrared spin scan radiometer lost intermittently for about a year from anomaly time, then lost completely.	Spacecraft cannot be commanded when VHF transmitter #1 is on.
Anomaly	Time (hours)		3,400	5, 300	068 '9		22,410	26,560	30, 120	56,976
	Index		∞	o ∙	01		-	~	m	•

Remarks							Anomaly discovered during spacecraft tests.				Somewhat less than one year later side I was found to be healthy and was used again.
Corrective Action											
Mission Effect		Insignificant.		Degraded operation of the VISSR.	No effect due to redundancy.	Total loss of visible and infrared data.	Degraded operation of the VISSR, but no additional mission degradation because both VISSR encoders failed previously.	Negligible; redundant side of S-band sub- system utilized.	Negligible mission effect.	Minor loss of space environment monitoring data.	Megligible due to redundancy: side 2 was used.
Cause		Unkriown.		Unknown .	Unknown.	Unknown.	Unknown .	Unknown.	Unknown.	Unknown.	Unk nown .
Description	GOES-1	One solar array temperature sensor failed,	COES-2	Photomultiplier tube #1 failed in the visible/infrared spin scen radiometer (VISSR).	Encoder in the VISSR failed.	Second (redundant) and infrared data.	Fhotomultiplier tube #4 failed in the visible/infrared spin scan radiometer (VISSR).	One side of the S-band subsystem exhibited 5 to 8 MHz frequency shift.	X-ray reference voltage telemetry point failed.	One channel of energetic particle sensor noisy sance launch.	One side of the attitude determination and control subsystem failed.
Ancmaly Time (hours)		,		8, 760	13, 200	14,130	20,850	38,110	,	ω	1,870
Index		s		7	~	•	•	vo	v	-	N

Nees rks		Officially declared "degraded" 7000 hours later.				Problem went away three weeks later.	Problem later went away.	Viss officially declared a failure at approximately 35,000 hours; the speceraft was then placed on
Corrective Action (if known)								
Mission Effect		Significant and increasing data loss.	Some degradation of VISSR operation.	Apparently minor.	Not too serious since primary encoder still available but "roll down" of expanded frame was no longer possible.	Minimal effect.	Negligible, since earth sensor #1 was used.	Loss of all experiment data by 23,800 hours on orbit.
Cause		Lubricant build up in VISSR.	Unknown.	Unk nown .	Unk nown .	VISSR torque anomaly of undetermined nature.	Unk nown .	Dur to degrading encoder bulb.
Description	[-S200	Increasingly severe line loss in the visible/in- frated spin scan radiometer (VISSR).	Intermittent mirror mtepping in the visible/infrared spin scan radiometer (VISSR).	The solar x-ray monitor position read out and stepper operated intermittently.	Back up encoder for the visible/infrared spin scan radiometer failed.	Visible/infrared spin scan radiometer (VISSR) full disk pictures stopped at approximately 1810 lines and expanded frame made lost.	Nigh bit error rates and degraded picture when earth sensor 82 used.	Hang ups in the primary encoder for the visible/ infrared spin scan radiometer (VISSR) becoming progressively
Aronaly Time (hours)		3, %0	8,610	098.	10,920	14,040	17,640	19,480
Index		.	•	•	٠	•	•	•

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Remarks				No effect during early portion of spacecraft life but misalignment is superted to increase as fuel is depleted; therefore VAS images must be corrected.		ORIGIN OF PO		GE IS ALITY	
Corrective Action (if known)		Ground work-around developed to eliminate the resulting gap in use data.			Design changed for GOES 5.		Problem corrected on future GOES.		
Mission Effect		Not serious.	Insignificant.	Negligible.	Small; engine fired at 2nd apoque instead of third successful action.	Small: batteries subsequently starting charging but it took 5% hours to charge.	System must be operated in sun reference mode to obtain SEM K-ray data.	Not serious.	Not serious.
Cause		Unknown.	Unk nown .	Design defect; spacecraft imbalance.	Attributed to thermal design.	Unknown .	Due to workmenship.	Unk nown .	Unk nown.
Description	(30 0 55 - 3	Photomultiplier tube 84 failed in the visible/ infrared spin scan radiomater.	One solar array temperature sensor failed.	0.54" miselignment between spacecraft body axis and spin axis.	Apogee engine temperature started dropping unexpectedly.	Battery voltage did not increase when apace- craft first entered sunlight post-launch.	ELEM x-ray sensor does not function in earth sensor reference mode.	SFM x-ray positioner telemetry indicates ± 0.5° error when x-ray is stepped by increments of 1 or 2 steps.	Command decoder 01 intermittently failed to accept commands when cold (post eclipse) if command tone modulation exceeded
Ancesty Time (hours)		20,590		J	u	u	.	•	•
Index		"	11	-	~	~	•	•	٠

							ORIGI OF P	NAL I	PAGE Mal	is !Ty			
	Nemarks		Problem can be eliminated by adjustment to ground equipment.		Qualification temperatures re- defined post launch.		VAS and antenna pointing elightly affected during switch over.	Transmitter has not been powered since failure.		Occurred three times.	Continual problem on GOES.	Mas occurred 22 times.	
Corrective Action	(1f known)												Pads installed on GOES 5 and F.
	Mission Effect		Negligible.	No impact.	No impact.	Not significant.	Negligible.	Megligible; switched to transmitter #2.	Significant; loss of MEPAD data.	Negligible; RCS operational procedures modified and performance normal.	Significant, VAS encoder must be cuntinually powered which precludes use on ground of automatic control functions.	Small, often disrupts VAS operation.	Insignificant; used (MF receiver #2.
	Cause		Unknown.	Attributed to design.	Thermal design problem.	Unknown.	Acuracy effor.	Attributed to design, perts, workmanship, materials.	Attributed to part failure.	Probably due to a heat soak back problem.	Lubricant too thick.	Attributed to static discharge or floating ground.	Attributed to design.
	Description	\$-S205	PCM modulation in- terference with IRIG-B real time data.	Banding in VAS IX images during eclipse season.	S-band transmitter 2B temperature dropped to -28.5°C. during eclipse.	Magnetometer boom deploy telemetry point failed.	Design control slightly affected when switching from earth sensor to sun sensor reference mode.	S-band transmitter #1 feiled.	SEMS NEPAD solid state detector failed.	Thrust delivered by radial thrusters #1 and #2 considerably less than nominal.	Excessive VAS encoder torque buildup due to excessive lubricant.	Spurious/phantom commands change VAS configuration.	UNI Roceiver #1 (DCPR) failed.
Anomaly Time	(hours)		J	u	u	J	u	1,700	2, 320	3, 330	, 600 , 4	4,800	5,250
	Index		,	•	•	01	=	2	2	5	21	9	11

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1						OF	PO	OR	QUALI	TY		
Benarks	•	Condition lasts about 10 minutes and returns to normal.		Voyager used same translators and had similar problem.	Mas recurred several times, both pre - and post eclipse and returns to normal following ground commands.				Correlates with high investible solar particle event.			
Corrective Action (if known)												
Mission Effect		Not significant.	Insignificant, used alternate CTU but lost 65 minutes of SEM data.	No impact.	Insignificant; returns to normal.	No impact; temperature did not reach critical point.	Insignificant; commanded back to normal.	Significant; loss of magnetometer data.	Significant, not known whether effect will be permanent.	No impact on mission.	No impact.	No impect.
Cause		Possibly due to external 5-band source.	Possibly due to random part failure.	Possibly due to thick film resistor or translators.	Unknown.	Unknown.	Unknown.	Unknown.	Unknown.	Due to plume impingement on despin antenna.	Unknown.	Unknown.
Description	COES-4	S-band DCPR SNR increases about 20db daily.	Central Telemetry Unit (CTU) 81 failed.	S-band transmitter #2 downlink power de- creasing.	Abrupt loss of MF output from DCPR transmitter prior to eclipse.	Despin bearing assembly temperature aucesds predicted winter max of 32°C.	Central Telemetry Unit 82 reset 1tself.	SEMS magnetometer Hp axis failure.	Solar array output dropped abruptly (0.5%, 80mA)	Spin axis precesses during continuous axial jet firing.	2db ripple in DCPR passband.	CDA telematry transmitter #1 output decreased from 3.3 to 1.8 watts.
Anomaly Time (hours)		\$, 300*	069'9	€, 500	8, 590	10.600	13,700	11,900	15,400	,	,	,
Inches		81	61	90	2	2	2	*	\$	2	27	e 7

	Rission Ellect		Not serious.	Not serious.	Not serious.	Significant; loss of data.		Small; deployed cover early and had 14 days instead of planned 17 days to outgas spacecraft.	to Megligible; normal operation restored.	tic Small, commands sent to reset PMT.	Small; loss of house- keeping data point.	Small; loss of house- keeping data point.	Small; loss of picture data until commanded to normal.	Significant: VAS visible pictures badly striped and causes loss of visible images when anomaly occurs.
į	Cause		Unknown.	Unknown.	Unknown.	Unknown.		Unknown.	Problem isolated to specific circuit.	Attributed to static discharge.	Unknown.	Unknown.	Probably due to conflict between timing and frame mize logic.	Unknown.
	Description	COES-4	Battery 81 charge current telemetry does not respond when transitioning from charge to discharge.	UMP transmitter output higher than expected.	VAS mirror did not stop at line 001.	five telemetry points are anomalous.	2-3300	VAS radiation cooler cover temperature rising slightly faster than predicted.	All CTU #2 digital analog data invalid.	Phantom commands change VAS PMT channel 7 gain.	Demodulator 01 aquelch/unaquelch telemetry point falled,	MCS Fuel Tank pressure telemetry inoperative.	During normal frame aire command, VAS scan airer reversed its direction but failed to stop at the Morth limit.	Shift in responsivity of 3 of 8 VAS visible detectors during eclipse season.
	D880	8	Batter teleme respon from o	UNIT ts	VAS =	rive Fr		VAS COM T15	117 5	A SAV	2 2 3	23		3 m 6
	(hours) Desci	81	telese telese respon	. UNF tr higher	VAS =	Five .		c VAS COW Fibal That	575 A11	2.350 ⁺ Pha	3,090 Dem	4, 120 RCS	6,910 Dual Baland Balan	7,510 Shi 3 o det ecl

Corrective Action Nearks											
Corrective A (if known)											
Mission Effect		Negligible, used CTU #2.	Significant, not known whether effect will be significant.	Not serious.	Negligible, does not effect SEMS operation.	No effect.	Not serious.	Not serious.	Not serious.	Not serious.	No impact.
Ceuse		Unknown.	Due to high level solar particle event.	Unknown.	Unknown.	Unknown.	Unknown.	Unknown.	Unknown.	Unknown.	Due to jet impingement on
Description	5-S300	CTU 01 failed.	Solar array output dropped abruptly.	+5 wolt power supply woltage level exceeds tolerance.	HEPAD voltage sensor very sensitive to temperature fluctuation.	VAS filter wheel position telemetry point in- cremented in wrong direction when command executed.	2db ripple DCPR.	Spursous command indications.	Battery 81 charge current telemetry saturates about half the time during high rate charge.	Battery 02 charge current telemetry saturates about half the time during high rate charge.	Spin axis precession.
Ancesaly Time (hours)		. 160	9,280	•	•	•	•	,	•	•	•
Index		•	•	01	n	21	=	*	\$1	91	r,

Nescks											
Corrective Action (if known)											
Mission Effect		Negligible, mag- netometer sensors still usable.		Caused loss of about 50% of experiment data.	Megligible.	25% data lost.	50% data lost.	Loss of experiment.	Commands eventually accepted and operation normal.	Megligible; commands eventually accepted and operation normal.	Negligible.
Cause		Unknown, cause not investigated.		Design error or over- sight; sensors were light sensitive.	Unknown.	Probably due to micrometeoroid impact.	Unknown.	Unknown.	Unknown.	Unknown.	Unk nown .
Description	8- 4 81	Flipper on NESS experiment failed.	1:22-1	Sumlight entered sensor of electrons and protons experiment.	Ion Composition Experiment high voltage power supply failed.	Detector window of Low Energy Obsmic Rey Experiment punctured.	Plasma Experiment high woltage control circuit inoperative at high limits.	Short in -6 wolt power supply in Energetic Electrons and Protons Experiment.	Spacecraft required 3 to 4 hours to warm-up before commands were accepted following eclipse.	low Energy Protons and Electrons Experiment "A" section saturated.	Fast Electrons Experiment high voltage power supply abnormally turned itself off.
Anomaly Time (hours)		39,000		•	4,150	6,930	10,650	16, 340	21, 360	26, 320	28, 440
Index		٦		-	~	•	•	•	•	-	w

Nemarks					Stailer problem on ISEE-3.	OF	RIGIRI PO		PAGE H QUALITY	3		
Corrective Action (if known)												
Mission Effect		Negligible since subsequent maneuvers normal.	Negligible: temporary problem which did not recur.	Possible partial operation; no further data available.	Spacecraft shutdown during eclipse; solar power adequate for spacecraft loads during non-eclipse.		Small; caused a 6-bour loss of data.	Negligible.	Negligible.		Serious loss of experiment data.	Serious loss of experiment data.
Cause		Attributed to garbled command.	Attributed to "glitch".	Caused by defect in a second level power supply.	Caused by battery degradation and consequently, overpressure.		Unk nown.	Unk nown .	Due to fatigue effects in channel- tron electron multiplier.		Unknown.	Unknown.
Pascription	ISEE-1	ACS switched from pulsed firing mode to continuous firing mode during attempted recrientation maneuver.	Magnetometer did not respond to commands.	Ion Composition Experiment power supply shutdown; could not be commanded back on.	Battery failed.	1522-2	Spacecraft shutdown due to undervoltage.	High voltage failure in Fast Plasma Experiment.	Solar Wind Experiment count rate degraded.	E-22SI	Gamma Ray Burst Experiment pulse height analyser mamory failed.	Loss of pulse height analyzer in High Energy Cosmic Ray Experiment.
Anomaly Time	(HOLLS)	29, 160	31,580	38,610	39,450		16,820	21,500	37,000		3,620	4,360
		σ	9	ä	ä		4	~	•		-	~

	11,1		,		Corrective Action	41.51
Index	(hours)	Description	Cause	Hission Cirect	(II KINGHI)	
		1266-3				
•	11,200	Short in low voltage power supply of solar M-rays and electrons expe	Unknown.	Small; loss of electron portion of experiment but x-ray portion not affected.		
•	13,940	rtion of Solar Manu Experiment atopped outputting counts.	Unknown.	Possibly 50% loss of experiment.		
•	16,050	Sizable hydrazine use and spin rate changes prior to attitude maneuver.	Probably caused by bad command sequence.	Small since maneuver completed by redundant system and no re- currence of problem.		
٠	22,460	Pailure in solar wind instrument.	Unknown.	Negligible, since solar wind information apparently recon- structed from data from another part of the instrument.		
^	29, 130	Battery voltage dropped to 3 volts (should have been 20v).	Caused by battery degradation and consequently, overpressure.	Negligible, battery not needed for present or remaining portion of mission.		Similar problem on ISEC-1.
-	02	1UE Panoramic Attitude Scanner 01 failed.	Due to failure of a CMOS IC.	No effect.		
~	100	On-board computer halts, 4k and 8k memories crash, etc.	Possibly to thermal design.	Negligible; software work-around developed.		
m	190	Camera deck temperature decrease from +10°C to +8°C.	Attributed to soft- ware error.	No effect.		
•	9	Short wavelength back- up camera grid voltage incorrect.	Due to temperature.	Negligible, use prime camera.		Camera performa properly in cold temperatures.

Remarks					Intermittent problem.				OF	POOR	QUAI	LITY		
Corrective Action (if known)				Procedure changed to allow lamp to cool.	Resolved by changing from right hand to left hand polarization of ground antenna.									
Mission Effect		Negligible, used redundant unit.	Negligible, method daycloped for attitude recovery.	Negligible.	Not serious.	No effect on power output.	Negligible; problem cleared but space-craft drifted ll*.	Negligible, redundancy available.	Negligible; work- arounds implemented.	Neyligible, alternate camera used.	Negliqible.	Negligible.	unt serious.	Medigible; gred another act of heaters.
Cause		Unknown.	Unkmwn.	Attributed to not lamp.	Ground station problem.	Due to array thermistor failure	Unknown.	Possibly due to a beating problem.	Possibly caused by EMI.	Problem in scan control mode.	Due to improper configuration of camera.	Possibly due to correlation with Earth's radiation bults.	Attributed to OMC qlitch.	Unknewn.
Description	108	Long wavelength cumera scan failure.	Purcramic Attilude sensor #2 does not accept commands.	Camera lamp did not fire.	Telemetry rate change command not executed.	Solar Array temperatures appear abnormal.	Temporary loss of On- Hoard Computer telemetry data.	Gyro #6 failed to start.	Aperture pr.wiem.	Long wavelength camera did not return to stand- by mode.	Abnormally high start wavelength background.	Sporadic false/lost commands from command decoder fl.	Fixed rate slew command not executed.	Hydrazine catalyst beds #4 and #6 not heating.
Anomaly Time		405*	550	1, 320	1,440	1,440	3,890	10,700)5,285	15,790	19, 900	29,800	21,480	25,270
3	N N N N N N N N N N N N N N N N N N N	٠	9	٢	æ	•	10	11	12	13	2	15	16	11

16 ----

Bearing				Unit performs normally but telemetry in error.						•		
Corrective Action (if known)												
Mission Perfector		Not serious.	Small, unit taken off- line but probably usable in an emergency.	Negligible.	Negligible.	Small, lost redundancy.	Small effect; degraded performance.	Negligible, redundancy available.		Small, degraded SAD tracking but returned to normal after a couple of weeks.	No effect.	Negligible.
93114	9000	Probably due to lost command by command decoder or camera logic.	Possibly due to a thermistor failure.	Possibly due to a thermistor failure.	Unknown.	Probably due to gyro feedback loop open.	. חייעוסשווי	Unknown.		Due to high beta angle.	Unknown.	Attributed to sets of parallel solar cells with intermittent electrical connections in an acea of probable high temperature.
Pagenting	anı	Incorrect short wavelength read-out values.	Gyro #1 gradual temperature drop.	Gyro #3 temperature drop.	Loss of PCM stream from S-band antenna.	Gyro #1 abnormally high rate and delta values.	Gyro #5 gradual temperature increase.	Gyro #2 failed.	LANDSAT-2	Sun memmors partially ineffective.	Array degradation was 22.2% at the end of 39 months in orbit (higher than expected).	Array current notching.
Anomaly		26,250	30,000	31,100	33,500	35,880	37,200	39,400		27,200	28,100	31,500
	7	91	19	92	22	22	23	77		•	~	m

Nema r k s				Later indications show high friction present.	Occurred on Landmat-3.	Possible redistribution of lubrication allowed reactivation.			GINA POO				
Corrective Action (if known)										۳		> -	
Mission Effect		Negligible.	Negligible; NBTR #2 used.	Negligible, RMP-1 turned-on.	Negligible, scan monitor switched to 3 source.	Very serious; caused loss of sp.cecraft but operation later restored	Significant, loss of all wideband stored data.	Small, operation restricted to recording 1 orbit per day of "health" data on the last half of the tape.	Negligible, not critical to spacecraft operation.	Small, restricted payload operation.	Negligible; operated properly on second command.	Negligible, ECAM properly enabled again.	Nc,ligible, recovered normal operations.
Cause		Unknown.	Unk nown.	Unknown.	Unknown	Possibly due to lubrication of bearings supporting the flywheel.	Unknown.	Unknown .	Unknown.	Unb nown.	Possibly due to noise.	Unknown.	Unknown.
Description	LANDSAT-2	VMF receiver output briefly abnormal while loading ECAM.	Marrow band tape recorder	RMP-2 motor current began running high.	Infrequent occurrences of MSS missed line starts.	yaw flywheel failed.	WBVTR #2 failed.	NBTR #2 failed to play back until the 3rd playback attempt.	Telemetry excitation line failed open.	Decrease in solar array output, increase 2 months later, decreased again 3 weeks later.	OAS solenoid closed properly on command but re-opened anomalously.	Unencoded C10 command via VHF disabled ECAM.	Yaw flywheel stopped again for about half orbit.
Ancmaly Time (hours)		34,758	34, 886	37, 305	39, 100	41,956	46,712	45,464	49,770	53, 184	58, 155	61,350	61,390
Index		•	₩.	ø	~	s	σ	10	11	12	13	*	15

	Anomaly					
Index	(hours)	Description	Cause	Mission Effect	(if known)	Remarks
		LANDSAT-2				
91	62,665	Command clock power supply #2 failed.	Unknown.	Small, switched to redundant power supply but only I command link now open.		
		LANDSAT-3				
-	w	Left solar paddle did not slew as expected at deployment.	Possibly due to shadowing of sun sensor.	Neyligible, slight deployment delay.		
~	u	Higher spacecraft disturbance torques than expected.	Unknown.	Insignificant.		
•	92	COMSTON-B, cell 4 failed to verify and execute a command.	Unknown.	No effect.		Cell 4 was commanded to zeroes and was no longer used.
•	• \$6 • • • • • • • • • • • • • • • • • • •	RBV camera 01 intermittent white level saturation.	Unknown.	Negligible; did not interrupt RBV operation.		
v	79 7	COMSTOR-3, cell 4 changed from all zeroes to all ones.	Unknown.	Negligible, redundant COMSTOR-A used.		COMSTOR-B returned to service at 2976 hours.
•	009	Small percentage of MSS processed pictures have random patches of "salt and pepper".	Unknown.	Not serious.		
•	1,440	ECAM halted due to a fixed core checksum error.	Attributed to bit failure in core location.	No effect.		Checksum modified to accommodate the error
•	1,600	MSS band 5 degradation, no video sensor 25 video output on band 5, and degraded output from sensor 26,	Attributed to contamination from residual gas molecules.	Significant; loss of IR data.		Periodic outgassing performed to clean sensors but not successful in long run.
n	3, 190	SMART #6 fired on analogend of tape detection for WBVTR #1.	Unknown.	Not serious.		

Corrective Action (if known)			Subsequent tests showed normal current.							
Corre			40 E	Switch to scen monitor light source B temporarily resolved problem but re- curred.					Mission planning instructed not playback both payloads at night.	Landaat's 1 and 2 had similar occurrences.
Mission Effect		Not serious.	No effect.	Significant overall loss of data.	No effect.	No effect.	No effect.	No effect.	Small effect.	Little impact.
Cause		Caused by inadvertent tape recorder operation to end-of-tape.	Due to high headwheel current on WBVTR #1.	Cause unknown.	Unknown .	Unknown	Trip legitimate.	Due to high head- wheel current on WBVTR 81.	Due to simultaneous playback of MSS and MSV during space- craft night, thus discharged batteries to low level.	Occurs over magnetic anomalies.
Description	LANDSAT-3	SMART 84 and 5 fired on digital and of tape datection for both WB tape recorders.	SMART B2 fired.	MSS missed/late line styrts.	APU time code to MSS rollover of 10th's and 100th's of a second occurred a few milliseconds earlier than rollover of the even second.	We power map 02 low values for helix current and collector temperature.	swart 66 tripped on end-of-tape protection.	SMART #7 fired on end- of-tape detection for WBVTR #1.	Low unrequiated voltage.	MSS extra scan monitor pulses cause early line starts of extra end-of-line codes.
Arces ly Time (bours)	(Bonts)	3, 260	3, 367	3. 800	4. 300	÷, 300	5.497	¥8.3	6,145	6,720
	×	10	Ħ	2	13	•	15	*	2	•

Anomal Les

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Nemarks			Numeral 10,600 hrs.						Similar situation observed on Landsats 1 and 2 as sessonal variation.			Wavyn 42 continues to be used for MSS and MBV data when required.
Corrective Action (1f known)												
Mission Effect		Negligible.	Negligible, RMP-1 used.	Significant, WBVTR #1 subsequently used only for playback of MBV data.	Small, rear scanner returned to normal.	No effect.	Mot serious.	Megligible ECAM restarted and normal operation resumed.	No effect.	Small, loss of 3 months of date.	Negligible, work- around developed.	Significant. data acquisition severely limited.
Cause		Possibly due to friction buildup in the 2nd or 3rd stage gear reduction.	Unknown.	Unknown.	Possibly due to RFI.	Attributed to failed telemetry circuit.	Possibly due to noise from VMF system.	Possibly due to timer reset command.	Unknown.	Probably open circuit or failed component in MSS multiplexer.	Unknown.	Due to either broken tape or jammed qears.
Description	LANDSAT-3	LSAD motor winding voltage and temperature gradually increasing.	NMP-2 input current increased and spikes occurred on telemetry.	Playback of MGS data on MBVTR 81 nolsy.	Momentary Near Scenner giltches.	Right solar panel temperature abnormally high.	Non-authorised CIU commands.	SCAN halted when S-band timer reset commanded.	Abnormal solar array current notching.	All MES sensors suddenly failed to transmit quantum levels between 1-7, 9-15, 33-39, 41-47.	Short circuit in command matrix A drivers.	MBVTR 81 failed when commanded to fast
Anomely Time (hours)		9 , 900	10, 500	10,913	14,900	17,500	16, 500	20,747	21,840	24, 378	29, 361	31,626
Index		•	2	7	2	2	*	2	*	۲.	2	2

	Anomely				•	
	1		į	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	Corrective Action	3
N N	(hours)	Description	asne.)	Alsaion Errect	(II KIIOMII)	2
		L-MDGAT- 3				
2	32, 500	PSS line length occasionally varied by 2 or 3 pixels.	Unknown.	Small, ground work- arounds being attempted.		
æ	33,000	was occasional missed and-of-line codes.	Unknown	Madigible, normal operation restored by switching from scan monitor A to B.		
35	34, 526	SCAN halted.	Attributed to an illegal word getting into memory.	Insignificant.		
æ	%, 700 007 .¥	MBV Camera 42 Bubscene was 20-104 white background.	Caused by intermittent improper shutter closure.	Significant loss of MBV data.		
		LANDSAT-4				
-	u	Ku-band antenna will not deploy.	Unknown.	Very serious, but follow-up antenna movement attempts successful.		
		HAGBAT				
-	Ü	Design occurred approximately 4 maintes late; only one of two timers functioned.	Possibly due to higher than expected thermal resistance between the fourth stage and the timer.	Negligible.		
~	ŭ	Coarse sun sensor data not decodable.	The cause could have been a hard-ware or algorithm problem; or the rircuitry may have been miswired.	No serious mission effect since other attitude data were available.	A special model was derived for application to the mission.	
~	·	One scalar magnetometer lamp (of two) required slightly more RF power on orbit than in ground tests.	Unk nown .	Megligible.		

			ORIO OF	NAL PAGE	: 13 Lity			-			
Nemarks								Datteries 2 and 7 (of 8) already turned off.			
Corrective Action (1f known)			Loss of 70-80 percent of scalar magnetometer data but little Pission effect since the vector mag- netometer provided sufficient information.								
Mission Effect		Apparently not serious.	Attributed to some kind of feedback from the power supply.	Progressively severe degradation of power supply from inability to charge battery.	No effect on mission objectives.		Megligible.	Megligible.		Partial loss of data.	Negligible, because of earlier failure.
Cause		Unknown.	Caused loss of lock in the tracking filters.	Essentially unknown, but possible loss during launch of thermal panel/shield around the IR scanner on the base of the spacecraft.	Direct sumlight on the sides of the sumshades penetrated their black plastic skin.		Unknown.	Unknoem.		Unk nown .	Unknown.
Description	MAGSAT	Drift track of spacecraft pitch axis exhibited an unpredicted tendency.	Intermittent noise in the lamp excitation circuitry of the Scalar Magnetometer.	Internal temperature of bess module about 10°C higher than expected.	Loss of star camera date for periods of 30-40 minutes.	NIMBOR-4	Nimbus-4 turns twice per orbit.	Dattery 4 turned off.	H I I I I I I I I I I I I I I I I I I I	when channel 5 off full- time, channel 4 off as required for power magnegates.	Batteries 4 and 6 (nf 8) turned off.
Arces 1y Time (hours)		•	2	2	%		,	61,106		37,824	29,000
I a		•	•	•	•		~	~		-	~

Index	Ancmely Time (hours)	Description	Cause	Mission Effect	Corrective Action (1f kncwn)	Nemark o
		NIMBUS-5				
•	60, 290	HDMS3-B exhibited short playbacks.	Unknown.	Loss of some stored data.		
•	006 '09	HDRS-B (tape recorder) returned to normal operation.	Inknown.	No adverse effect, portion of end-of-tape not being used.		
•	\$. 8	HDMSS-A data became noisy.	Partially due to tape flutter and wow.	Loss of some stored data.		Attampted to fine tune ground stations to accommodate incressed flutter and wow.
•	71,165	Prime CONSTOR went into illegal mode many times during l pass.	Attributed to Y-enable pulse being to short.	Loss of 1 orbit of ESMR data.	Afterwards ground station work-around.	Mas happened before.
^	71,550	MDBSS-A failed; tape did not move.	Unknown .	Non-real time data collection restricted to Tape Recorder B.		
•	3 , 300	MDMS-B failed; no modulation.	Probably due to broken belt or tape.	Significant, space craft restricted to real time data acquisition only.		Loss of ESHM Antarctic coverage for the Mavy.
		9-90-91				
-	12,000	ESMR horizontal channel failed.	Unknown.	Small, partial loss of ESMM data.		
~	15,770	THIR radiometer motor failed.	Unknown.	Small; loss of TMIR instrument.		
•	15,660	ENS scanhead locked at NADIR view.	Unknown.	Small; partial loss of ERS date.		

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Corrective Action	(11 Khown)		A positive 12-second charge placed on momentum pitch coil and duty cycle re- turned to average 50 range.				Work-around being developed.				
	Alssion Ellect		Megligible, returned to normal.	Not serious.	Serious, limits Nimbus-6 to real time data acquisition only.	Not serious.	Serious, causes re- maining 7 batteries to become overcharged and too hot.	Small, reduced water coverage from 90% to 50-60%.	Small, data no longer collected in the area of \$10° of the solar equator.	No affect, lens heaters were turned off.	No effect; problem was expected.
			Unknown.	Unknown.	Unknown.	Unknown.	Unknown.	Unknown.	Due to sun glint.	Due to erroneous thermal mold.	Due to type of detectors used for the data channels.
	Description	9-S0001N	Average yew wheel motor drivers duty cycle exceeded 20%.	Prime COMETOR switched out of verify mode into indeterminant mode.	HDMSS-B failed.	Apparent NIM-5 sequence was found in COMSTOR NIM-6 location.	Battery 96 lost its capability.	Use of CZCS threshold on mode causes loss of data in CZCS channels 1-4.	CZCS data taken within ilo of solar equator worthless.	SAMS lens temperature increased to 53°C.	SAME; interference on data channels and chooses amplitude.
Ancesty	(Pours)		.5, 623	42,426	\$0,06	50,447	55, 460	•	.	\$	53
-	I NO		•	w	•	•	•	4	~	•	•

Renarks		Mas eeen in test.	Dropout appears to be level sensitive.	Problem could have existed pre-leunch; loading both memories with different programs had not been tested.	Occurs randomly in real time data operations with high gain and threshold off.			This was expected.		
Corrective Action (1f known)										
Tipe in the contract of the co		Megligible.	Megligible.	Small; memory must be reloaded for each new scan pattern.	Not serious.	Small: performance adequate.	Not serious.	Megligible; within allowable roll rate amplitude.	Small; requires 2 commands be sent.	Small, problem has not recurred.
į		Unknown .	Unk nown .	Attributed to internal logic fault that prevents switching between memories.	Unknown.	Unknown.	Unknown.	Unknown.	Unknown.	Unknown.
;	Description NIMBUS-7	TOMS high voltage dropped 25% for 1 data frame and 2 disturbances on TOM PMT output for this frame.	SBUV output drops to zero for 1 sample during solar calibration in continuous scan mode.	Only I memory unit in the SAMS PCL accessible.	CZCS deta dropout on channel 4 data.	After activating SAMS cooler, detector cooled to only 165*K.	VIP telemetry glitches when CRCS DC restore for any channel goes to positive.	Spacecraft attitude disturbance at CZCS scan turn-on and turn-off.	EMS solar assy, moved 2° right on a 1° right command.	SAME scan shifted 43 counts, cell 43 changed from command 557 to zero, PCL program shifted to a new location.
Accessly Time	(hours)	185	*	976	+ 02+	\$	675	o 60	1,040	1,193
-	Index	•	•	•	3	•	10	a	ä	a

Remarks							Occurs during earth night/non-scan period.	Correlates with solar incidence angle.		
							Occur night,	Oorre Incid		
Corrective Action (if known)										
Mission Effect		Small; causes some problems in ground computer housekeeping data processing.	Small; channel 18 data, direct measurement of earth flux, unusable but other data used to derive earth flux.	Small, resulted in several orbits with no SAM II operation.	Megligible.	Not serious.	Not serious.	Not serious.	Small, scan routines 3 and 4 no longer used; scan routine 5 is now SOP.	Small; ERB channel 18 data not usable.
Š		Unknoem.	Unknown.	Unknown.	Attributed to simbal motor torque margin and lubricant viscosity and later to gimbal slew malfunction.	Possibly due to a clock race condition.	Unknown.	Unknown.	Unknown.	Unknown.
Mecription	NIMBUS-7	SAM II power on/off status telemetry monitor erfatic.	Degradation of EMB scanning channel #18 output.	Difficulties with execution of real time commands and CONSTOR loading.	EMB scanlead went into a forbidden sone.	Commands did not execute.	SBUN/TOMS signature of continuous scan data telemetry changed.	DGAS sensor 2 elevation decreases from 4.8 ThV to 4.0 ThV and elevation position levels out at 160 counts for about 1 to 2 extra samples.	ERB scan did not go on when commanded following a scan routine change.	ENB channel 18 went from occasionally noisy to full time noisy.
Anomaly Time (bours)		7. 1 8	7,8	1,700 to 3,000	1,700	1,760 to 2,668	1,037	2, 100	2,375	2,773
į		7	ş	2	2	9 1	61	8	:	æ

Reserks							Problem was essentially negligible to start with later (orbit 4200) observed 90% of the time and coused reduced CZCS operating time.	LIMS was turned off on Orbit 3,092 after 4,865 operating hours (turned off permanently).		
Corrective Action (if known)									Periodically turn off Battery 4 so charge/ discharge sharing balanced for other batteries.	wew procedure instituted to use only the middle of the tape, lose 65% of tape.
Mission Effect		Not serious.	None, has not effected data collection.	Negligible; reloaded PCL and continued with normal operation.	Negligible, does not effect SAM II data or operations.	Small.	Small effect.	Small.	Negligible.	Negligible.
Cause		Unk nown.	Unknown.	Unknown.	Unknown.	Due to DC restore problem.	Unk nown .	Due to increased detector temperature caysed by depletion of the cryogen methane.	Due to newer Battery 4 mismatched with other older batteries - problem expected.	Unknown.
Description	NIMBUS-7	3 commands failed to execute from redundant COMSTOR.	EMB scan angle encoder output showed sharp drop.	SAMS limb scan went to an illegal stop.	SAM II: 4 count variation in RVCT analog telemetry monitor.	CZCS channel 5 output occasionally low.	240mm notch in array current occurs every orbit at 25 minutes; after spacecraft night to day transition.	LIMS lost lock on the limb.	Battery 84 high charge/ load sharing relative to other batteries.	Tape recorder #1 stalled in record mode at BOT +5 minutes, recovered, later had data dropouts.
Ancmely Time	(STOCK)	3,530	4,189*	4,520*	4,763	4.777	6, 4	5,235	5,242	5, 337
-	Y MOU	23	5	22	*	23	99	8	8	Ħ

Rome rk s		Now left on contin- uously.	Involves apparent shadowing of SAM II azimuth sunsensors.						Could eventually allow lubricant to leak and result in binding of bearings.			
Corrective Action (if known)		Finally turned on after many attempts.					Decontamination cycle performed which corrected problem.					
Mission Effect		Negligible.	Negligible.	Negligible.	Megligible, used calibration lamp #2.	Small, operational procedures implemented to circumvent problem.	Negligible.	Megligible.	Megligible, did not result in voltage or current changes.	Not serious.	No significant loss of data.	Negligible; PCL was reloaded and no further problems.
Cause		Unknown.	Attributed to S-band antenne getting into fov.	Attributed to clock-race problem.	Possibly due to calibration lamp #1.	Possibly due to CDIU current.	Unkrown.	Indicative of drop in output of Gundiode oscillator.	Attributed to leak in metal bellows assy.	Unknown.	Unknown.	Unknown.
Description	NIMBUS-7	Unable to command TUMS high woltage on.	SAM II; whole disk of sun not in fov at sunset.	Commands did not execute.	CZCS mannels 1-5 showed 4 step decrease during calibration.	Could not acquire space- craft though spacecraft receiver AGC levels adequate.	C2CS channel 6 detector temperature.	SMMR channel 1 crystal current monitors showed decrease counts.	Left SAD housing pressure drops.	SPER channel 1 output and calibration data went to full scale for about 30 seconds.	I frame drop-out cn tape recorder #2 near BOT in playback.	SAM PCL jumped into unscheduled calibrate and then back.
Anomaly Time (hours)		5,576	\$,600	6, 391	6,741	7,096	7, 106	7,429*	10,6%	11, 788	11,790*	12,150
Index		35	æ	*	35	9	ŗ.	9	ድ	\$;	7

•				Operation normal in non-scan, nadir view.			Had been seen in teat.		Concentrated in S.E. Asia area.	Recorder positioned to bypass the "gap" area.			
Remarks				Operation non-scan,			Hed bean		Concentrat Asia area.	Recorder bypass t			
Corrective Action (if known)													
Mission Effect			Not serious.	Small, caused loss of ERB scanning channel.	Negligible, returned to normal following eclipse.	No effect.	No effect.	Neqligible, returned to normal within l orbit.	No effect.	Small.	No effect.	No apparent effect.	Negligible, problem went away.
90.00	agen		Unknown.	Unknown.	Caused by solar eclipse.	Unknown.	Due to input to LVDT counter floating in the standby mode.	Unknown .	Unknown.	Possible due to foreign object between tape and heads.	Attributed to instrument seeing some kind of reflection.	Unknown.	Possibly due to Analog MUX and/or A/b converter.
	Description	NIMBUS-7	ERB failed to go to long- wave check position as commanded.	ERB chopper stopped rotating.	Solar array output dropped 30%.	Transponder downlink turned-on spontaneously.	SAMS limb LVDT telemetry output became erratic after instrument placed in standby mode.	Manifold pressure increased out-of-limits following simultaneous fixings of + pitch and - roll.	Intermittent instances of receiver in-	Tape Recorder #2 si ved a 12.5 minute gap on playback.	SAM II changed from fast scan mode to slow scan mode before fast scan completed.	TOMS chopper motor current dropped.	VIP subsystem - all analog telemetry went to .4 TMV level for 32 minutes.
Ancealy	(hours)		13,125	14,538	15, 725	16,572	17,158	19, 295	24, 200	25,690	27, 890	28,905	
	Index		\$;	\$	ş	+	•	46	8	51	52	53

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	Romarks									
Corrective Action	(if known)									
·	Mission Effect		Small, squibs fired after repetition of firing commands.	Small, ERB scan operation placed on 2 out of 4 day duty cycle.	Smeil.	No mission effect.	Not serious.	Negligible.	Not serious.	No mission effect.
•	Cause		Unknown.	Possibly due to structural resonance structural trans- mission.	Ground station problem.	Possibly due to higher earth albedo in orbit than was simulated in thermal/vac.	Unknown.	Possibly due to race condition between incoming command and internal command clock timing.	Unknown.	Design problem.
	Description	NIMBUS-7	Squib firing required refiring for LIMS methane squib, Smell squib, CZCS.	ERB scanning interferes with LIMS limb scanning.	Ground receivers unable to lock on to 4kbps VIP when transponder modulated with 25 kbps DIP data.	Unexpected high temperature of CZCS cooler door and cone due to door heater.	Digital solar aspect sensor; small errors for brief periods (occasional 3 count jump in aximuth).	Real time commands and commands loading commands not executed properly.	CZCS channels 1-4 gain less than expected.	Stells cold horn views
Anchely Time	(bours)		•	,		•	,	•		•
,	Index		3	\$\$	\$	53	8	55	9	61

Corrective Action (if known)		1 to		ient Also occurred on TIROS-N and the USAF DMSP spacecraft.	orced atus rmally.	urned to	tem acted	Corrected in software.	acecraft.			
Mission Effect		Small, returned to normal.		Small, no permenent degradation to page- craft.	Small; CPU %) forced back to "ok" status and operated normally	Negligible, returned to normal.	Negligible, system acted acted normal.	Negligible.	No effect on spacecraft.	No effect.	Negligible.	Not serious.
Cause		Due to time base unit being reset without re-selection of Recorder #3.		Probably due to thrust developed by flow of hydrazine propellant.	Due to timing switching problems at handover from boost mode.	Unknown.	Probably due to spurious switching.	Apparently due to a wiring error.	Unknown due to lack of data.	Due to ACS algorithm assuming spherical earth instead of real ellipsoid.	Possibly due to contamination from the apogee motor burn.	Due to thermal gradient.
Description	NOAA-5	Scanning Radiometer Recorder #3 would not playback.	NOAA-6	Large spacecraft disturbance and attitude perturbation just post- launch.	CPU #1 indicated "not ok" at initial contact.	One thermistor on Rocket Engine Assy #2 indicated saturation or full scale reading.	Skew gyro replaced the z gyro in the gyro use matrix.	Analog telemetry channels 303 and 277 are reversed.	SAD command mode changed from normal mode to complement mode.	Spacecraft attitude shift of 0.1" in pitch and roll when sun-moon flag set for 2 quads of the ESA.	Hydrazine components run horcor than expected in 160% sun.	Small difference between the readings
Aromaly Time (hours)		22, 100		u.	w	w	ų	w	u	u	w	380
Index		30		-	~	m	•	so.	ø	^	©	•

ı				ORIGIT	NAL DOR	PAGE (8 'Y					
Powerks				Would degrade the instrument if it got would.			CTN-2A taken out of service.			Data sollection function taken over by HDA.		
Corrective Action (if known)												
Hission Effect		No effect.	Data quality not effected.	Small, causes MSU channel 3 gain decrease.	Small, incorrect telemetry point.	Small, caused in- correct yew update but workstroand used.	Negligible, redundancy available.	Small, tape recorder still usable.	Megligible, data still usable.	Small, initially not serious but eventually taken out of service.	Small, normal operation returned after each occurrence.	Negligible, commanded back to normal.
Cause		Unknown.	Unknown.	Due to poor design of an attenuator in a local oscillator circuit.	Uhknoem.	Unk nown .	Unknown.	Unknown.	Unknown.	Attributed to low leakage resistance in lock-up capacitor CIO.	Attributed to normal eging.	Unknown.
Description	9-WOM	Nitrogen latching valve temperature almost doubled, then returned to normal.	MEU channel gains and crystal currents took longer to stabilize then expected.	MEU crystal current decrease and space count increases at a rate of 4-5 counts per day.	Faulty DTP4A pressure	Twaperature bias abift of about 0.5 per hour in skew gyro.	Excessive bit error rates and data dropowts from DTR-2A.	DTR-1A started exhibiting noise.	AVHUR channel 3 becoming increasingly noisy.	OTR-28 began a pattern of loss of sync lock and slow data starts.	AVMIR excessive scan motor jitter, loss of sync.	Uncommended 4 level increase in TED electron/proton high walt see proper surply.
Arcmely time (Bours)		009	720	3, 300	3,640	7,650	7,990	13,510	15,040	15,400	10.670	19,240
į		01	a	21	2	*	15	9 1	1	=	2	2

Nemarks			Capacitor identified as problem before launch.							yaw "x" -axis wheel- speed is unloaded with nitrogen firing on a once-a-day basis.		
Corrective Action (if known)												
Mission Effect		Negligible, back-up gyro used.	Small, problem comes and goes.	Negligible, yaw gyro was commanded out and the roll gyro back in.				Negligible, redundant units available.	No effect.	Small effect.	Negligible; compensated by ground processing.	No impact.
Cause		Unknown.	Due to failed CKROS ceramic capacitor in Logic Register Circuit, but "self heals".	Unknown.		Malfunction in the Atlas booster caused thrust reduction		Unknown.	Possibly due to mechanical hang-up.	Attributed to higher than expected torque from solar pressure.	Unknown.	Unknown.
Description	HOAA-6	Holl gyro exceeded stability specification.	AVMAR electronics current and 6.2v reference dropped, temperature changes, scan motor current intermittent erratic	Increasing attitude errors.	NOA-B	Spacecraft did not attain operational orbit.	HOAA-7	DFR-4A failed to playback.	AVMER earth shield door slow to deploy.	Magnetic coil un- loadings not completely effective.	TIP clock I second ahead of command clock.	After rate maneuvers, requiated nitrogen pressure increased to 661 psi in a few seconds; held for 23 seconds then Autroased to 515 in 20 seconds.
Arcealy Time (hours)		21,120	23, 300	26,110		u		u	Ü	J	u	•
Index		~	*	23		-		-	~	•	•	•

MOMA-7 Command receivers stay in operate mode continuously	Cause Suspected cause is pror cost cable	Mission Effect	(if known) (shown) Repaired at NOAA lab.	Nemarks
operate mode continuously rather than reverting to standby. Array drive electronics baseplate temperature higher than expected; enhibits continuing tends.	poor coax cable fabrication workmanship in SEM. Unknown.	Small: temperatures decreasing, possibly due to declining sun angle.	ì	Contingency plans for loss of SAD developed
	Unknown.	Small.		Causes small attitude transient for about 2 minutes in roll-and- Fitch.
	Unknown.	Megligible.	Commanded back to normal but command correction must be timely to prevent data loss.	Similar to incident on NOAA-6.
	Unknown.	No significant impact on data.		
	Caused by power/ signal ground coupling.	No significant effect.		Similar to problem on MOAA-5.
	Unknown.	Negligible.		Detectors stabilised but detector #1 not used extensively.
	Unknown.	Megligible.		May be related to EMI generated in detector 02 during breakdown.

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Nemark s			ORIGII OF PC	NAL PA OOR QU	GE 19 ALITY			Occurred 26 times.
Corrective Action (if known)		Cycling vidicon power for 20 minutes per orbit removed the artifacts in science images.	Propene detectors were turned off to allow venting.					
Nission Effect		Small	Negligible.	Negligible.	Negligible, instrument warmed up ok.	No effect.	Negligible, "B" system available.	Megligible, procedure implemented to turn the detectors off at night.
Cause		Attributed to sensitualty of vidicon blanking circuitry to t' high temperatures resulting from continuously "on"	Due to internal water vapor.	Software error.	Unknown.	Attributed to attenuation of solar flux due to water evaporation from spacecraft.	Possibly due to generic cause.	Unknown.
Description	5 5	Coronagraph/polarimeter vidicon beam not blanked off properly during retrace.	Intermittent high count rates indicative of internal arcing in soft x-ray polychromator instrument.	Fine pointing sun sensor 81 bissed by about 4 arc- minutes from the 'struments.	Mard x-ray burst apectromater detectors and low voltage converter temperatures lower than expected at turn-on.	3 Active Cavity Radio- meter Semsors showed upward drift.	Soft x-ray polychro- mator PCS drive en- coder bulb failed open.	Soft x-ray polychro- mater thin window high woltage flip flope spuriously reset during orbit night
Anomaly Time (hours)		•	•	•	•	•	00	8
Index		•	•	∽	•	^	•	

, to			Unit finally failed;	May be part of Anomaly 69.	Or I	OOK 40		
Corrective Action								
Missing Wifert		No effect.	No problem as long as mater microprocessor is runing.	Negligible.	Megligible; data normal after high voltage setting reduced.	Megligible, corrected via moftware.	Small, detector #2 no longer used on a requiar basis.	Medigible; spacecraft was commend back to proper attitude and correct quide stars reacquired.
•		Unknown.	Possibly due to internal flare mode software becoming confused with rapid flare threshold level changes.	Unknown.	Unknown.	Unknown.	Attributed to breakdown of detector.	Unknown.
1	NATURAL DESCRIPTION OF THE PROPERTY OF THE PRO	Mandom 0.3 amp pulses on pulse load bus and quiet load bus.	Microprocessor in the hard x-ray imaging spectrometer shuts down about once per day in slave unit.	Soft x-ray polychro- mator major diltch during orbit night turned off FCS micro- processor and propane detectors high voltage, changed raster motor positions, smitched from NIU clock to internal clock, lowered +5 V bus, ruined PCS analog MIX data.	Soft x-ray polychro- mator PCS detector 86 shows increasing gain indicative of a lesk.	C and DN clock jumped forward by l hour, 9 minutes over South Atlantic anomaly.	UV spectrometer/ polarimeter instrument high count rate from detector #2 led to unscheduled shutdown of power converter.	Selected quide stars were lost by the on- board computer and caused a roll error of 3.5.
Accessy Time	(Bours)	\$ 20	§	8	920	•30	91	1,150
•	X 000	01	=	3	ន	.	ន	4

Index	Anomaly Time (hours)	Description	Cause	Mission Effect	Corrective Action (1f known)	Nema rk
		.				
£1	1, 295	Intensity level of both fine pointing sun sensors degrading with time, cause on-board computer to put syacecraft into night mode during orbit day.	Unknown.	Megligible, software changed to provide more frequent calibrations and adjustment of thresh- old.		
2	2, 320	Spacecraft lost the sun during a slew maneuver.	Caused by software "bug".	Negligible, space- craft commanded back to sun center.	Software presumably corrected.	
2	2, 330	Mediation sensitivity of alcroprocessor random access memory causes trandom state changes over South Atlantic Anomaly (in C and DH)	Unknown.	Small, some loss of instrument data due to equipment turn- offs.	Work-arounds developed.	
2	2, 450	Mard x-ray imaging spectrometer micro- processor 82 failed.	Mardeare failure.	Negligible.		
11	2,590	Star tracker 81 data showed 2 stars in view Cue to star number not switching in telemetry.	Probably due to software error.	Apparently no impact.		
2	3, 460	MO tape recorder segment counter bit 29 stuck.	Due to a part failure.	Small, ground system software changed to work-around.		
2	3,480	Telemetry and clock out-of-sync.	Unknown.	Negligible, commanded back to normal.		
*	3,640	Monitoring software were indicated fatal error in coromagraph/ polarimeter.	Possibly due to software problem.	Megligible.		
æ	3, 72¢	Soft w-ray poly- chromator raster drive stepper motor occasionally fails to complete a step when commanded.	Unknown.	Megligible, back-up Motor available.		

Rees rks								Not clear if "micro" is microcossor or microcode.		Raster commanded to a "sit and state" position.	
Corrective Action (if known)											
Mission Effect		Negligible, software workaround developed.	Negligible.	Negligible.	Megligible, redundant unit available.	Small, control regained and Gyro B used.	Small severely limits use of instrument.	Megligible.	Small.	Small.	Small, skew wheel switched to yaw and roll allowed to drift.
Cause		Possibly due to multiple reflections of earth albedo getting into Fine Pointing Sun Sensor field of view.	Could be software or hardware problem.	Could be software or hardware problem.	Unknown.	Attributed to transient radiation susceptibility of complementary MOS semi-conductor in the electronics.	Possibly due to degradation in parts in erase, expose and read-out control circuits.	Unknown.	Due to fuse design.	Unknown.	Due to fuse design.
Description	5 5	Systematic slow shift of 10-15 arc seconds and back in pitch during last 10 or 12 minutes of speceraft day.	During on-board pitch and yew updating, the gyro angle error was not included.	Moll budgets updated wh.le quide stars occulted.	Hard x-ray burst spectrometer micro- processor #1 failed.	Gyro C failed.	C/P vidicon experiences inter- mittent read out lock- ups.	Soft x-ray polychro- meter BSC "micro" hung up.	Roll reaction wheel lost.	Soft x-ray polychro- mator solenoid valves incorrectly disabled.	Yaw reaction wheel lost.
Amomaly Time (hours)		3, 800	7,080	4,120	4,250	9, 560	4. 600	5, 760	6,570	9,500	6,760
Index		*	۲.	8	\$\$	8	τ	æ	č	*	35

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Nemarks				OI OF	RIGIN PO	IAL PA	GE 18 ALITY				
Corrective Action (if known)											
Mission Effect		Significant, spacecraft no longer useful for scientific data collection.	Negligible	Negligible.	Negligible.	No effect.	Not significant	Not serious.	Negligible, eventually stabilized.	Minor.	Megligible, sensitivity still adequate.
Cause		Due to fuse design.	Unk nown .	Unknown.	Unknown.	Unk nown.	Unknown.	Unknown	Unknown.	Due to solar structure.	Unknown.
Description	# S	Pitch reaction wheel lost due to fuse failure.	Erratic torquer bar telemetry and torquers not responding correctly to commands.	High Gyro-B motor current.	Problem in Tape Recorder B.	Decrease in sensitivity by a factor of 200 in uv spectrometer in Lyman-alpha range.	On certain fast motions, x-ray polychromator unpowered raster cam Z _b auto rotates.	Spacecraft disturbances of up to 3 arc-seconds at x-ray polychromator FCS raster flyback.	X-ray polychromator outer thermal shield unexpected rise to 76.c.	UV spectrometer scatter.	UV spectrometer sensitivity at short wavelength showed substantial degradation.
Ances ly Trae (bours)		7,220	7,870	12,200	12,400	,	,	•	•		,
rode x		£	r.	38	£	Q	7	\$	\$;	2

				ORI(OF	GINAL POOF	PAG QUA	E IS	;			
Roberts	Caused degraded VISSP. data; receiver no longer used.	Problem resolved after transmitter warmed up.						After this failure, speckeraft used only as a repeater for GOES-5 VISSR, DCS, and WETAX data.			Due to concern over possible unequal fuel depletion causing socceraft misslign-
Corrective Action (if known)											
Hission Effect	. · · · · · · · · · · · · · · · · · · ·	No mission effect.	Significant, payload data no longer available.		Small, wide band picture data not possible.	Minor; some in- convenience to ground station.	Megligible, primary unit used.	Significant; loss of VISSR data.	Not significant.	Not significant.	Small
Cause	Unknown.	Temperature related.	Unknown.		Unknown.	Unknown.	Probe bly due to blown encoder bulb.	Probably due to short circuit in the encoder.	Unknown.	Unknown.	Unknown.
Description	SMS-1 S-band receiver #1 reduction in MF power.	VMF transmitter has drop-outs in downlink.	S-band transmitter 01 reduced power output.	2-982-5	S-band Transmitter anomaly.	Wif RF power telemetry point failed.	VISSR back-up encoder failed.	VISSR primary encoder failed.	Two solar array temperature sensors failed.	Battery #1 discharge current telemetry sensor failed.	Possible reaction control system block- age suspected:
Mocmaly Time (hours)	42,575	51,600*	\$1,980		27,060	27,110	52, 360	96, 900	•		•
, ag	•	~	n		-	~	•	•	•	٠	•

Remark					Precludes trickle charging, eventually caused noise on AVHRR 3.5 micron channel.			ORIGI OF P	NAL PAGE OOR QUAL
Corrective Action (if known)				Coffection put into on- board software.			On subsequent spacecraft, hardware modifications implemented and procedures instigated to check torque on "B" nut at launch pad.	On subsequent spacecraft, contamination shields were installed and 6 additional temperature sensors were provided to better map thermal performance of the RCS.	On subsequent spacecraft, the set point dead band widened.
Mission Effect		Small.		Negligible.	No significant effect on mission.	No effect on mission, both baseplates below allowable upper limit of 30°C.	Small, nitrogen system countoracted tumble until stability regained and then momentum wheels took over.	No mission effect.	No effect on mission.
Cause		Fossibly due to ground station or earlier anomaly.		Due to open detector in I quadrant; attributed to lead bond contamination due to dirty masks or some other process control deficiency.	Cause unknown but somehow related to battery charge circuit.	Attributed to improper thermal mode and too small a AVHRR radiator.	Attributed to failure of hydrazine system "B" nut; hydrazine leak due to probable relaxation of "B" nut because of pyro shouk.	Due to improper thermal design and contamination of surfaces by apogee motor.	Caused by leakdor current in the thermal control electronics doing to a worst case condition.
Description	SHS-2	S-band low power mode prohibited.	T1 ROS - N	Degraded output from one of the earth sensor quadrants causes small attitude excursions whenever one of the quadrants is temporarily disabled by the software because of sun intefference.	Battery bus current oscillation in taper charge mode.	AVHRR baseplate and SSU baseplate temperatures stabilized above predicted temperature.	Loss of attitude control; lost array orientation to the sun; battery voltage dropped to 18 volts; s cecraft began rolling and tumbling.	Reaction support structures and hydrazine temperatures high.	Telemetry indicated heaters on and louvers open simultaneously.
Aromaly Time (bours)		,		u	+	u	u	u	u
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Renarks				Receiver operates in a band that carries TV and smarrour radio traffic.								
Corrective Action (if known)		On subsequent spacecraft, the latch was redesigned and special pre-launch handling requirements instituted.			Software corrected.						Software change mode for subsequent space- craft.	
Mission Effect		No mission effect.	Small, loss of 1 of 3 SSU channels.	No mission effect.	Negligible	No offect, TCE'S commanded back on.	No effect, operation is normal in bias mode.	Negligible; started via command.	Small, correct calibration constants were loaded.	Negligible, on-board software corrected.	Negligible; was dis- abled and reenabled to regain sync.	Negligible; on-board software corrected.
Cause		Due to design.	Cause unknown.	Attributed to spurious ground signals in the frequency band of the command receiver.	Unknown.	Unknown.	Unknown.	Unknown.	Software problem.	Software problem.	Software problem.	Software problem.
Description	TIROS-N	HIRS/2 cooler door opened at shroud jettison.	No data output from SSU channel 3.	Command verification without commands being initiated.	Incorrect constant in on-board software caused a 5° yaw error.	TCE 82-816 turned off erroneously at turn-on of CPU 81.	SEM TED proton counters output higher than expected at first turnon.	GEODAT program not running in back-up CPU.	Incorrect error factor gyro bias constants.	Day/night flay in CPU telemetry appeared 1.5 minutes late.	CPU #1 telemetry lost sync after dump of stored command table.	Eclipse flag did not come on after eclipse.
Anomaly Time (hours)			w	u	u	w	u	u	160	790	270+	380
Index		^	6	œ	01	a	12	2	5	15	16	7.1

	Remarks		Drift stabilized at acceptable point.	Transmitter continued to be used but link threshold is marginal at elevations below 20.					78. 17 Y T LLALI		
Corrective Action	(if known)						High input gate leakage is the auspect failure mechanism which was seen on NOAA-A.				
	Mission Effect		No impact on data quality.	Small.	No impact.	Small, error rate reduced by running the tape transports from end to end several times.		No effect.	No effect; corrected via software threshold reset.	No effect.	No effect on data gathering.
	Cause		Unknown.	Unknown.	Unknown.	Unknown.	No effect, use CPU 81.	Due to moon in field in view.	Unknown .	Due to moon in field of view.	Due to noise spike on 1 KHz clock.
	Description	TI ROS-N	MSU channel 2 space temperature calibration point drift.	S-band transmitter #3 power output dropped from 9 watts to 4 watts.	Battery currents went to c/300 instead of c/60 when power sub- system went into trickle charge mode.	High bit rate errors on DTR #2A and 2B.	Back-up computer malfunction due to intermittent "stuck" bit in ROM address register position 5.	AV: space and back- scan values changed abruptly over a period of 25 seconds.	All ESA detectors show a rapid change at sun interference in quads 2 and 4.	HIRS space view values changed for 3 cycles then returned to normal.	SSU lost sync in auto calibrate mode.
Anomaly	(hours)		4 90	1,200	1,650	1,700+	1,990*	2,060	2,110	2,130	2,250
	Index		18	91	90	21	22	23	5¢	25	%

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Remarks						Spacecraft went into tumbling and control restored 5 days later.	0		AGE IS UALITY
Corrective Action (if known)					Backup skewed gyro commanded to replace yaw gyro.				
Mission Effect		Loss of house- keeping telemetry point.	No effect.	Not serious.	Negligible.	Small, CPU #2 had to be used despite erratic behavior.	Negligible.	Medigible, tempera- ture did not increase enough to cause any problem.	Negligible, remaining battery packs sufficient to carry spacecraft load.
Cause		Unknown.	Unknown.	Due to minor algorithm error: algorithm assumes spherical instead of ellipsoidal earth.	Unknown .	Possibly due to failure in CPU control logic.	Attributed to reduction of optics contamination due to direct exposure to sunlight during tumbling (see anomaly #31).	Suspect that a heater which is bonded to a thermistor lifted.	Due to a shorted cell caused by manfacturing techniques.
Description	TIROS-N	Failure of temperature sensor.	Commanding failed to activate SEMS TED proton output.	Slight spacecraft attitude shift when sun-moon flag set for 2 ESA quads.	Erratic behavior of the yaw gyro caused earth sensor quadrant loss indication and an abnormal shift to yaw gyro compassing mode.	CPU #1 failed.	AVHRR channel 3 change in calibration.	Thruster valve #9 exhibited high temperature excursions reaching peak of 44°C.	Temperature tunaway of buttery pack 2A after several days of erratic behavior.
Anomaly Time (hours)		4,125	7,130	7, 320	9, 280	11,130	11,520	12,600	14,780
Index		27	28	53	30	31	25	33	*

Renarks		Redundant unit selected but in the interim the CDU selected improper attitude control modes and the SSU lost sync.						Since yaw gyro also marginal spacecraft switched to yew gyro compass modej could mean up to 1" error in attitude per- formance.		
Corrective Action (if known)										Spacecraft went into tumbling, control could not be regained; battery voltage de- graded and spacecraft could not be contacted.
Mission Effect		Small	Small, battery stabilized after special charge re- gime.	Negligible, did not effect data collection.	No effect.	No impact on mission.	Loss of instrument.	Caused increasing yaw updates.	Small, causes 0.35* pointing error perturbation in roll and pitch during periods of moon interference.	End of mission.
Cause		Unknown .	Attributed to "soft" short caused by manufacturing techniques.	Possibly due to intermittent in recorder data handling circuitry.	Attributed to noise.	Degradation due to aging.	Thought due to blown fuse caused by a shorted filter capacitor on the +28V input power line.	Unknown .	Unknown.	Unknown.
Description	1.1 NOS-N	IMU power supply failed.	Battery lA temperature increase.	DTR 3A/3B intermittent high bit error rates.	HIRS patch power telemetry indicates low values; intermittent.	Pitch gyro bias shift.	AVHRR; loss of cutput.	Erratic behavior of pitch gyro.	ESA change in detector output for quadrant 1.	Backup IMU power supply failed; primary already failed-see anomaly #36.
Anomaly Time (hours)		16,270	16,920	17,230*	17,420	17,900	17,970	18,000	19,630	20, 800
Index		S	9	37	38	65	Q	7	42	‡

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Parathe				Digital data used from the platinum re- sistance thermometer which is the more reliable sensor.				Was found to have failed before launch.		Itam reported as failed pre-leanch, then worker wall fer over 300 hours, then failed evain.
Corrective Action (if known)									sass input voltage monitor limit was revised to 28.6v in moftware.	
Mission Effect		Megligible, moftware tables corrected.	Negligible.	Negligible.	Megligible, work- around developed.	Wegligible, actual transmitted power was normal.	Meyligible; not a problem with reder-	loss of telesatry point.	113	Loss of telemetry point.
Cause		Due to overlaid data from another tempera- ture sensor.	Possibly due to dap between corners and shield, optical properties of corners.	Possibly due to calibration error.	Attributed to transferring of material from thermostat points thus altering the gap.	Due to some 'an- emplained change in the power monitor.	Due to pre-launch error in establishing high limit.	Unknown.	Unk nown .	Unk nown .
Description	SEASAT	SAB anterna panel back- slide temperature sensor went from -47.5°F to +160.0°F while front side sensor stayed between 54°F to 44°F.	Madar altimeter showed o temperature points significantly varmer than expected.	Scan motor temperature from analog data 5* higher than same temperature point from digital data.	Altimeter thermostat cycled repidly.	L-band power map power monitor reading dropped abruptly from 773 watts to 643 watts.	SAR transmitter driver current out of specification.	SAR temperature monitor was discovered to be faulty.	mantor low limit setting does not reflect the IR drop in cable and is thus below the lower limit of the interface woltage required for operation.	21 Gm electrical temperature monitor failed.
Avone ly Tame (hours)		u	u	8	5 5 7	ž	%	2	2	su.
Index		-	~	n	•	•	•	•	•	•

Nomerke		Neder altimeter commanded off for 9 days.		Not known why inter- ference not also exhibited in rear quadrant.	VIRR was turned off for cooling and special monitoring implemented to turn it off before it reached 100°F.	Started operating again but failed permanently again 12 days later.				SEASAT falled before anomaly investigated.	
Corrective Action (1f known)				Work-arounds developed to disconnect roll-error signals during predicted interference period.							
Mission Effect		Negligible.	Negligible.	Small	Negligible.	Small.	Megligible, loss of 9 days of altimeter use.	No effect.	Negligible.	Unknown.	Small, work-arounds developed.
Cause		Unknown.	Unknown.	Caused by sun interference in right scanner of the horizon scanner.	Unknown.	Unknown.	Due to low voltage on unregulated bus.	Due to temperature monitor being mounted too close to heaters and both heaters on.	Suspected frequency shift in spacecraft downlink.	Unknown.	Due to sneak circuit between affected disable command and the VIRR shut- down command.
Description	SEASAT	Excessive radar altimeter baseplate temperature.	Glitch in altimeter current.	Large error in front scanner quadrant.	VIRM detector temperature approached upper limit of 95°F (was 94.3°F).	VIRN scan motor stopped rotating.	Altimeter low voltage monitor shut dow, the altimeter transmitter.	Altimater signal processor temperature monitor climbed 16°C in 7 minutes when the heater bus was turned on.	Ground station unable to hold solid lock on spacecraft receiver.	Migh data rate recorder low order channels bad; parity errors.	VIRR no voltage CICCUIT was found in disabled state after a command sequence to start the VIRR star metor.
Ancmely Time (bours)		\$0\$	935	060 .	1,000	1,510	1,515	1,560	1,660	1.85	1,970
Index		10	ä	2	a	2	23	2	11	•	•

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Nomarks				Similar problems on other Agenas.				Impact of low tempera- ture on instruments had been seen pre- launch.	symptoms seen in pre- launch tests.	OF POO		GE 13 ALITY
Corrective Action		,									Different voltage/ tempera- ture regime commanded.	
Mission Pffert	201010101010101010101010101010101010101		No impact.	Loss of mission: current drain re- duced power levels and drained batteries; S-band contact with spacecraft lost.	Negligible.		Negligible.	Caused intermittent incorrect operation in several instruments.	Megligible, recorder operated normally after it was left in playbach at the end of the pass and temperatures	reached 18°C. Negligible.	Negligible.	Negliçible.
	Cause		Due to loss of data loads, one occurrence due to bit error.	Design of slip ring assy prome to shorting.	Due to cold clouds.		The unit possibly breaks limit when looking at bright earth.	Unknown.	Unknown.	Unknown.	Unknown.	Unknown.
-	Description	SEASAT	Missing data in SMMM scan data; several occurrences.	Short carcuit in soler array slip ring assy.	Pitch and roll excursions.	SE S	1.27 micron spectrometer ACLDV read high limit error toggles in and out.	Observatory module temperature exceds specifications at low end (1s. too cold).	Tape recorder A did not respond to playbeck command and on next pass did not indicate reads.	atory Module 1 reference and con-	inquration changes. Battery 81 cell fail alert occurred.	1.27 micron spectrometer ACLDV out of limits.
Ances ly Time	(hours)		2,280	2,520	,		J	J	u	u	340	365
	Index		2	22	~		-	~	m	•	•	•

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Nema rito	Suspected prior to launch based on pre- launch pressure data.						ORIGINAL PAGE IS OF POOR QUALITY				
Corrective Action (if known)								Pump off times limited to less than 5 minutes, established rule to not turn-off pump under loads conducted ion pump characterisation tests.			
Mission Effect		Megligible.	Megikatble.		Megligible, did not degrade MTG per- formance.	Megligible, redundant thermostat used.	Negligible, temperatures stabilised ok.	Sme 1 1 .	No effect.		
•		Unknown.	Due to a strong and variable gravity gradient torque near periapsis.		Due to leakage of games into the 4cc pressure transducer reference cavity.	Due to 1 of 2 series thermostats failing closed.	Temperature predictive model not based on flight battery data (based on pre-production procetype batteries) and was in error.	Unknown.	Due to a combination of increased viscous friction of the throttle valve lubricant, and unbalanced pressure differential across the throttle valve bellows under cruise.		
1	VIKING OMBITER 1	Two to 5 db degradation in either the NF system or command detector unit.	Ges leak in roll axis.	VIKING LANGER 1	Telemetry indication of reduction in internal pressure within RTC-1.	De-orbit feedline heater thermostat duty cycle changed.	Battery temperatures predicted to increase by 15° but increased by 40°.	GOME ion pump current turn on translant.	Valve drive amplifier power 60% greater than recorded in pre-launch checkouts.		
-	(a poet)	15,575	19,600		J	ŭ	u	·	2,000		
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Neerks		ORIGINAL HAMP IS								
Corrective Action (if known)		Mode control logic line drivers "on" continuously for pertinent modes.	Self correct by cycling selsmometer.	Corrective commands transmitted.	Cycle ion pump off and on for I minute during atmospheric analysis ex- periments.	Vibrate GOME shuttle while metering; "level full" signal sub- sequently received.		Smed different uplink sweep but still recurred.		
Mission Effect		Megligible.	Negligible.	Negligible.	Resulted in operations with a degrading high voltage mource.	Negligible.	Megligible.	Megligible.	Negligible.	
Censo		Possibly due to a short in a 100 obm resistor or a senattive IC chip causing coupling between logic gates or an intermittent short.	Possibly due to system transients.	Due to control sequence containing an insufficient boom command to free the boom restraint latch pin.	Due to arcing/corona.	Unknown.	Due to short from a small metallic particle in cable insulation or partial delamination of the cable insulation.	Attributed to loss of receiver sen- sitivity or spurious lock on some other signal or NFI.	Unknown.	
Description	VIKING LANDER 1	UMF transmitter operated in 1 wat mode instead of the planned 30 watt mode.	All amplitude data in the seismometer data stream went to sero.	Surface Sampler (SSCA) Latch pin Jemmed.	Veriations in GOM ion pump current from day to day.	GCMS "livel full" signal not received.	Surface Sampler "no-good" during excavations on several occasions.	Maceiver 82 did not lock-up during down- links for 14 hours.	Double execution relay link amomaly during orbiter playback of lander data.	
Ancesty Time (hours)		000 .	•, 000	900	6,230	009.	•,720	12,500	13,950	
Index		•	-	•	•	91	=	2	13	

Reserts					Caused drop in SMR and occasional loss of telemetry signal.		Caused a spacecraft smargency.		Lost 2 pounds of gas; spacecraft commanded to roll-drift mode to conserve the little remaining gas.	
Corrective Action (if known)			Receiver not used when temperature exceeded 67*F.		Changed ground operations software.		Cogrected via commands.	Commanded yaw turn to clear jet.		
Mission Effect		No effect, wince instrument had already run out of helium.	Negligible but intermittent problem.	Can still acquire wind data but accuracy degraded.	Negligible .		Small offect.	Megligible.	Negligible.	This anomaly and anomaly 03 caused depletion of control gas and spacecraft
Ceuse		Due to soil splatter which may have pre- vented sealing of the test ceil, or ceil drain valve may have failed open or valves used to sample head space que may have failed.	May be manifestation of anomaly 012.	Unknown.	Unknown.		Due to timing offset between Processor A and B.	Unknown.	Unk nown.	Unknown.
Description	VIKING LANDER I	Biology chromatograms had no peaks.	Unexpected 6db decrease in Receiver 02 AGC.	Open circuit in wind sensor 82.	Telemetry DAPU block coder clock changed phase by 180°.	VIKING ONBITER 2	During planned switch from Processor B to A, uncommended switch to low-qain antenna and single subcarrier mode occurred.	Leak in yaw axis attitude control jet.	Major leak developed in roll axis; continued for 2 deys, then intermittently.	Leak developed in redundant MCS.
Ances ly Time (hours)		14.290	17,000		,		17,40	18, 800	21,170	21,170*
Index		*	2 1	*	7.1		~	~	•	•

Remarks				Moise had been seen in p.e-leunch tests.		Pre-launch value was			
Corrective Action (if known)							Recovery plan developed but not clear what it did or whether it was needed.		
Mission Effect		No impact.	No impact.	No lampact.	No impact.	No impact; continued throughout.	Negligible	Megligible, 3 other channels available.	No impact.
S. C.		Possibly due to base ring latch mech- anism obstructing the bioshield cap ring during separation.	Due to coupling into Campus tracker and lack of roll filtering in soft-ware.	Due to "off" impedance of the resistance type transducer being in excess of 130,000 ohms.	Unknown.	Unknown.	Probably due to electrical problem.	Due to low frequency noise or vibration.	Possibly due to tampe relation- slip duries record/ playback.
	VIKING LANDER 2	Spacecraft disturbance.	x and R gyro bias erratic and did not stabilize.	Command detactor in phase integrator noisy when off.	Terminal descent valve driver amplifier current 20% higher than seen in tests.	Metaorology ambient temperature sensor noise increased such that the difference between the reference and ambient tempera- ture was 20° relative to 10° expected maximum.	GCMS LPA carriage atrobe light failure.	Terminal descent landing redar experienced 2 periods of false lock.	Loss of bits during tape recorder play- back on Track 4. reverse direction.
Aronally Time	(Barrow)	2,300	2,300	2, 300	2,300	2, 300	3,450	6, 590	
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Penazrite		Tape recorder apparently turned-off early due to GOMS "data ready" signal going inactive early.		Not investigated since surface sampling terminated at about this time.	Similar occurence happened on Viking Lander I a year before.				Occurred three times on Voyager I and several times on Voyager II.
Corrective Action (if known)			Corrected via software.					Reconfigured via ground command.	On-board software modified.
Mission Effect		Small; slight loss of data but subsequent operation normal.	Small; slight loss of data.	Small; boom achieved commanded positions in subsequent operations.	Caused loss of Lander II downlink; Lander II had to be operated via a relay link with a. orbiter.	Operations with Lander II were terminated.		No effect.	No effect.
Cause		Caused by fast noise glitch.	Due to timing conflict.	Unknown.	Probably due to a failure in the low woltage supply/ woltage regulator of the TWTA.	Unknown.		Possibly due to extending boom causing motion in speceraft and on-board computer switched thrusters to correct motion.	Possibly due to incompatibility of the turn rate to position gain and incremental rate dumping with the magnetometer/science boom higher order structural frequencies which causes the number of roll pulses generated to exceed the pulse count limit.
Description	VIKING LANDER 2	Approximately 20 minutes of GCMS organic analysis data missing from tape on playback.	Met instrument data missing from relayed data transmission.	SSCA boom stopped assmuth travel at about 39.	Tern 02 failed.	Computer failed.	VOYACER 1	Unexpected on-board command to switch from primary pitch and yew thrusters to redundant thruster branch when magnetometer boom was extending.	Unexpected on-board command to switch from primary roll thrusters for redundant thrusters branch during first roll turn of spacecraft.
Ancmaly Time (bours)		10, 150	11,930	13,630	18,190	39,550		u	9
i de		•	07	=	2	13		-	~

Anomal tes

Renarks		Maneuver planning implemented to conserve hydrazine.	Found when both the wide angle and narrow angle televisions did not respond to filterwheel stepping anomalies.					Mee commended to and left in the clear position for the Jupiter encounter.	
Corrective Action (if known)					Operational procedure instigated to use low power mode whenever possible and minimize high power mode.	Processor A clock was reset from the ground to eliminate the 48 second offset.	Gyro conditioning tests instituted at six month intervals.		Software modified on Voyager II.
Mission Effect		Small, required more hydrazine use than planned for all maneuvers.	Megligible; on-board software modified to preclude use of falled. memory location.	Megligible, scan platform became unstuck and operation favorable.		Small.	Sme11.	Negligible.	Megligible.
Cause		Due to thruster exhaust plumes impinging on portions of the spacecraft.	Unk.xown .	Possibly due to debris (possibly from assembly at JPL) in azimuth gears and later crushed by gears.	Attributed to early wearout of 1 or more MSC 3005 transistors in each of the amplifiers.	Believed caused by extra counts picked up by a ripple counter due to a time phasing problem.	Attributed to low capture loop gain.	Unknown.	Due to 40 spurious power-on reset signals which were probably caused by Joynan radiation.
Description	VOYALER 1	Thrust velocity &V 20% less than expected.	The 12th bit of the FDS "A" memory failed high.	Commanded scan platform azimuth sl@w was not successful.	S-band high gain antenna driver solid state amplifier exhibited degraded NF power output and decreased input current in the 20 watt high power mode.	Commands generated by CCS processor A occurred 48 seconds early.	Gyro A pitch axis showed abnormal drift rate and drift rate-rate of change.	Photo polarimeter analyser wheel sticking.	FIS clock lost 8 seconds.
Anomaly Time (bours)		<u>8</u>	2,400	₽,100	•	10,920	11,660	12,770	13,100
Index		e	•	•	•	•	•	•	01

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Reserts		Contact was lost since antenna was not pointing towards earth.				Reactivated, but problem recurred three months later.		
Corrective Action (if known)		Spacecraft was commanded through a side lobe to switch to the low gain antenna and contact was thus re-established; re-acquisition commands were then transmitted.		Uplinked software to store slew commands and re- execute them every 48 seconds to reposition platform if creep has occurred.	Software modified to permit operational work- around.			
Masion Effect		Created a spacecraft emergency.	Not serious; loss of telemetry point.	Negligible.	Some loss of sen- sitivity.	Negligible	Instrument degraded to some extent.	PDS memory B not usable; operations limited to PDS memory A.
Cause		Unknown.	Possibly due to partially open circuit associated with the series or parallel padding resistors.	Probably due to cable wind-up which can apply enough torque to pull the scan platform.	Possibly due to transistor leakage caused by 2 or more Delrin insulating sleeves decomposing due to high intensity radiation.	Possibly due to internal short or bad connection.	Possibly due to 1 of 4 transistors in a transistor bridge in the filter wheel stepper motor circuit shorting out.	Most probable cause is that a CD 4049 integrated circuit inverter failed high or its input shorted to low.
Description	VOYAGER 1	Star tracker locked on Alpha Centauri instead of Canopus after a series of turns.	X-band feed temperature transcheer intermittently produces saturated readings.	Scan platform executed elevation also commands properly but then crept out of commanded position.	Star tracker #2 could not be commanded into come angle settings 3,4 or 5.	Plasma instrument stopped transmitting usable data.	Photopolarimater filter wheel stopped.	Bit 4 in all BK words of PDS memory B stays high.
Anomaly Time (hours)		19,250	25, 560	25,730	36,060	27,000	98,08	35, 700
Index		Ξ.	2	£1	4	15	9	71

Remarks	The heater was originally installed unly to evaporate condensation during launch.	Science boom deployed to within 0.2° of latching but did not latch; later it was found to be within 0.06° of the correct position.	Not known whether Byro Amps B did not activate or whether the telemetry indication was wrong.	ORIGIN OF PO		er is Llity
Corrective Action (if known)	The flash off heater was used to raise the temperature and halt the degradation.				Star tracker softwere mcdified.	
Mission Effect	Megligible.	Negligible.	Megligible, used redundant unit.	No effect.	Not serious. Negligible.	No mission effect.
Cause	Unknown.	Probable cause is debris in the folding strut hinge or insufficient drive in the folding strut.	Scame evidence that a transistor in the output switching portion of the pyro switching unit failed.	Due to faulty teleme- try caused by combi- nation of an un- balanced grounding design in the pyro switching unit and that the superzip squibs short to ground during fixing.	Due to outgassing. Star tracker low	act due to a flurry of bright particles. On-board processor had improperly positioned the spacecraft for the search due to processor switching relationships.
Description	VOYACER 1 Crystalization and hardening of the motor dampers on the Nichelson motor in the infrared spectrometer and radiometer.	WOYAGER 2 The microswitch on the folding strut did not provide the signal which indicates full deployment of the science boom.	Pollowing the Melease FTG Boom command, no indication was received that the Pyro Amps B had activated.	Pollowing the spacecraft launch vehicle separation command, an indication was received that both pyro "superzip" strands A and B were activated.	Short pitch and yaw disturbances. Large attitude ex-	and yaw. Sun search required 34 hours instead of predicted five minutes.
Anomaly Time	,	٠	v	•		·
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Nemarks		Switch occurred because the computer "thought" the gyros had failed when their data did not match.		May be related to anomaly 85.	Maneuver planning implemented to conserve hydrazine.	Occurred five times.	OF	POOR C
Corrective Action (if known)						On-board software modified.		
Mission Effect		No mission effect.	Negligible, second attempt successful.	Negligible.	Small, required more hydratine use than planned for all maneuvers.	No effect.	Degraded instrument to some extent.	15 of 243 engineering telemetry points were lost.
Cause		First occurrence due to the gyros inability to keep up with booster motion and the second due to high vibration.	On-board computer did not give the command because the second computer was switching memory banks at the same time and the software inhibits any maneuver when such switching occurs.	Probably not a hardware problem.	Due to thruster exhaust plume impingement on portions of the spacecraft.	Possibly due to extending boom or incompatibility of the turn rate to position gain.	Probably failed IC in either a multi- plexer or the motor step logic.	Most likely cause is a leaky IC at one of the two input multiplexers.
Description	VOYAGER 2	The on-board computer unexpectedly switched from the primary to back-up gyros.	First attempt to eject science cover un- successful.	Spacecraft went into gyrations.	Thrust velocity Av less than expected.	Unexpected on-board command to switch from primary to backup thrusters.	Photopolarimeter analyzer wheel stuck in position 2.	Incorrect telemetry data from PDS engineering data commutator tree switch #3.
Anomaly Time (hours)		.	u	120	0.00	240	592	815
Index		•	6	6	10	n	2	ជ

Remark						
Corrective Action (if known)			Operational procedures instigated to use low power mode whenever possible and minimize high power mode.		Flash-off heater used to provide warming cycles for the instrument.	
Mission Effect		Small impact. The instrument is fully functional in slow scanning mode, but accelerated stepping mode is no longer possible because the lowered resistance would allow excessive current flow.	Smell.	Not significant.	Negligible.	Loss of receiver #1, backup unit #2 available but had an anomaly (#19) and Radio Astronomy Experiment could be used as a receiver if necessary.
Cause		Due to one of the motor winding logic file; fore changing states, possibly due to a transient from x-band turn-on.	Attributed to early wearout of 1 or more MSC 3305 transistors in each of the amplifiers.	Due to a design problem that was left uncorrected due to schedule and cost consideration.	Due to crystal- lization of the silicon rubber of the motor damper and beam splitter mounts.	Possibly due to a problem in the receiver's power supply.
Description	VOYAGER 2	low energy charged particle instrument motor winding drew too much current and overheated the instrument.	S-band high çain antenna driver solid stat? amplifier exhibited degraded RF power output and increased current input in the 20 watt high power mode.	X-band TWTA high gain antenna drive telematry monitor erratic when receiver goes in or out of lock.	Infrared spectrometer misalignment and increase in instrument NER.	RFS #1 failed.
Anomaly Time (hours)		7, 800	1,940	2,420	2,570	5,500
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Time		;		Corrective Action	į
 (bours)	Description VOYAGER 2		Alselon Elfect	(11 Allows)	
6, 190	RPS Receiver #2 lost its capability for adjusting for the effects of the Earth's rotation on the uplink signal.	Due to failed capacitor in receiver's tracking loop.	Negligible.	Uplink frequencies adjusted to match what the receiver "thought" they should be.	
15, 700	Heating of 1 side of the spacecraft bus when the spacecraft maneuvered off the sun line or when power consumption changed.	Unknown.	Small.	Contingency plans developed.	
16, 500	During Jupiter encounter, radiation built-up a charge on the spacecraft which dissipated through electro-static discharge.	Unknown.	The command receiver, wide angle television, photopolarimeter, and Cosmic Ray Experiment were damaged by Jovian radiation and electrostatic discharge caused frame start resets in the wide angle television.		
16,660	HET 2 Telescope guard circuitry hung-up in "high" state and causes loss of detector counts in channels 12,13,14, and 15.	Due to failure in the guard ECL circuit; either 1 of 3 transistors or a shorted capacitor.	No effect since instrument commanded to lower gain state.		
16,850	Photopolarimeter filter wheel skips every other position.	Possibly due to a failed part; probably related to anomaly file.	Negligible, information still usable.		
16,850	Cosmic Ray Experiment probably lost a commutator.	Possibly due to a weak part failure; probably relaind to anomaly f21.	Redundant unit available.		
32,830	Loss of the 7th LSB in the upper 256 words of FIS Memory B.	Due to failure of a lx 256 RAM, CD 4061A (a hybrid integrated circuit)	Small, PDS operations limited to Memory A.		

Newths	Eventually elevation motion normal but azimuth motion re- stricted.	Caused smearing of images.
Corrective Action (if known)	Platform unjammed by using motor at higher speed.	Corrected via moftware.
Mission Effect	Significant, scan platform stuck while the spacecraft was behind Saturn so this data lost.	Negligible.
Cause	Possibly related to wear of gears and a lubricant problem.	Due to tape recorder motion.
Description	VOYAGER 2 Scan platform azzmuth actuator stuck at 260° azimuth and 20° elevation.	Spacecraft attitude changes.
Anomaly Time Index (Nours)	15, 180	,
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APPENDIX B-2

ANOMALY CLASSIFICATIONS THE STANDARD APPROACH

ANOMALOUS INCIDENT CLASSIFICATION CODES, STANDARD APPROACH

I. Mission Subset

- U. Unsuccessful Launch
- S. Spacecraft with No Anomalies Reported

Spacecraft with Anomalies Reported

II. Mission Term

- L. Long Term
- S. Short Term

III. Mission Phase

- L. Launch and Acquisition
- O. Orbital (Steady-State)
- Q. Unknown

IV. Mission Effect

- 1. Negligible
- 2. Non-Negligible but Small
- 3. 1/3 to 2/3 Mission Loss
- 4. 2/3 to Nearly Total Mission Loss
- 5. Essentially Total Mission Loss
- U. Unknown

V. Spacecraft Subsystem

- a. Timing, Control and Command
- b. Telemetry and Data Handling

- c. Power Supply
- d. Attitude Control and Stabilization
- d# Propulsion
- e. Environmental Control
- f. Structure
- g. Payload (Experimental and Scientific)
- h. Unknown

VI. A. Incident Type

- E. Electrical
- M. Mechanical
- O. Other
- U. Unknown

VI. B. Incident Type

- C. Catastrophic Part Failure
- O. Other Part-Related Incident
- N. Non-Part-Related Incident
- U. Unknown

VII. Incident Cause

- A. Assignable
- N. Non-Assignable
- U. Unknown

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APPENDIX B-3

ANOMALY CLASSIFICATIONS ADDITIONAL CHARACTERISTICS

ANOMALOUS INCIDENT CLASSIFICATION CODES, ADDED CHARACTERISTICS

I. Anomaly Cause

- a. Space Environment
- b. On-Board Software
- c. Design, Other
- d. Quality Control/Workmanship
- e. Contamination
- f. Catastrophic Part Failure
- g. Catastrophic Circuit Failure
- h. Catastrophic Component Failure
- 1 Catastrophic Black Box Failure
- j Unknown

TOTAL

XI. Anomaly Type

- S. Systematic
- W. Wearout/Aging/Depletion
- C. Chance
- G. Glitch
- U. Unknown

TOTAL

XII. Testability

- Y. Yes
- N. No
- M. Maybe
- U. Unknown

TOTAL

XIII. Source

- 1. Part
- 2. Circuit/Subassembly
- 3. Component
- 4. Black Box
- 5. Subsystem/Interface
- 6. Interaction
- 7. Unknown

TOTAL

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APPENDIX C

PERFORMANCE SUMMARIES

APPENDIX C

PERFORMANCE SUMMARIES

This appendix presents spacecraft and major spacecraft subsystem performance summaries in graphical form. Appendix C-1 contains one chart per spacecraft, although some charts run to two or even three pages. Each chart identifies all of the spacecraft's subsystems and payloads. It further identifies each anomalous component within the subsystem or payload. All anomalies are identified on the chart at the time they occurred. Those that caused complete failure of the associated component are denoted by a circle; all others by triangles. Anomaly indications in the "Unknown Time of Occurrence" column are of essentially negligible mission effect and occur at some undocumented time(s) or are present throughout the mission. Survival times are also given for each subsystem and anomalous component. When an anomalous component is redundant, the survival times are given for the redundant units even if they have no anomalies. Other components without anomalies are not listed.

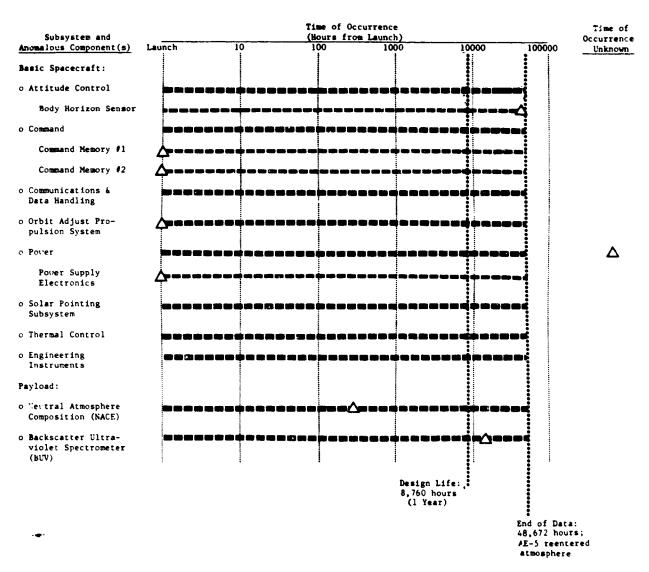
Appendix C-2 arrays significant anomalies and failures by major spacecraft subsystems. Since each program has a somewhat different breakout of subsystems, we have standardized on the eight defined in subsection III.A.5. In addition to being ordered by subsystem rather than spacecraft, this appendix differs from Appendix C-1 in two ways. First, only "significant" anomalies are included. These are generally those categorized as having a mission effect code of 2 or greater (see subsection III.A.4) although all anomalies in redundant units, whose mission effect is negligible because of the redundancy, are also included. The second

major difference is that time, rather than being plotted in hours as in Appendix C-1, is plotted in terms of spacecraft design life. For the major subsystems (Timing, Control and Command; Telemetry and Data Handling; Power Supply; Attitude Control and Stabilization; and Payload) an entry is made for each spacecraft whether or not it had significant anomalies in the subject subsystem. Note that an entry of "No significant anomalies" means on that subsystem only. The Structure subsystem does not appear since there were no significant anomalies in this subsystem in this update. Furthermore, for the Propulsion and the Environmental Control subsystems only those spacecraft are listed which suffered significant anomalies in these areas.

APPENDIX C-1

SPACECRAFT

PEPFORMANCE SUMMARY FOR AE-5



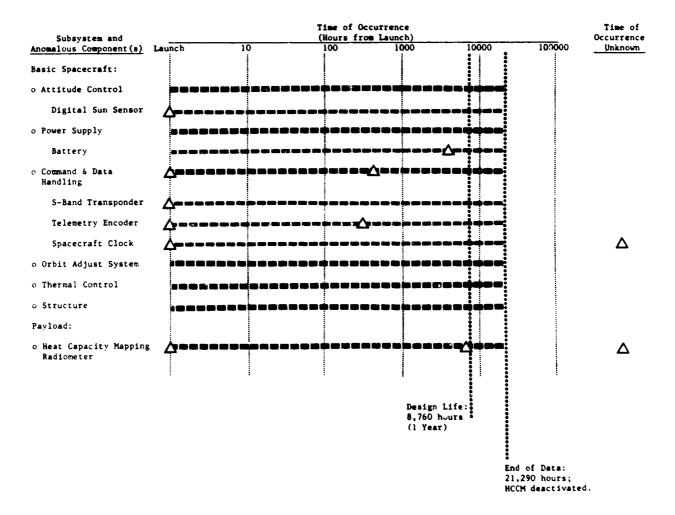
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indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

A indicates that this anomaly is not a failure.

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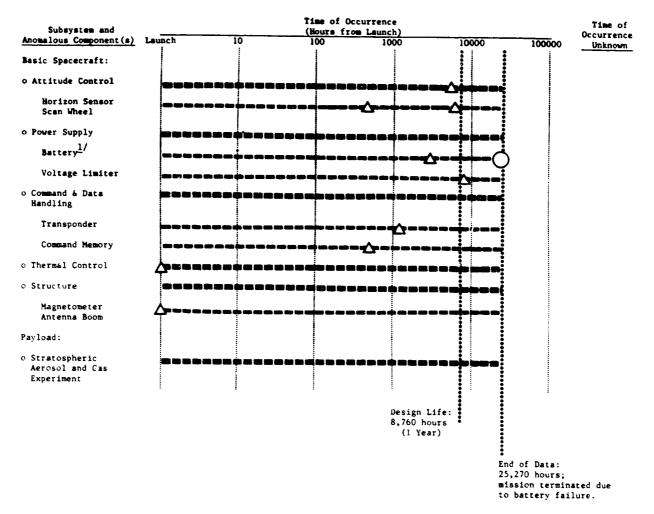
PERFORMANCE SUMMARY FOR AEM-1 (HCCM)



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indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

PERFORMANCE SUBMARY FOR AEH-2 (SAGE)



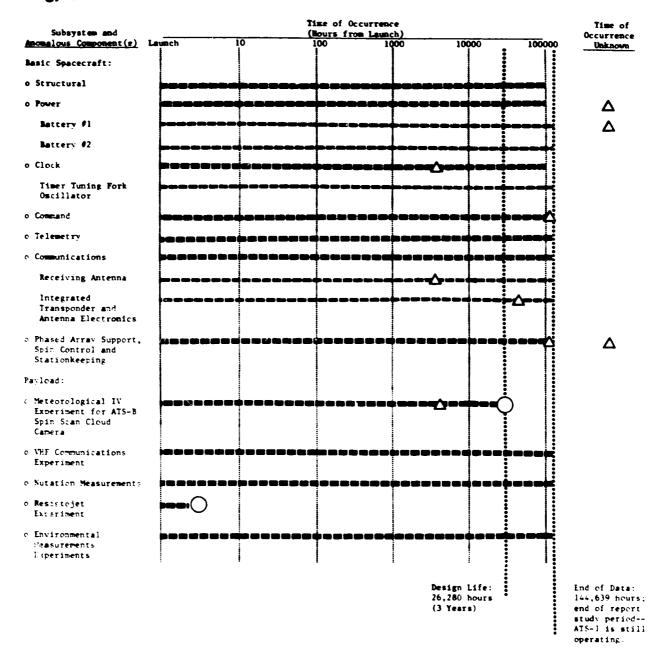
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indicates that that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or the component unusable.

 Δ indicates that this anomaly is <u>not</u> a failure.

^{1/} Battery capacity started to degrade at 2050 hours and failed completely at 25,270 hours.

PERFORMANCE SURGARY FOR ATS-1



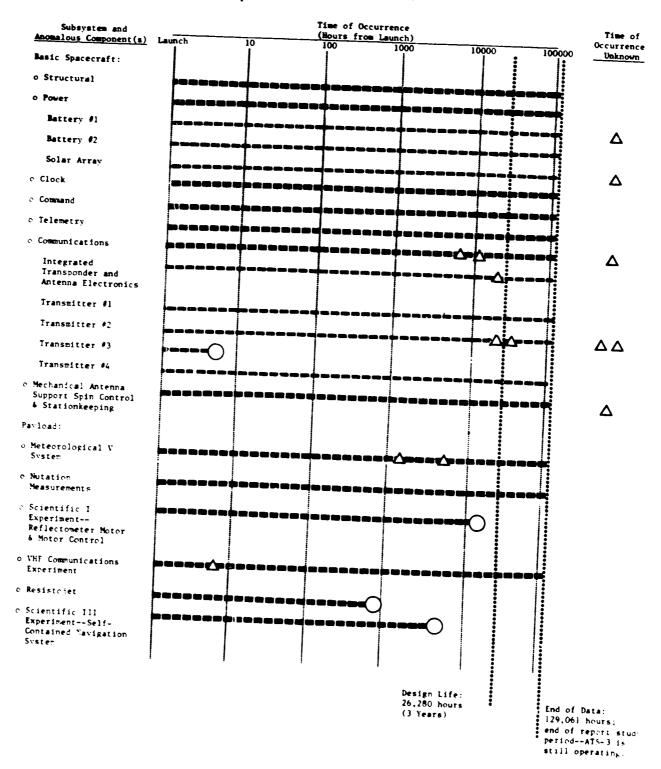
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A indicates that this anomaly is not a failure.

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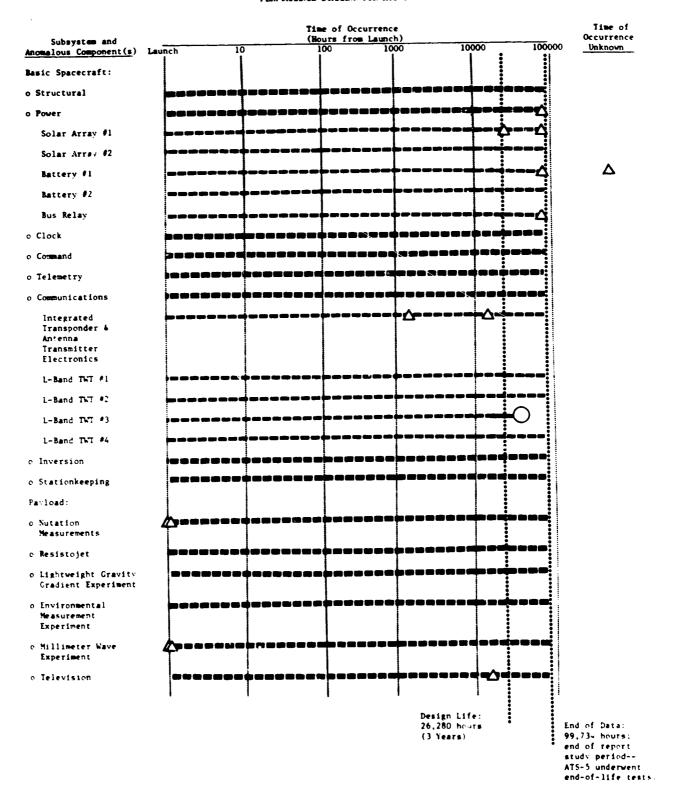
ORIGINAL PAGE 13 OF POOR QUALITY PERFORMANCE SUMMARY FOR ATS-3



Legend:

△ indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

PERFORMANCE SUMMARY FOR ATS-5



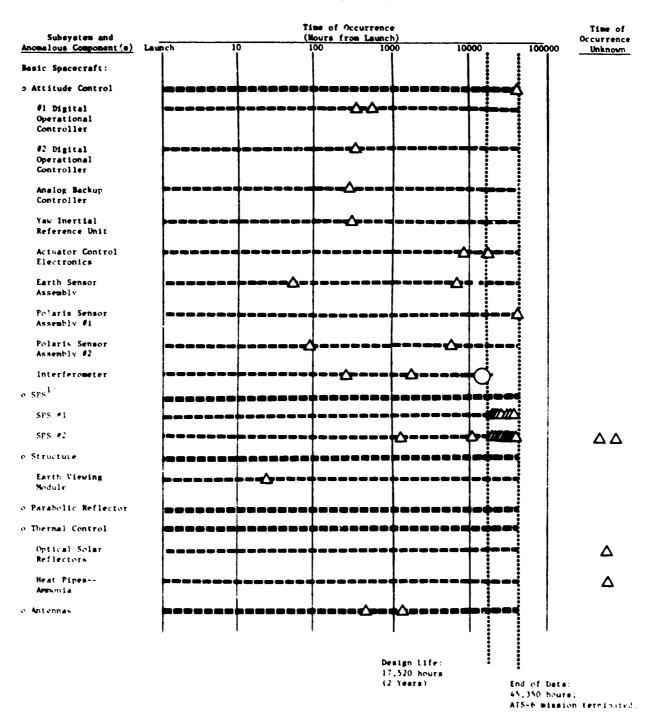
Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

△ indicates that this anomaly is not a failure.

200

PERFORMANCE SUMMARY FOR ATS-6



Legend

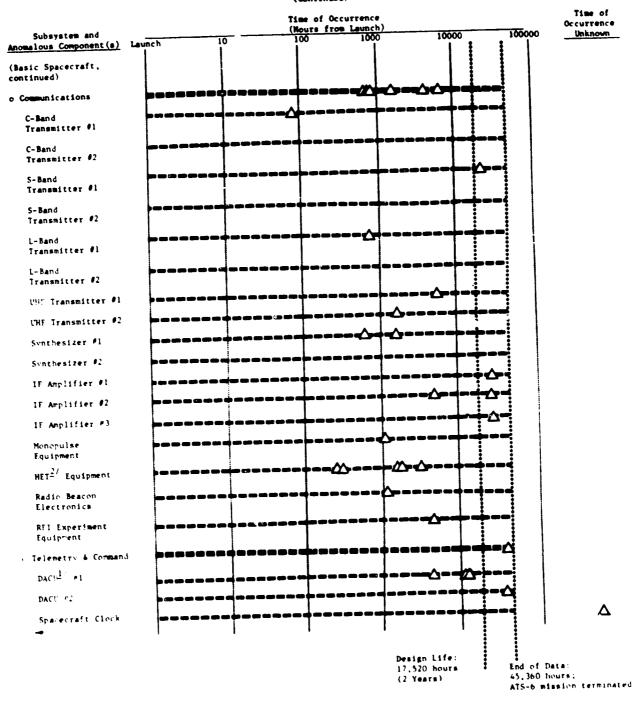
indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

A indicates that this anomaly is not a failure.

1 SPS . Spacecraft Propulsion Subsystem

ORIGINAL PACK 18 OF POOR QUALITY

PERFORMANCE SURGARY FOR ATS-6 (Continued)



Legend

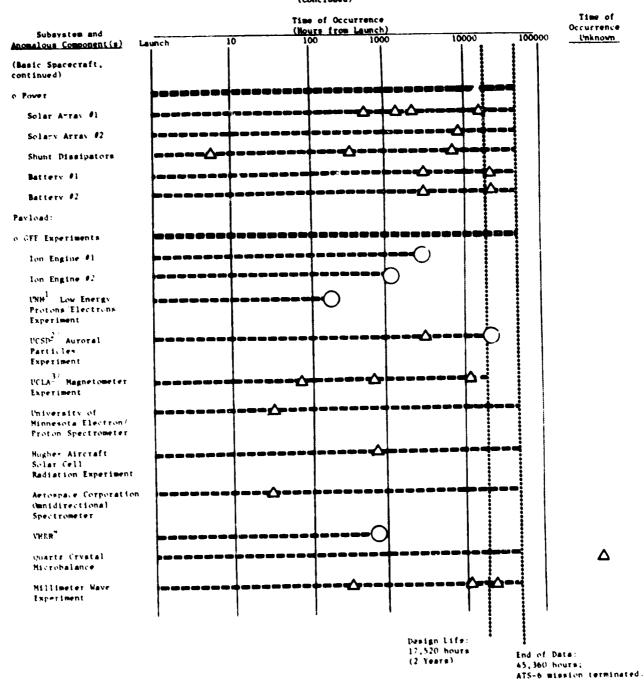
indicates this this anomaly is a failure, where failure is defined as the event that renders the subsistem and or

A indicates that this anomaly is not a failure.

1 DACL - Data Acquisition and Control Unit.

2/ HET - High Energy Telescope

PERFORMANCE STREAMY FOR ATS-6 (Concluded)

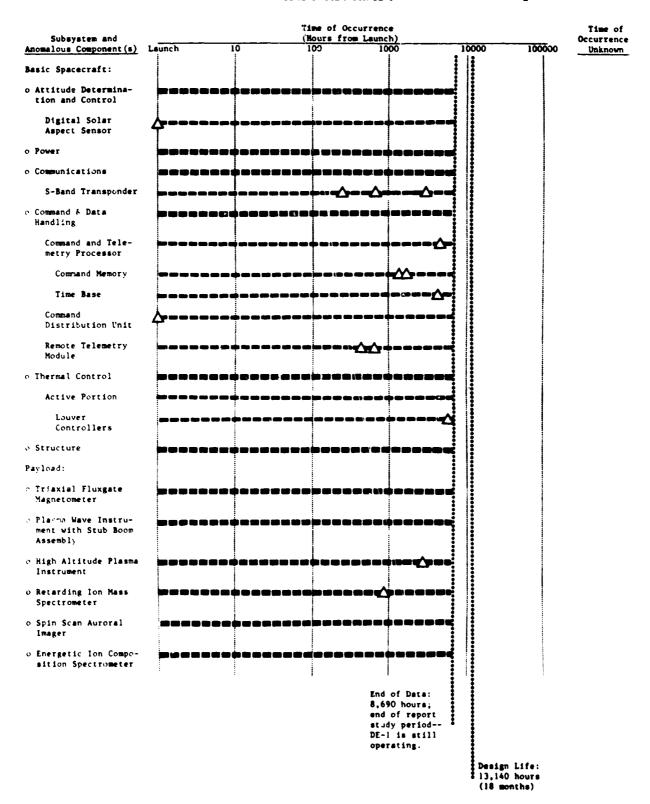


Legend indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

¹ UNN - University of New Mampahire.
2/ UCSD - University of California, San Diego.
3/ UCLA - University of California, Los Angeles.

VHRR . Very High Resolution Rediometer.

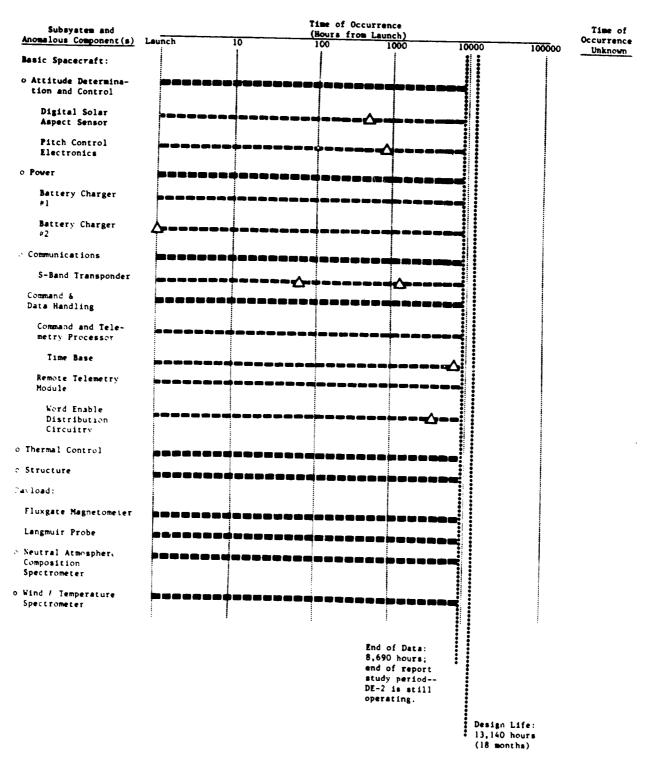
PERFORMANCE SUMMARY FOR DE-1



Legend:

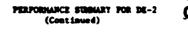
indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

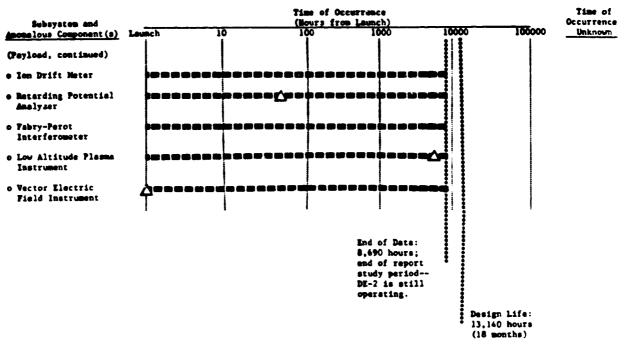
PERFORMANCE SUMMARY FOR DE-2



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

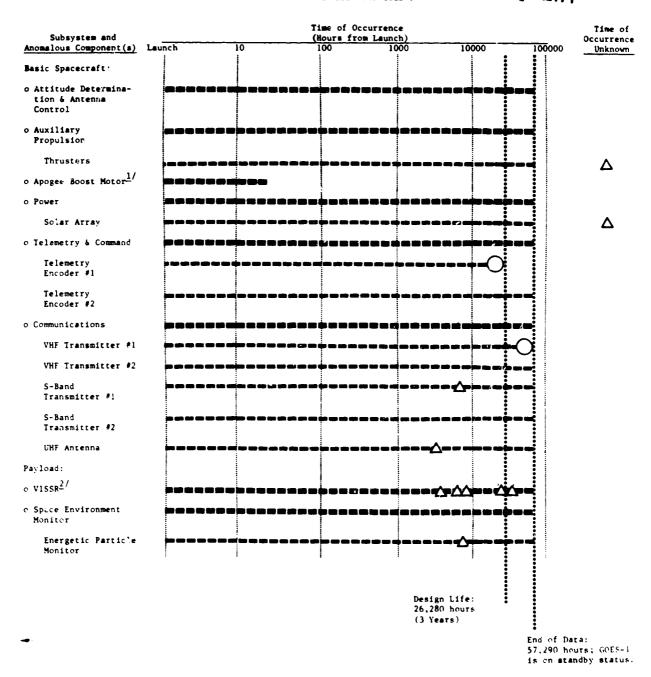




Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or

PERFORMANCE SUMMARY FOR GOES-1



Legend:

O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

The apogee boost motor is a one-shot device and has a normal lifetime of 24 hours

PERFORMANCE SUPPLARY FOR GOES-2 OF POOR QUALITY Time of Occurrence Occurrence (Hours from Launch) 100000 Unknown 10000 Subsystem and Anomalous Component(s) Launch 10 Basic Spacecraft: o Attitude Determination & Antenna Control o Auxiliary Propulsion o Apogee Boost Motor 1/ Δ o Power o Telemetry & Command o Communications UHF Receiver #1 UHF Receiver #2 S-Band Transmitter #1 S-Band Transmitter #2 Receiver #1 S-Band Receiver #2 o VISSR2/ Digital Multiplexer Payload: o VISSR o Space Environment Monitor Solar X-Ray Monitor Design Life: 26,280 hours (3 Years) End of Data: 42,670 hours; end of report study period--GOES-2 is

ORIGINAL PAGE IN

still semioperational.

Legend:

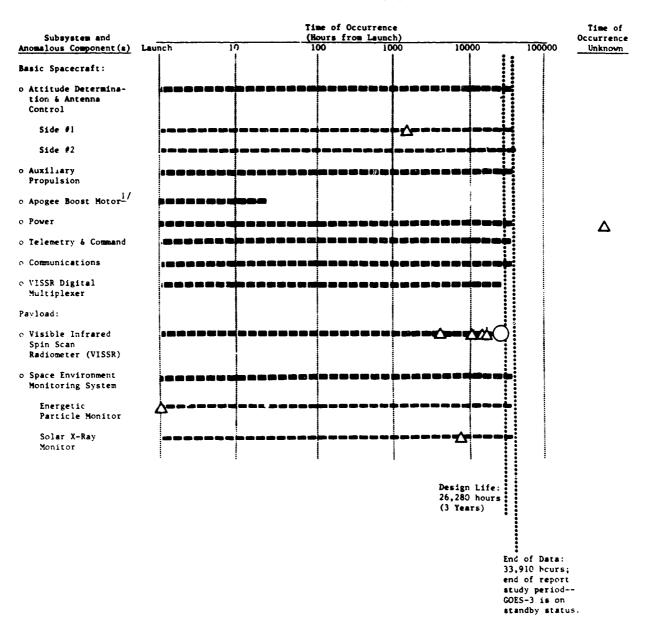
Oindicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

A indicates that this anomaly is not a failure.

1/ The apogee boost motor is a one-shot device at 2/ VISSR - Visible Infrared Spin Scan Radiometer

The apogee boost motor is a one-shot device and has a normal lifetime of 24 hours.

PERFORMANCE SUMMARY FOR GOES-3

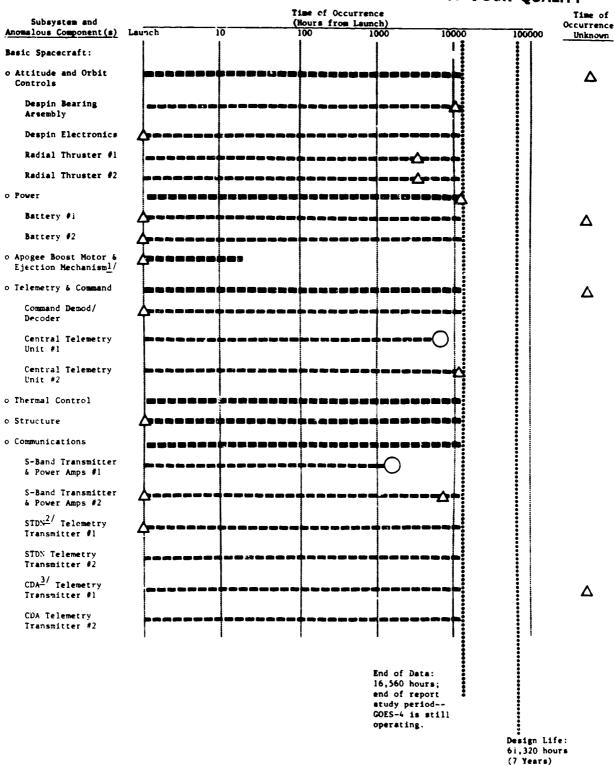


Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

\$\triangle \text{ indicates that this anomaly is not a failure.}

1/ The apogee boost motor is a one-shot device and has a normal lifetime of 24 hours.



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

△ indicates that this anomaly is <u>not</u> a failure.

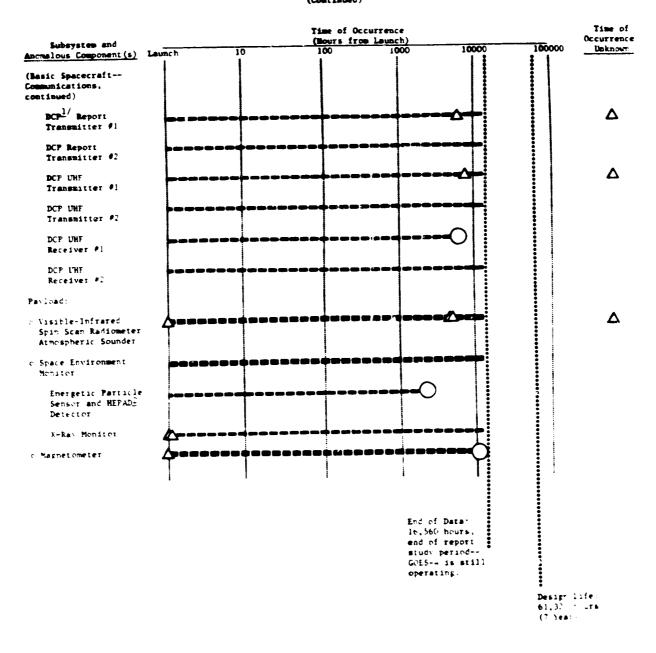
2/ STDN = Spaceflight Tracking and Data Network.

/ CDA - Command and Data Acquisition.

^{1/} The apogee boost motor and ejection mechanism is a one-shot device and has a normal lifetime of 24 hours.

OF POOR QUALITY

PERFORMANCE SURGARY FOR COES-4 (Continued)

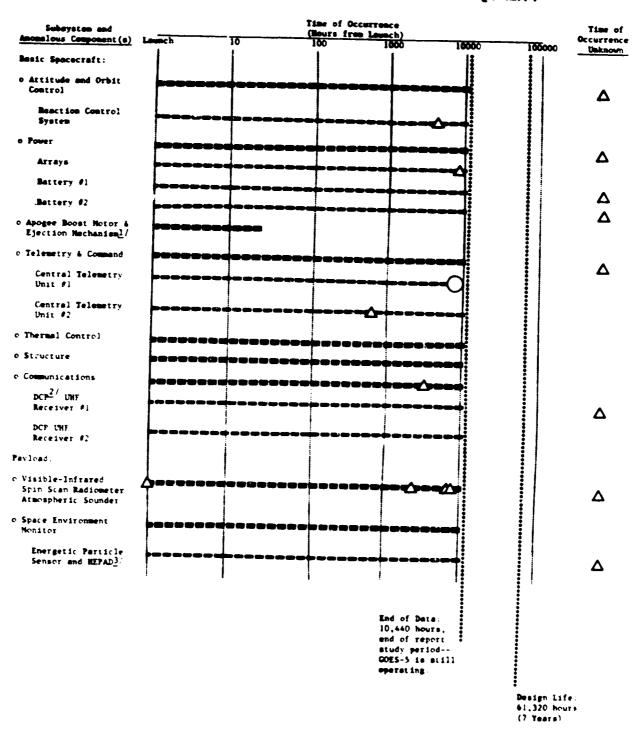


Leger.

Oundatates that this anomaly is a failure, where failure is defined as the event that renders the substant and/or component unusable.

^{1/} DCF = Data Collection Platform.
2/ MEFAL = High Energy Particle Detector.

ORIGINAL PAGE 18 PERFORMANCE SURGERY FOR COES-OF POOR QUALITY



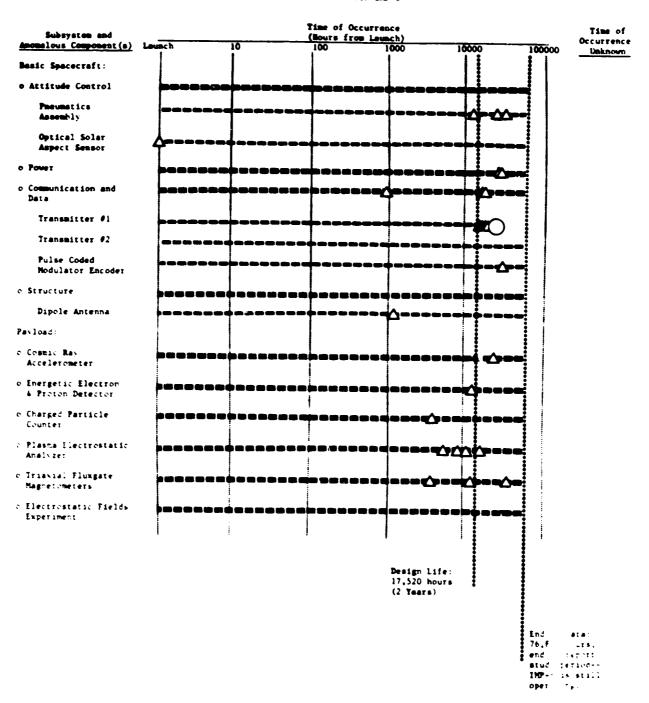
Legend

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or

The apogee boost motor and ejection mechasism is a none-shot device and has a normal lifetime of 24 hours DCP = Data Collection Platform.

MEPAD = Migh Energy Particle Detector

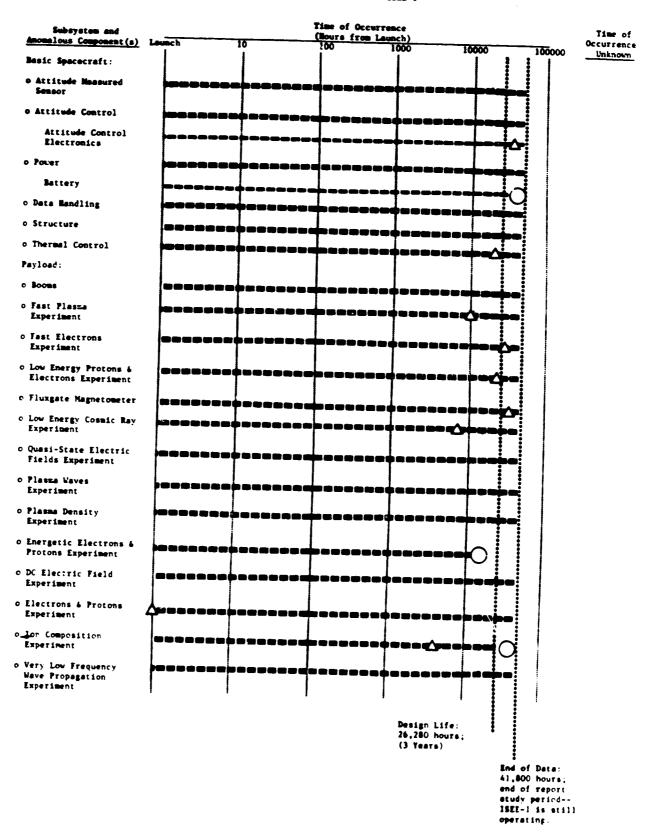
PERFORMANCE SUBMARY FOR LINE-8



Legend

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

PERFORMANCE SURGARY FOR 15EE-1

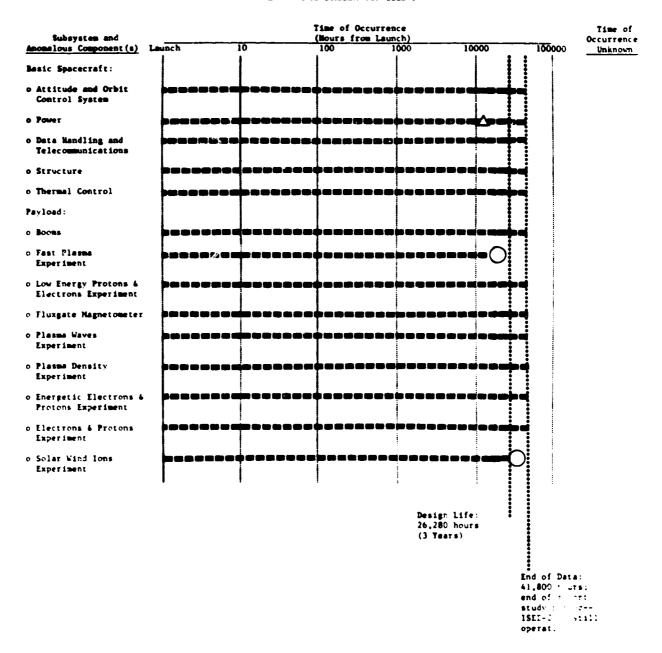


Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsister and/or component unusable.

 Δ indicates that this anomaly is <u>not</u> a failure.

PERFORMANCE SURBIARY FOR ISEE-2

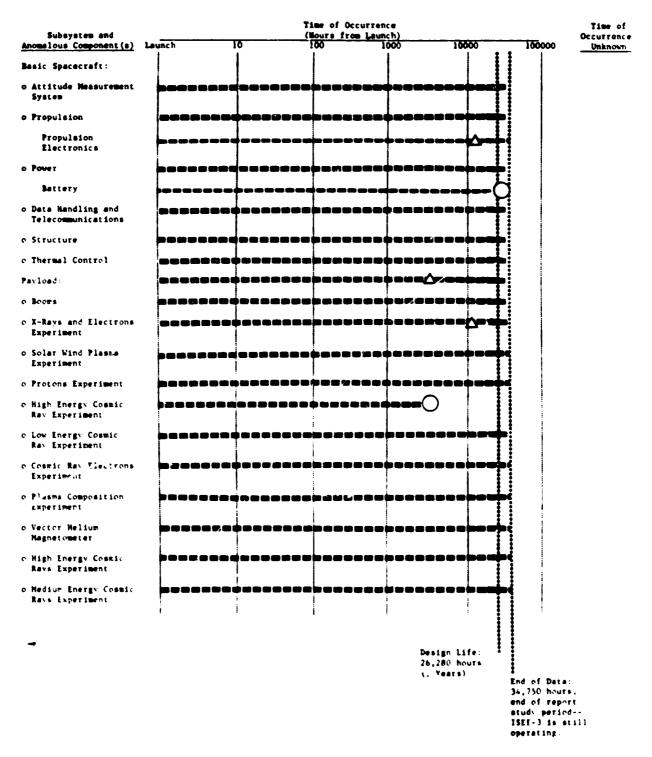


Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the some ster and or component unusable.

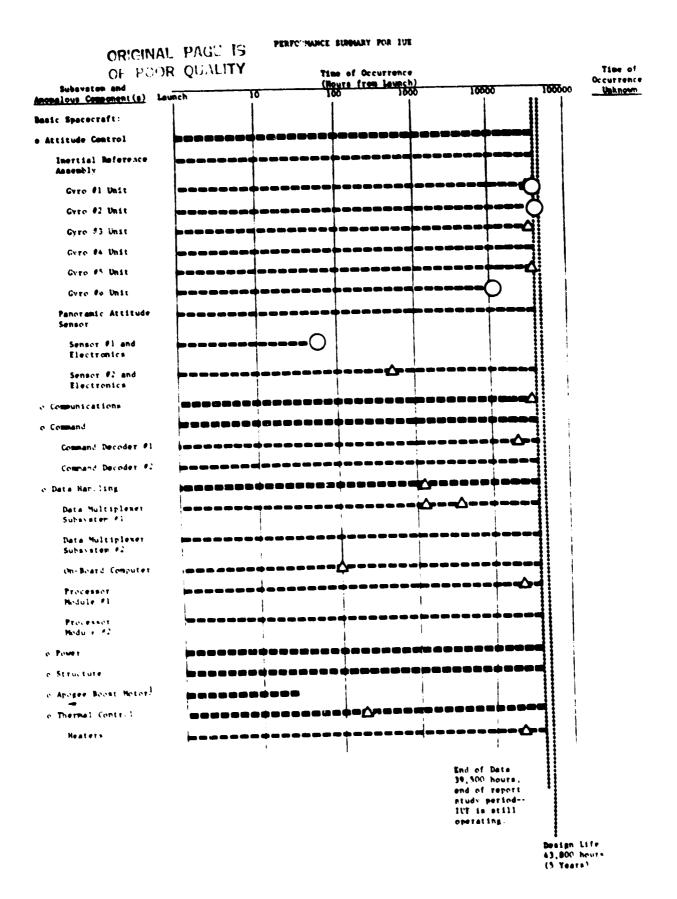
 Δ indicates that this anomaly is <u>not</u> a failure.

PERFORMANCE SURBARY FOR ISEE-3



Legen!

indicates that this anomaly is a railure, where failure is defined as the event that random the subsystem and component unusable.



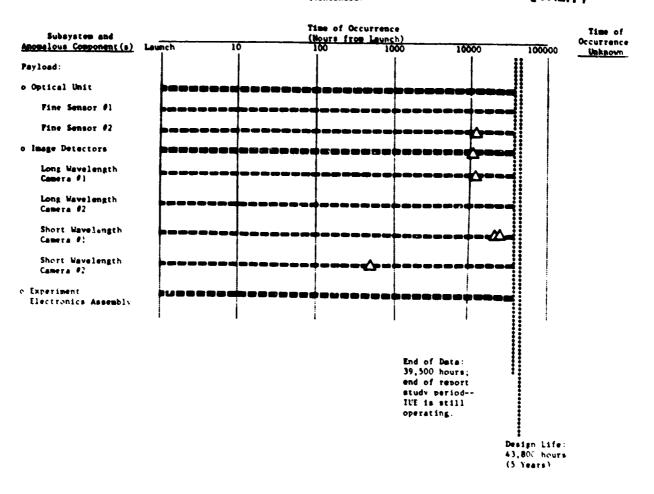
Legend

indicates that this anomaly is a failure, where failure is defined as the event that renders the autoviter and or component unusable

A indicates that this anomaly is not a failure

1 The apogee boost motor to a one-shot device and has a normal lifetime of 2s hours

PERFORMANCE SUMMARY FOR II. (Continued)

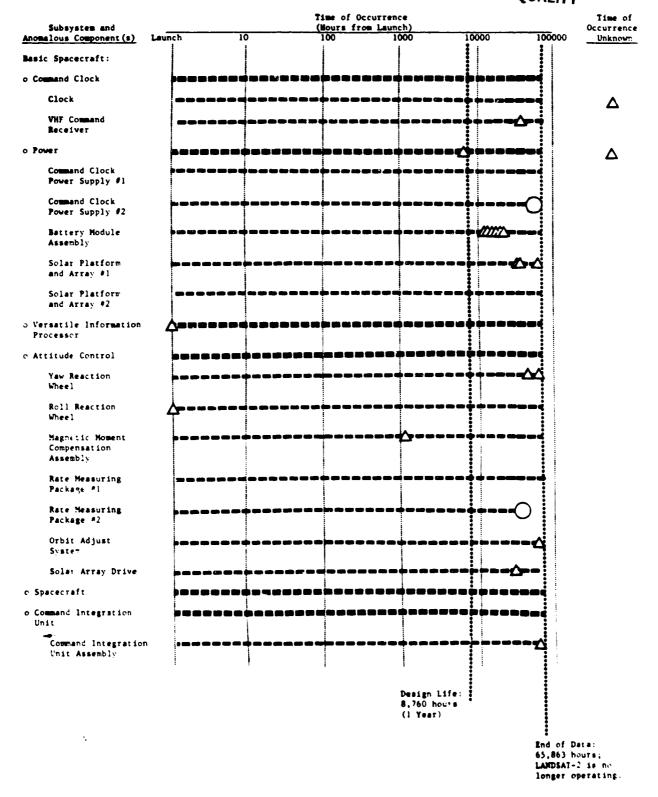


Legend

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

\$\triangle \text{ indicates that this anomaly is not a failure.}

PERFORMANCE SUMMARY FOR LANDSAT-2 OF POOR QUALITY



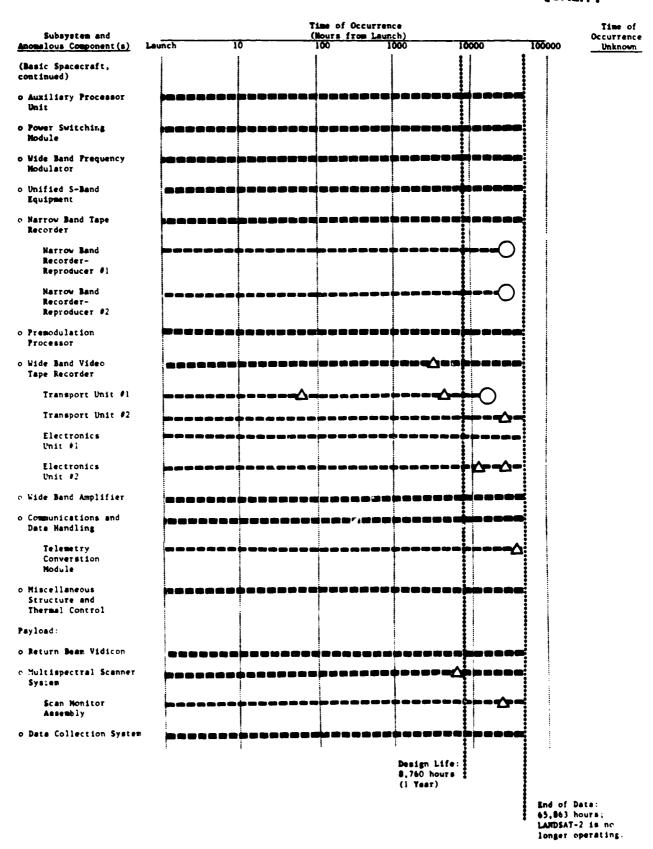
Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

 Δ indicates that this anomaly is <u>not</u> a failure.

PERFORMANCE SUBMARY FOR LANDSAT-2 (Continued)

ORIGINAL PAGE IS DE POOR QUALITY

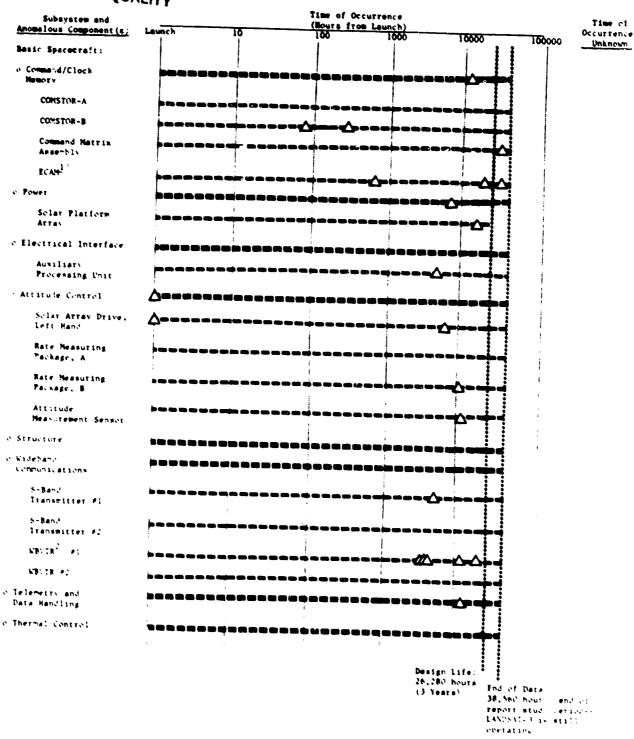


Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.



PERFORMANCE GLOBIARY FOR LANDSAT-3



Legend

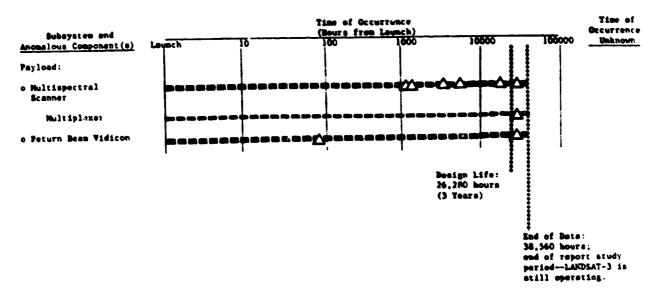
Oindicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable

Fr ECAM - ERTS Command Aussisars Memors

³ MBVTR - Wide Band Video Tape Recorder

PERFORMANCE SUBSIARY FOR LAWDEAT-3 (Continued)

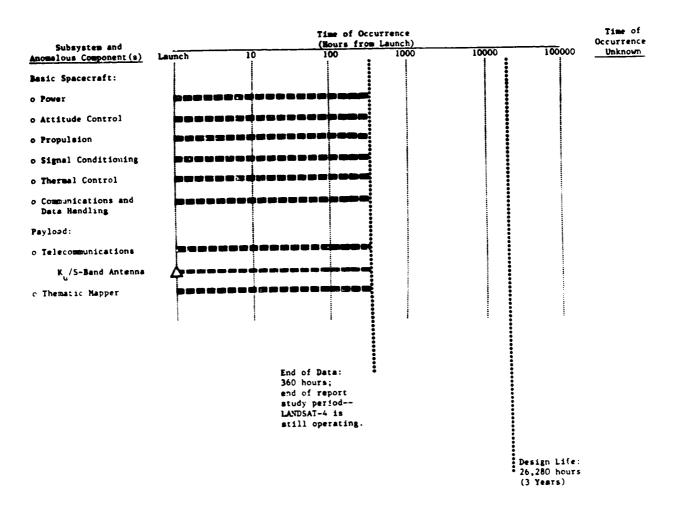
ORIGINAL PAGE 19 OF POOR QUALITY



Legend:

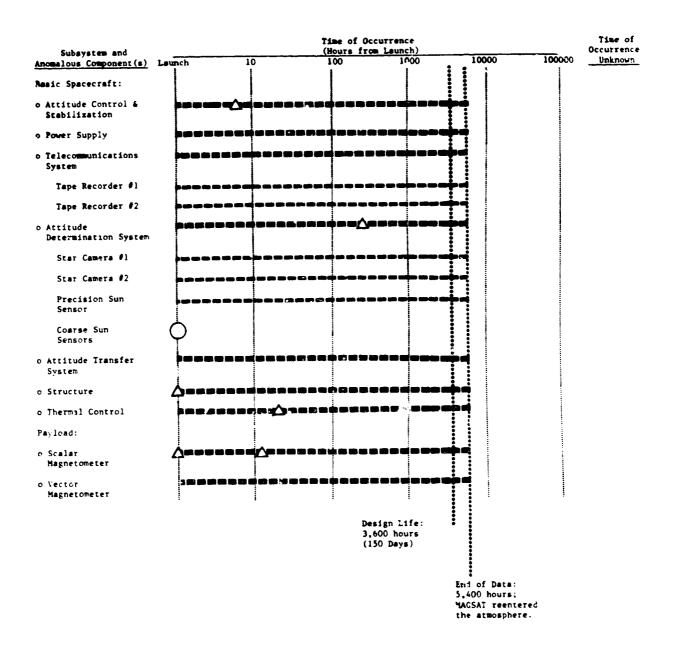
Oindicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

PERFORMANCE SUMMARY FOR LANDSAT-4



Legend:

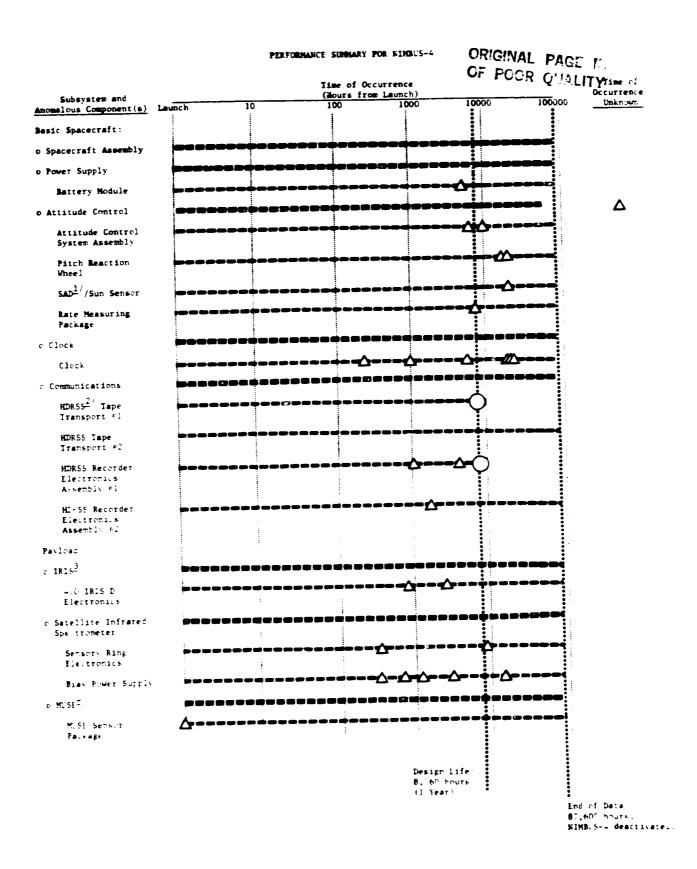
indicates that this anomaly is a failure, where failure is defines as the event that renders the subsystem and/or component unusable.



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

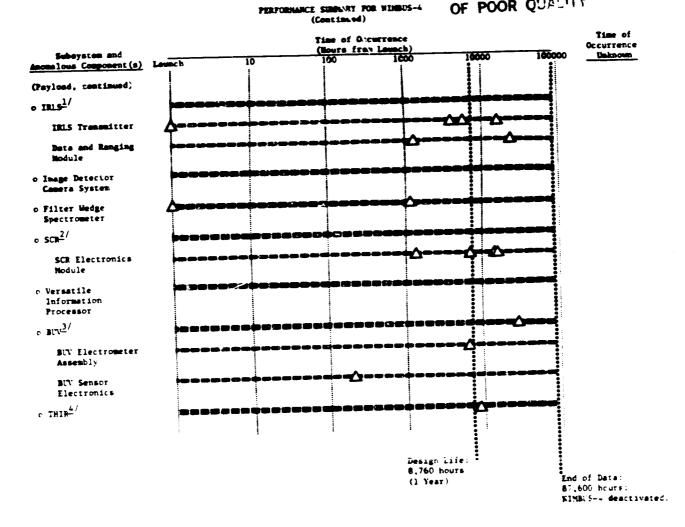
△ indicates that this anomaly is <u>rot</u> a failure



Leger.d

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsistem and is

^{1.} SAI = Sciar Array Drive.
2/ HDRSS = High Data Rate Storage System
3. IRIS = Infrared Interferometer Spectrometer
4/ HUSE = Monitor Ultraviolet Sciar Energy.



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

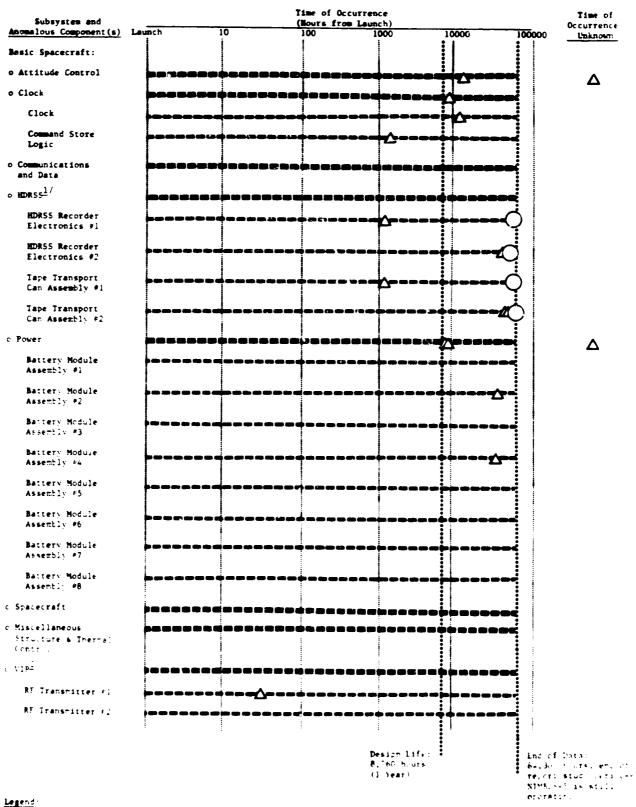
IRLS = Interrogation Recording Location System.

SCR = Selective Chopper Radiometer.

BCL = Backscatter Ultraviolet.

THIR - Temperature/Humidity Infrared Radiometer.

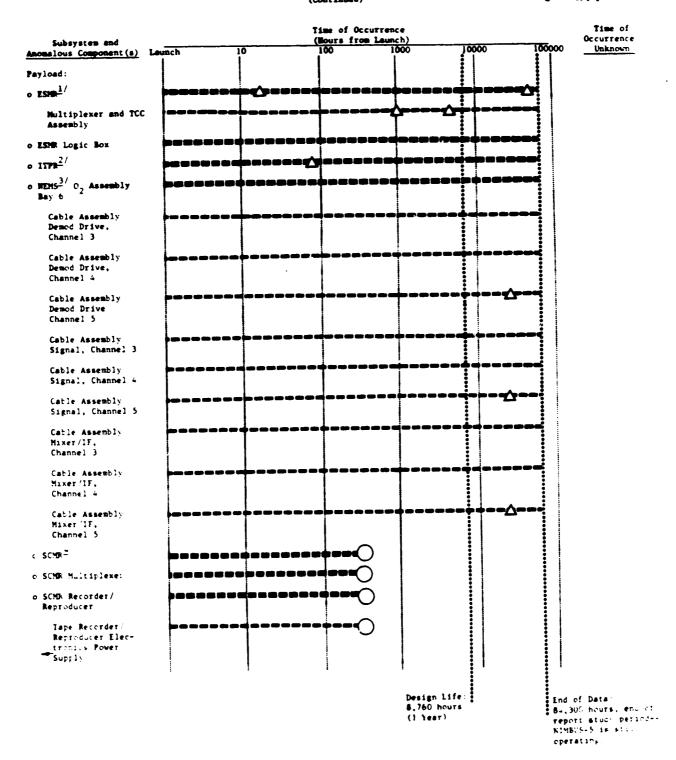
PERFORMANCE SURMARY FOR KIMBUS-5



indicates that this anomaly is a failure, where failure is defined as the event that renders the subsyster and it component unusable.

IDRSS - High Data Rate Storage System

VIP . Versatile Information Processor.



Legend

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsyster and/or component unusable.

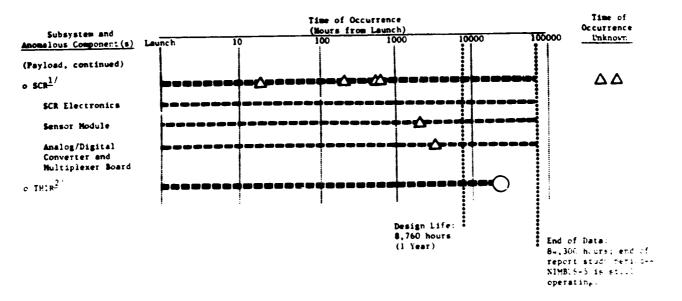
[/] ESIS - Electrically Scanned Hicrowave Radiometer

^{3/} ITPR - Infrared Temperature Profile Radiometer.

^{)/} NEMS - Nimbus-E Microwave Spectrometer

⁴ SCHR . Surface Composition Mapping Radiometer

PERFORMANCE SUPPLRY FOR HINBUS-5 (Concluded)



legeno:

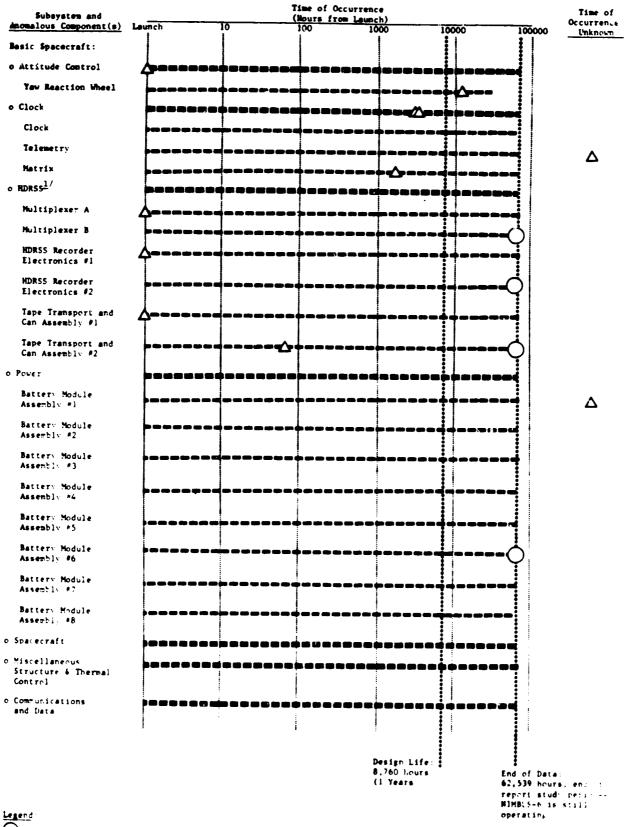
indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or

SCE - Selective Chopper Radiometer.

^{7-1 *} Temperature humidity Infrared Radiometer.

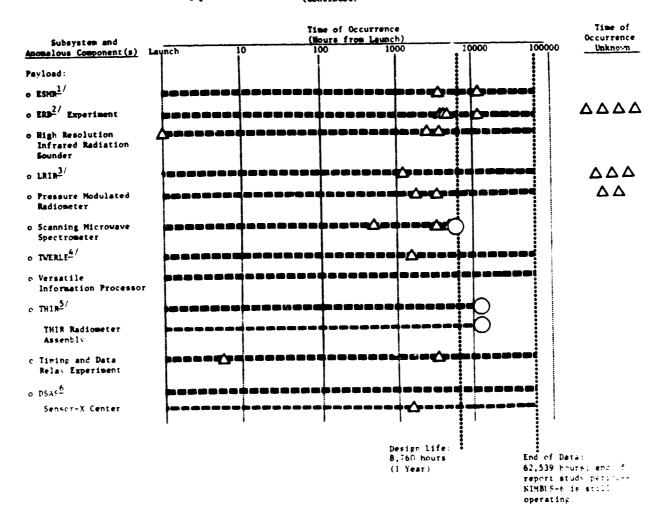
PERFORMANCE SURGARY FOR HIMBUS-6

ORIGINAL PAGE IS



indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

PERFORMANCE SUPPLARY FOR MIMBUS-6 (Continued)



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or commonent unusable.

^{1/} ESMR = Electrically Scanned Microwave Radiometer.

 $[\]overline{2}$: ERB = Earth Radiation Budget

³ LRIR - Limb Radiance Inversion Radiometer.

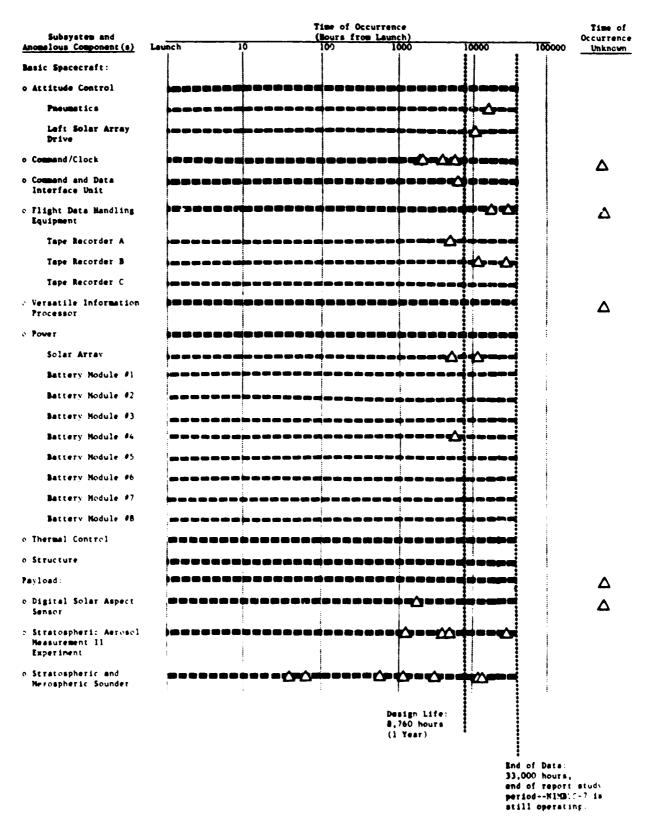
ENIN - Limb Registre inversion Radiometer.

6 TWERLE - Tropical Wind, Energy, Conservation and Reference Level Experiment.

7 THIR - Temperature/Humidity Infrared Radiometer.

6 DSAS - Digital Solar Aspect Sensor.

PERFORMANCE SURGERY FOR HIMBUS-7

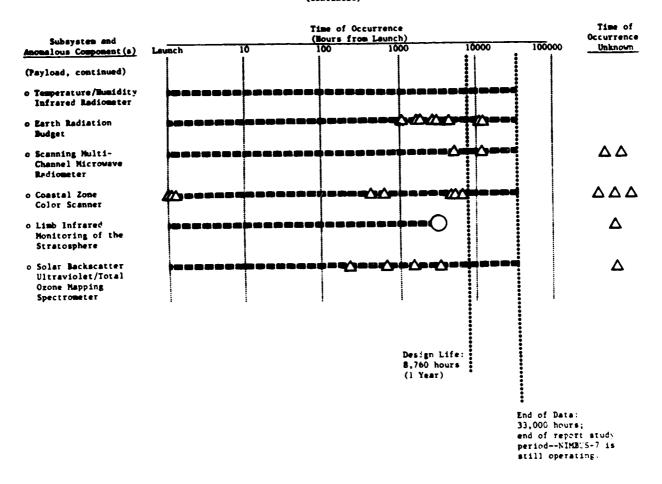


Legend

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

OPIGINAL PAGE

PERFORMANCE SURMARY FOR NIMBUS-7 (Continued)

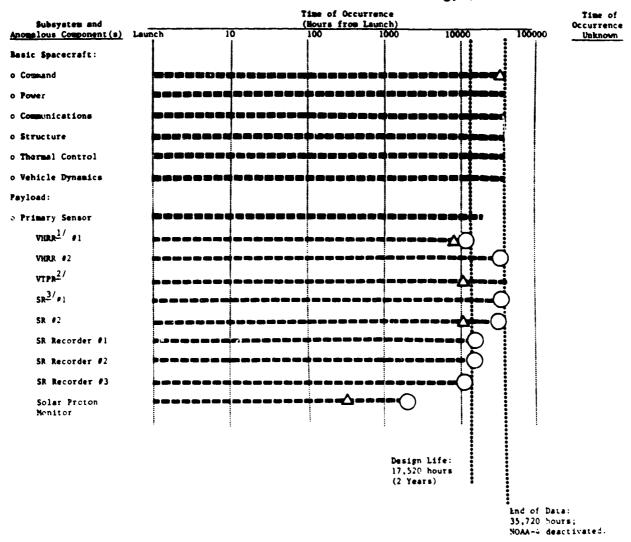


Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystement component unusable.

PERFORMANCE SUPPLARY FOR NOAA-4

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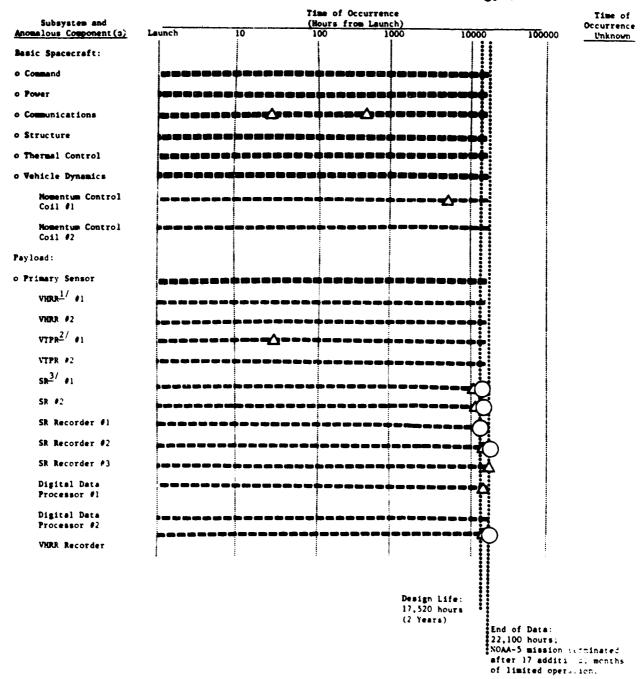


Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

^{1/} VHRR = Very High Resolution Radiometer.

[/] VTPR = Vertical Temperature Profile Radiometer. SR = Scanning Radiometer.

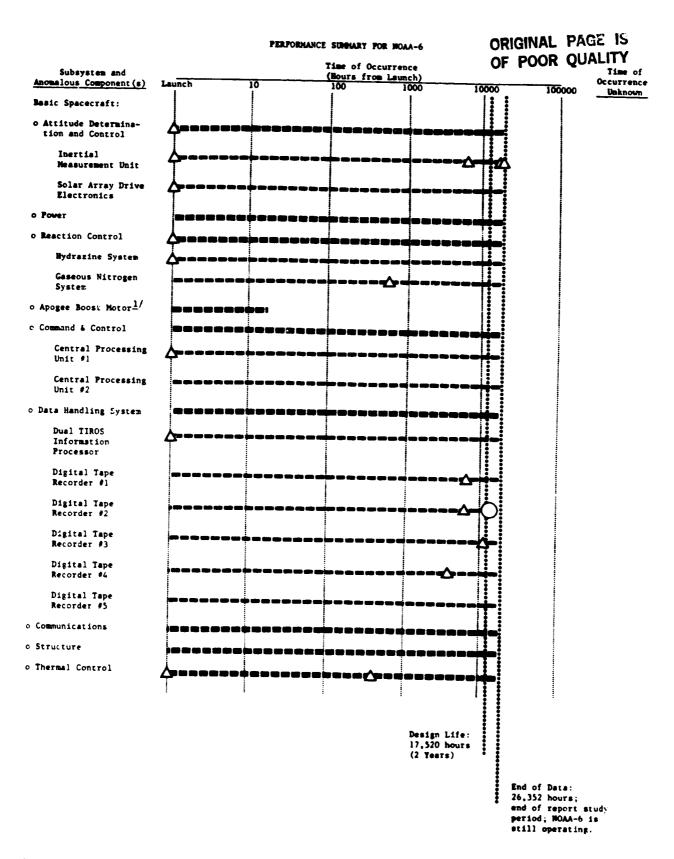


Legend:

Oindicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

\$\triangle \text{ indicates that this anomaly is not a failure.}

VMRR - Very High Resolution Radiometer. VTPR - Vertical Temperature Profile Radiometer. SR - Scanning Radiometer.



Legend:

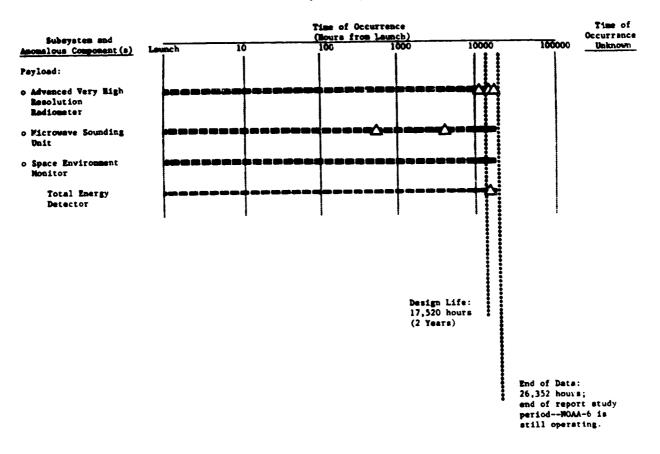
indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

\$\triangle \text{ indicates that this anomaly is not a failure.}

^{1/} The apogee boost motor is a one-shot device and has a normal lifetime of 24 hours.

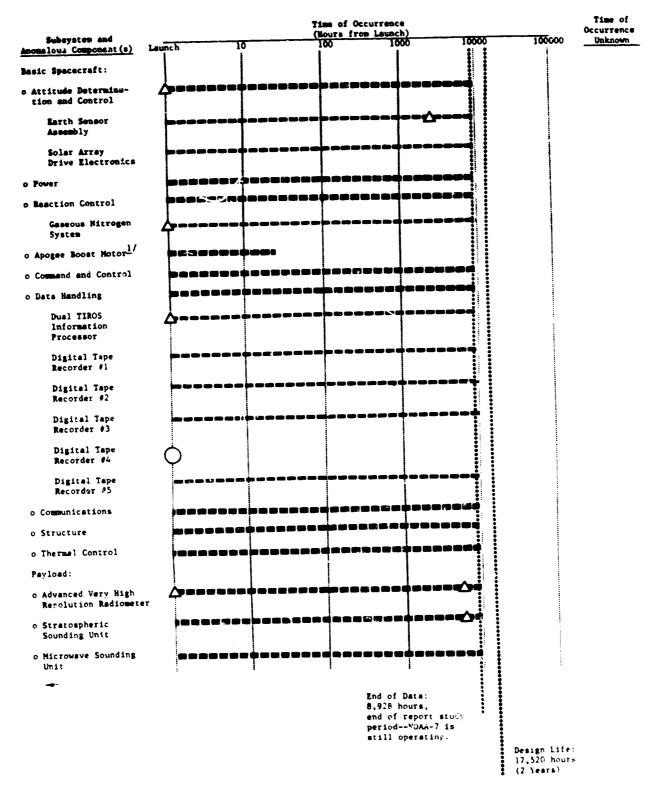
PERPORMANCE SUBMARY FOR MOAA-6 (Continued)

ORIGINAL PAGE IS OF POOR QUALITY



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

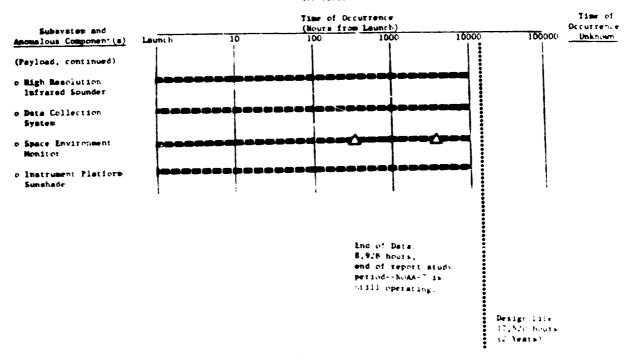


Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

¹⁷ The apogee boost notor is a one-shot device and has a normal lifetime of 24 hours.

PERFORMANCE SUBMARY FOR NOAA-" (Continued)

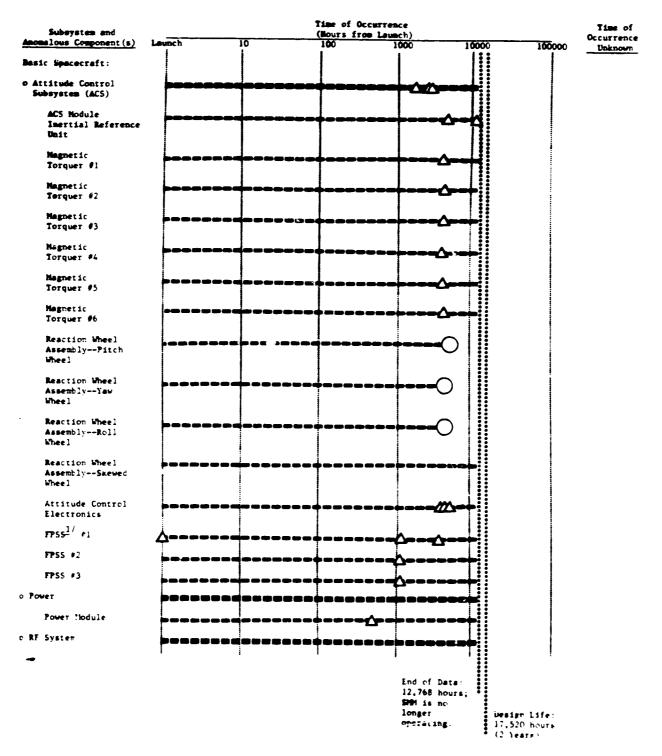


Logen!

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and it component unusable

PERFORMANCE SURBLARY FOR SAM

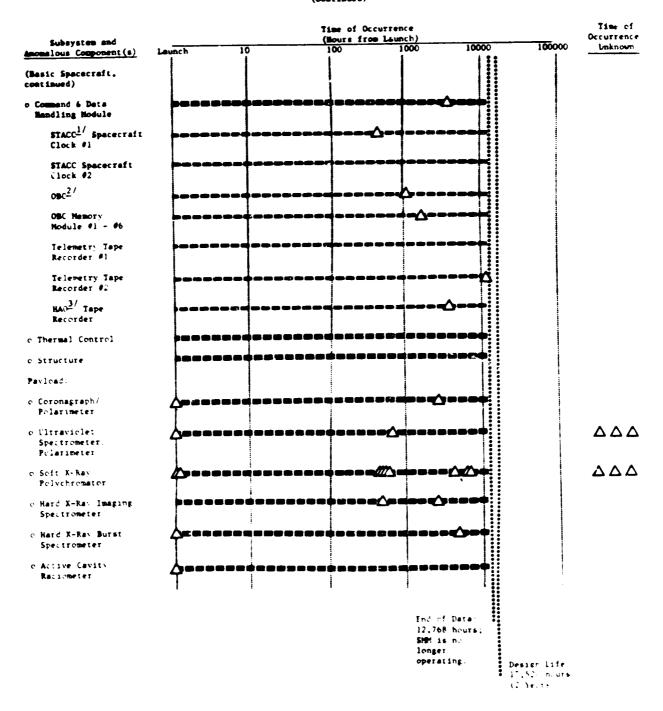
ORIGINAL PAGE 1S OF POOR QUALITY



Legend

indicates that this anumaly is a failure, where include is defined as the event that renders the subsystem and/or component unusable.

^{1/} FPSS - Fine Pointing Sun Sensors



Legend

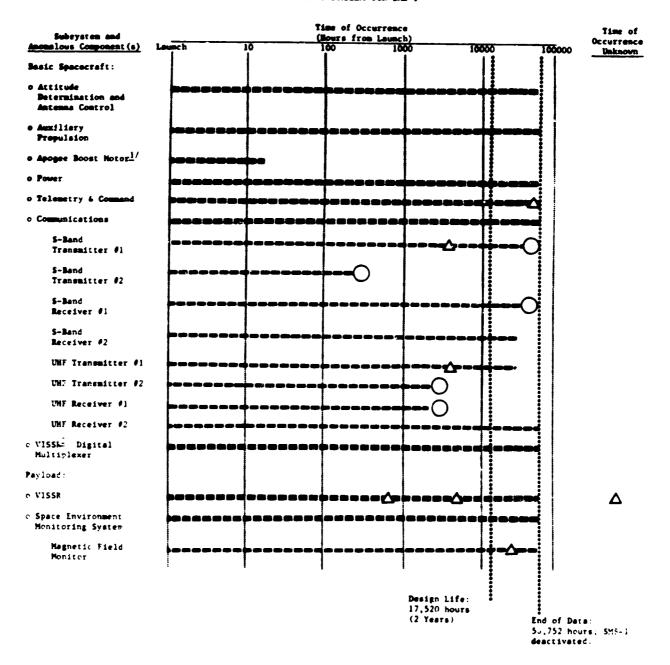
indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and it component unusable.

^{1.} STACC - Standard Telemetry and Command Components

OB(= On-Board Computer

[.] MAC - Hig' Altitude Observators

PERPORMANCE SURGARY FOR \$16-1

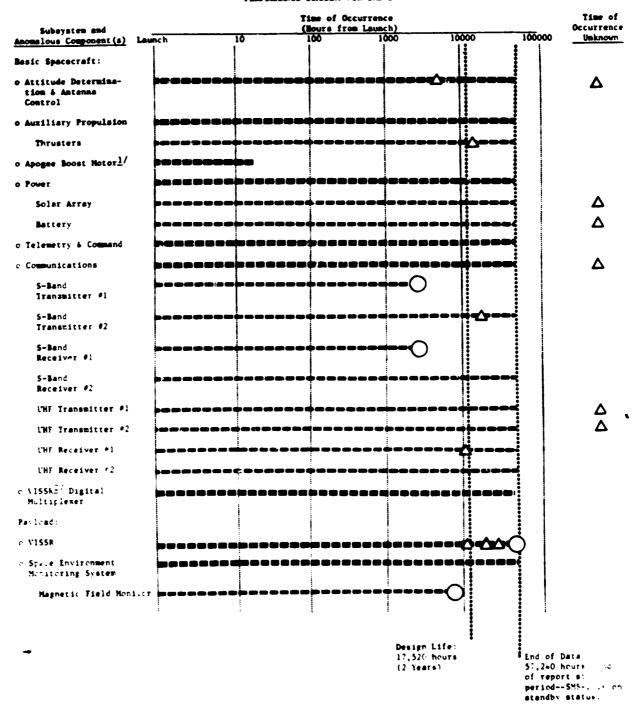


Legend

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

^{1/} The apogee boost motor is a one-shot device and has a normal lifetime of 24 hours.
2/ VISSR - Visable Infrared Spin Scan Radiometer.

PERFORMANCE SURBARY FOR SHS-2



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

^{1/} The apogre boost motor is a one-shot device and has a normal lifetime of 24 hours.

ORIGINAL PAGE IS PERFORMANCE SURBARY FOR TIROS-N OF POOR QUALITY Time of Occurrence Time of Subsystem and (Nours from Launch)
100 1000 Occurrence Anomalous Component (s) Launch 10000 100000 Unknown Basic Spacecraft: o Attitude Determination and Control Inertial

o Pover

Battery Pack 1A

Measurement Unit Earth Sensor Assembly Reaction Wheel Assembly--Yaw Reaction Wheel

Battery Pack 1B

Battery Pack 2A

Battery Pack 2B

Mattery Charge Assembly

o Reaction Control

Hydrazine System

Thrusters

o Command and Control

Central Processing Unit #1

Central Processing

Unit #2

o Data Handling

Digital Tape Recorder #1

Digital Tape Recorder #2

Digital Tape Recorder #3

Digital Tape

Digital Tape Recorder #5

o Apogee Boost Motor-1/

Design Life: 17,520 hours (2 Years) End of Data:

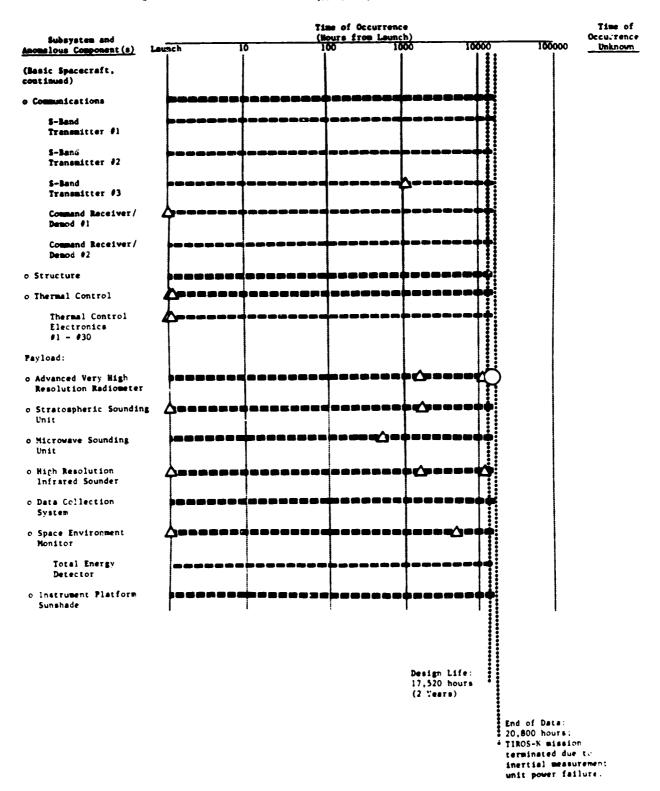
End of Data: 20,800 hours; TIROS-N mission terminated due to inertial measurement unit power failure.

Legend

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

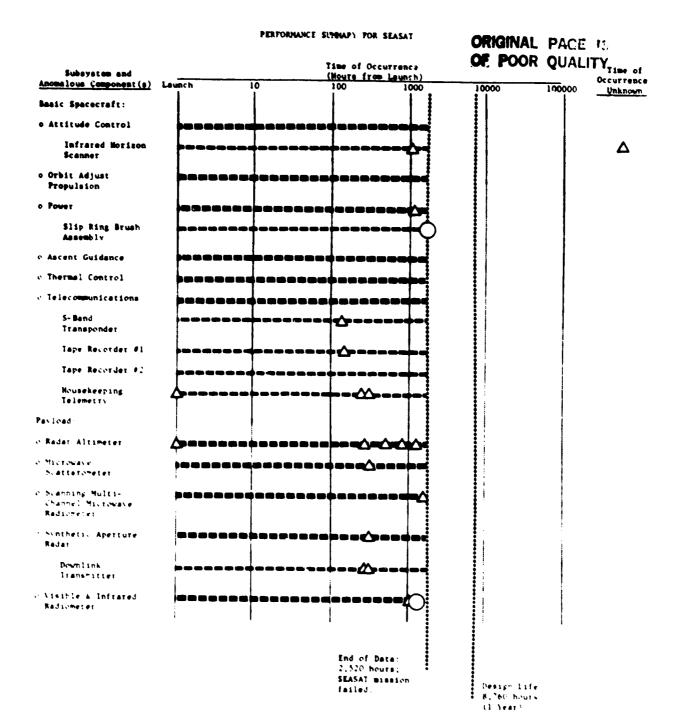
^{1/} The apogee boost motor is a one-anot device and has a normal lifetime of 24 hours

PERFORMANCE SURBARY FOR TIBOS-V (Continued)



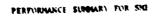
Legend:

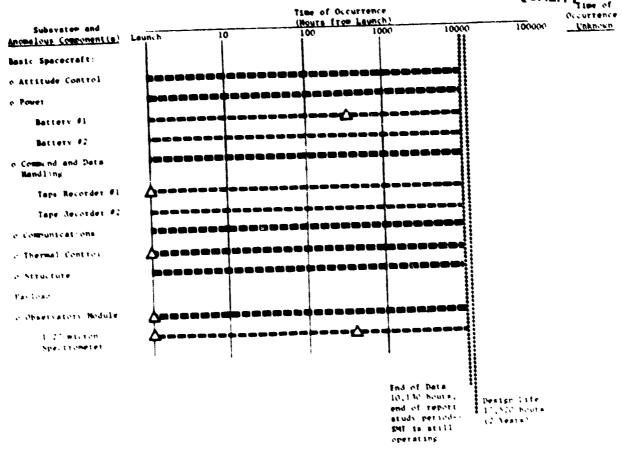
indicates that this anomaly is a failure, where failure is defined as the event that renders the subsyster and or component unusable.



Legend

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable

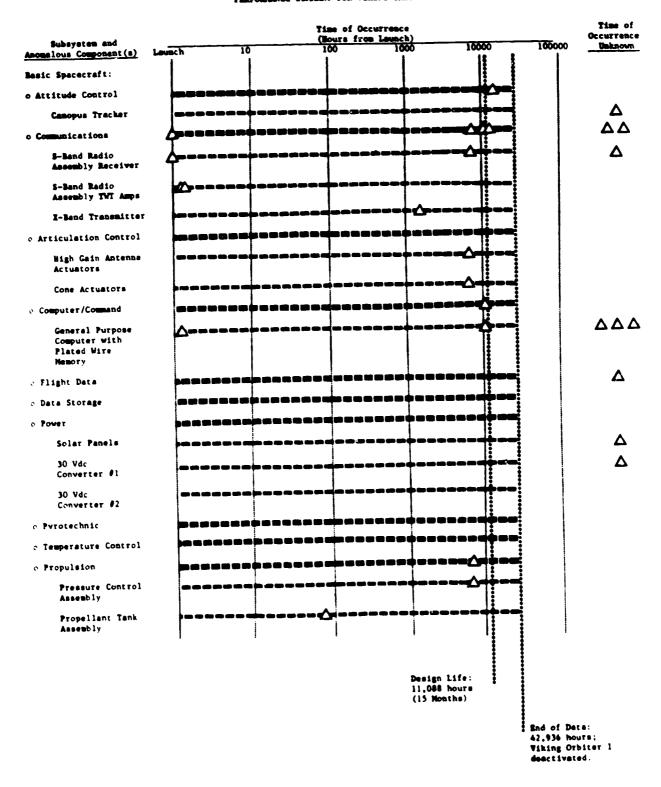




Legeni

Indicates that this animals is a failure, where failure is defined as the event that tenders the autorates and or in prosent unueab .

PERFORMANCE SURGARY FOR VIKING ORBITER 1

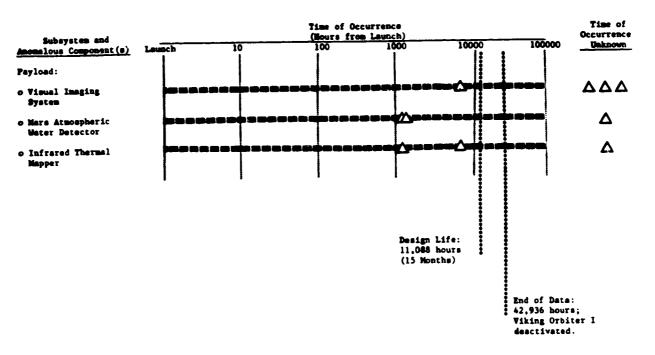


Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

PERFORMANCE SUMMARY FOR VIKING ORBITER 1
(Continued)

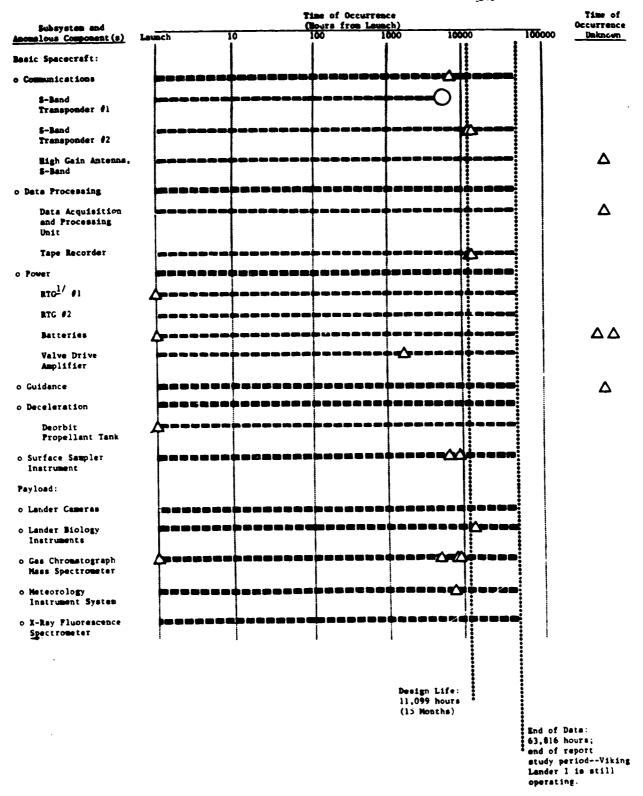
ORIGINAL PAGE IS OF POOR QUALITY



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

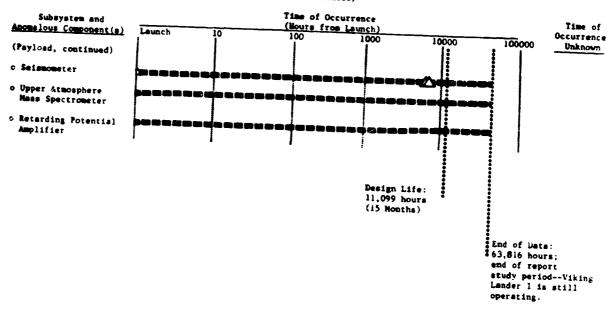




Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

PERFORMANCE SUMMARY FOR VIKING LANDER 1 (Continued)

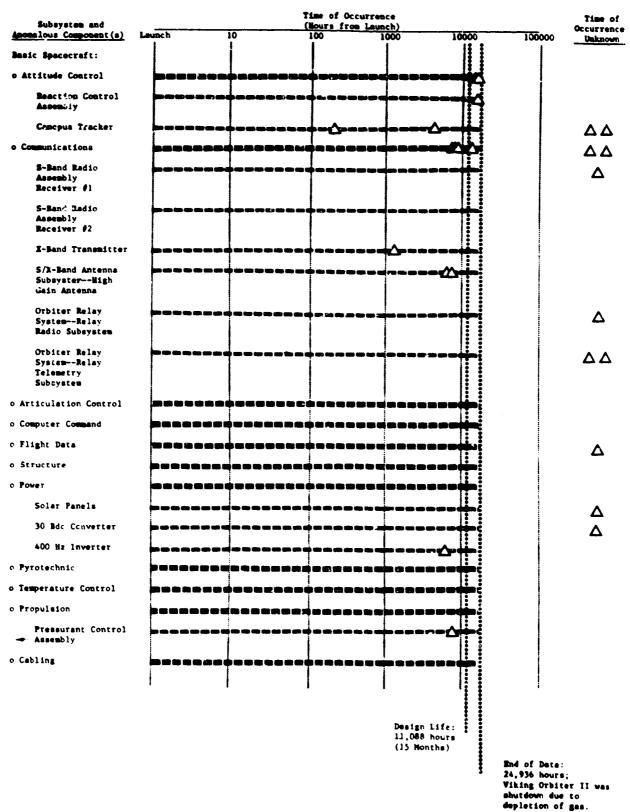


Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or

 Δ indicates that this anomaly is <u>not</u> a failure.

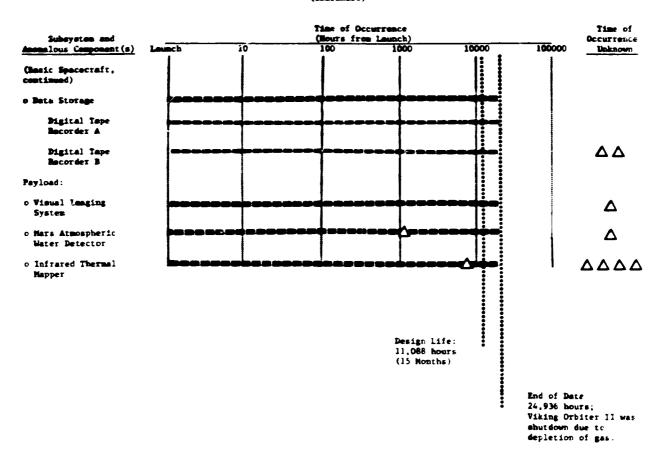
PERFORMANCE SUBMARY FOR VIRING ORBITER 2



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

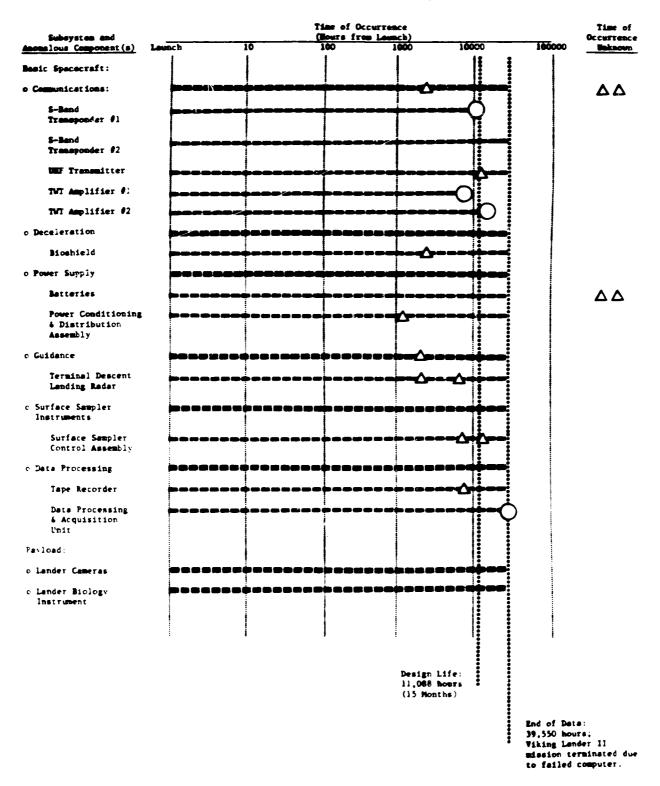
PERFORMANCE STREAMY FOR VIETNS GREITER 2 (Continued)



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and or component unusable.

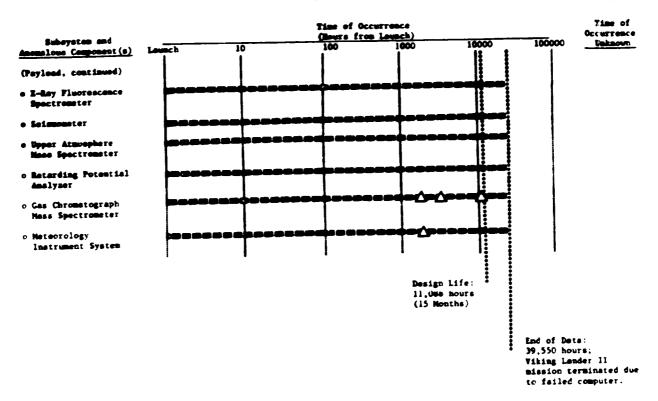
PERFORMANCE SIMBURY FOR VIKING LANDER 2



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the aubsystem and/or component unusable.

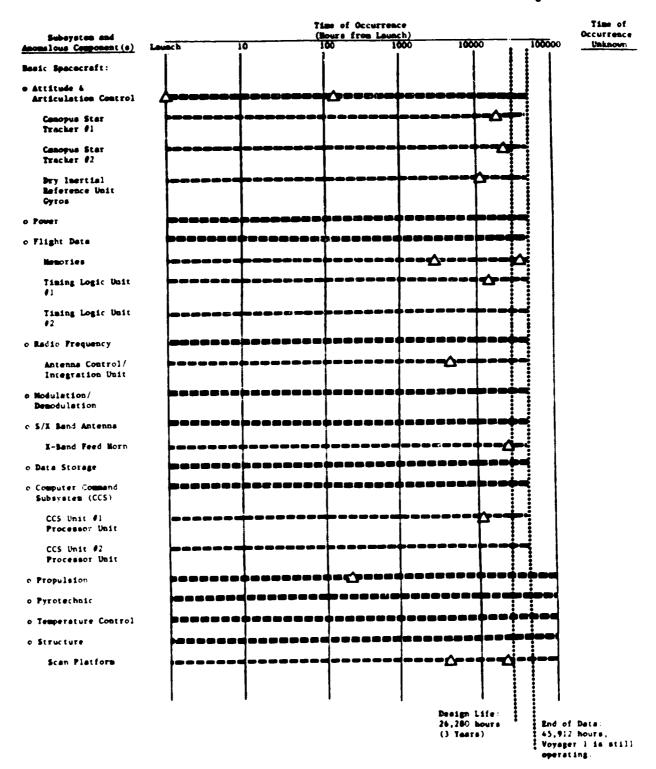
PERFORMANCE SIRBMARY FOR VIRING LANDER 2 (Continued) OF SOOR QUALITY



Legend:

Oindicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

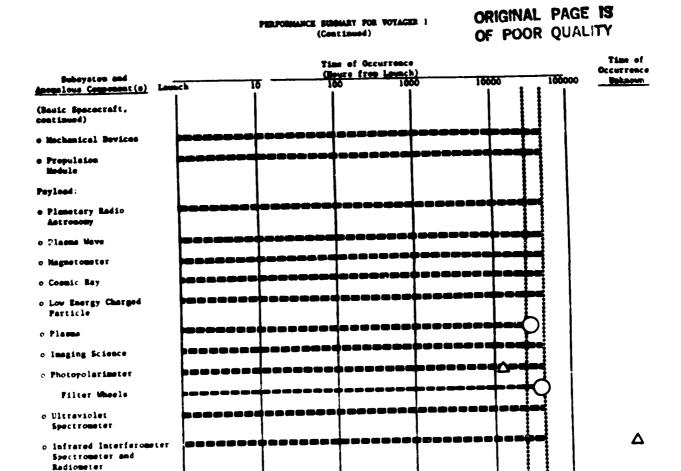
ORIGINAL PAGE IS OF POOR QUALITY



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

A indicates that this anomaly is not a failure.



Legend

Oindicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/o: component ususable.

Design Life: 26,280 hours

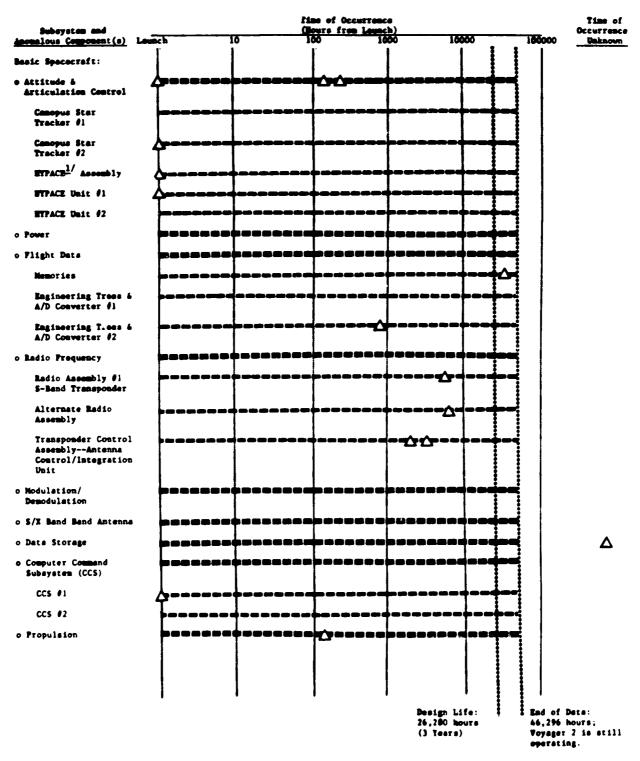
(3 Years)

End of Data: 45,912 hours;

Voyager 1 is still operating.

A indicates that this anomaly is not a failure

ORIGINAL PAGE IS PERFORMANCE SUBMANY FOR VOYAGER 2 OF POOR QUALITY



Legend:

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

A indicates that this anomaly is not a failure.

1/ MYPACE - Mybrid Programmable Attitude Control Electronics.

ORIGINAL PAGE IS OF POOR QUALITY Time of Time of Occurrence (Nours from Launch) Subsystem and Occurrence 10000 100000 Leunch Amomalous Component(s) Unknown (Basic Spacecraft, continued) o Pyrotechnic Pyro Switching Unit #1 Pyro Switching Unit #2 o Temperature Control o Structure Scan Platform o Mechanical Devices Science Boom Deployment o Propulsion Module Payload: o Planetary Radio ASTTORONY o Plasma Wave o Magnetoneter o Cosmic Ray Electronics Package o Low Energy Charged Particle Electronics Package o Plasma o Imaging Science o Photopolarimeter Electronics o Ultraviolet Spectrometer o Infrared Interferometer Spectrometer and Radiometer Design Life: End of Data: Design Life: 3 26,280 hours 46,296 hours Voyager 2 is still (3 Years) operating.

PERFORMANCE SUBMARY FOR VOYAGER 2 (Continued)

Legend: indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

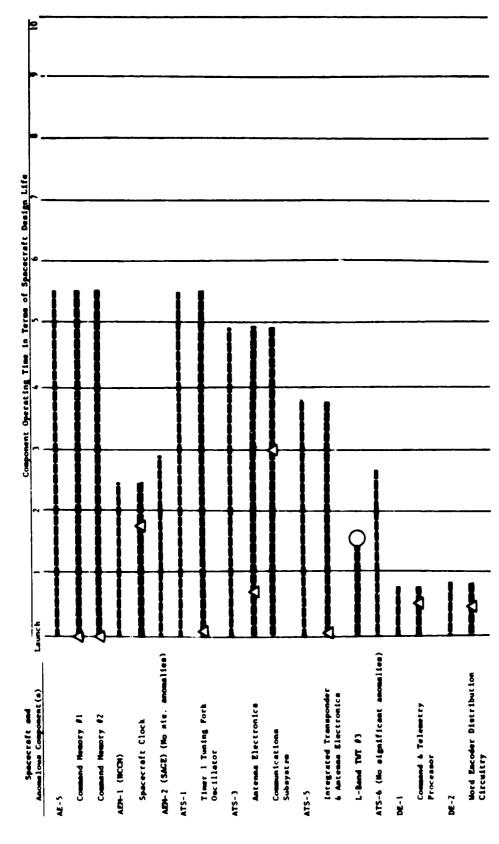
A indicates that this anomaly is not a failure.

APPENDIX C-2

SUBSYSTEMS

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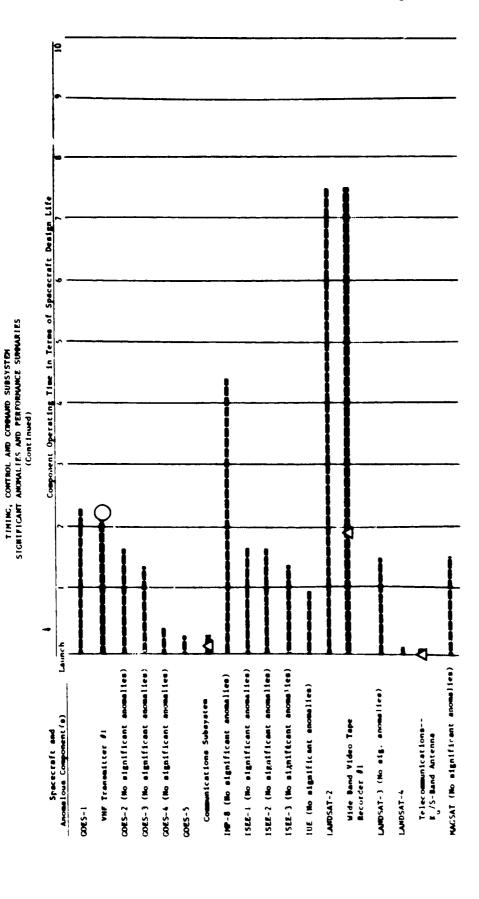
TIMING, CONTROL, AND COMMAND SUBSYSTEM SIGNIFICANT ANIMALIES AND PERFORMANCE SUMMALIES



O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. A indicates a significant anomaly that is not a failure.

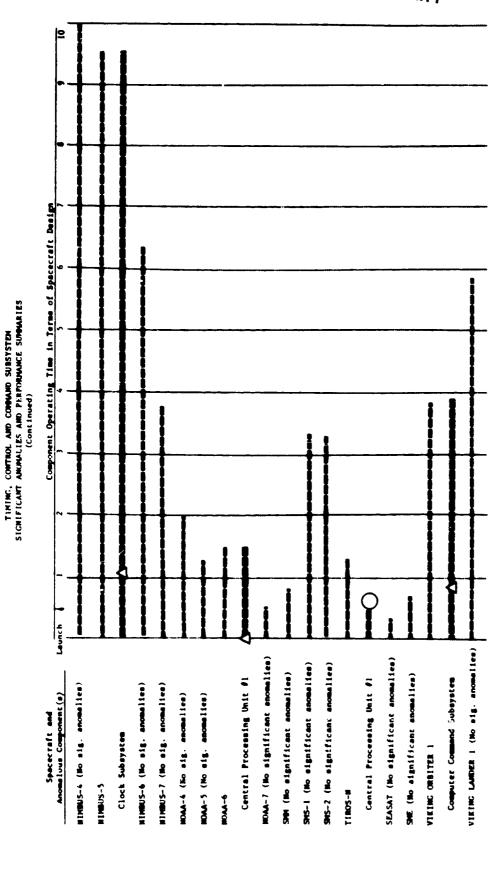
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O indicates that this anymaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. |regend:

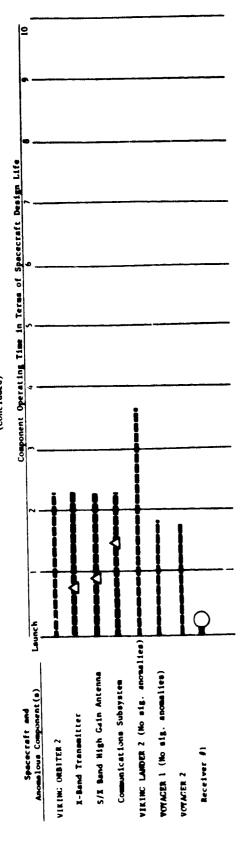
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O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. Δ indicates a significant anomaly that is not a failure.

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TIMING, COMTROL AND COMMAND SUBSYSTEM SIGNIFICANT ANOMALIES AND PERFORMANCE SUMMARIES (Concluded)

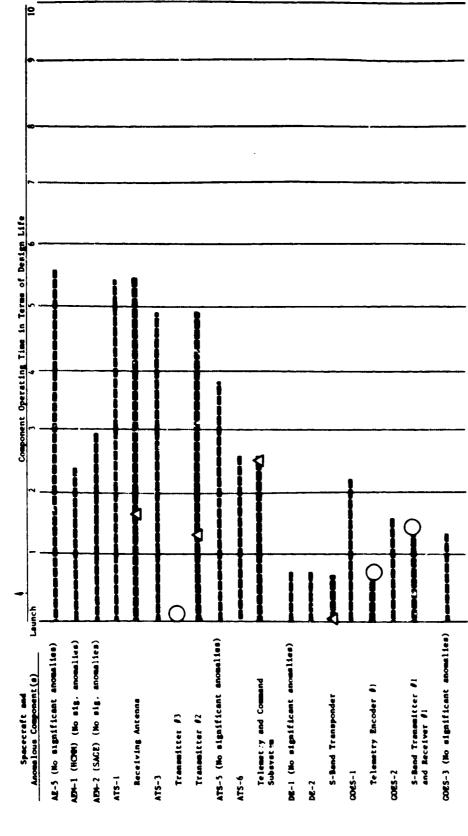


O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. regend:

A indicates a significant anomaly that is not a failure.

266

ORIGINAL PAGE IS OF POOR QUALITY

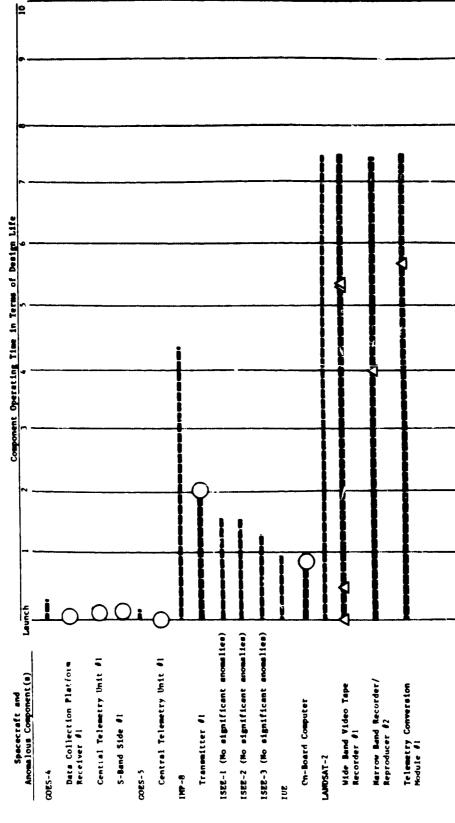


TELEMETRY AND DATA MANDLING SUBSYSTEM SIGNIFICANT ANOMALIES AND PERFORMANCE SIMMARIES

indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. Δ indicates a significant anomaly that is not a failure.

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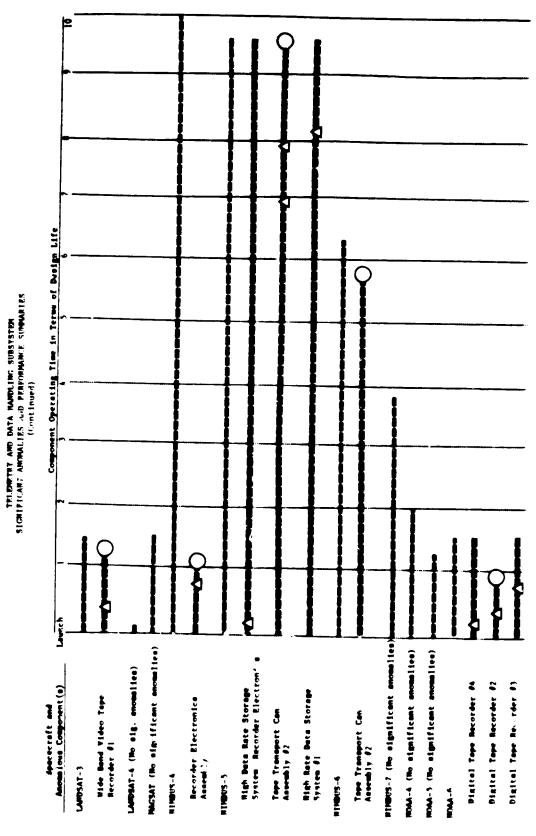
TELEMETRY AND DATA HANDLING SUBSYSTEM SIGNIFICANT ANOMALIES AND PERFORANGE SIMPLARIES (Continued)



Legend:

Oindicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

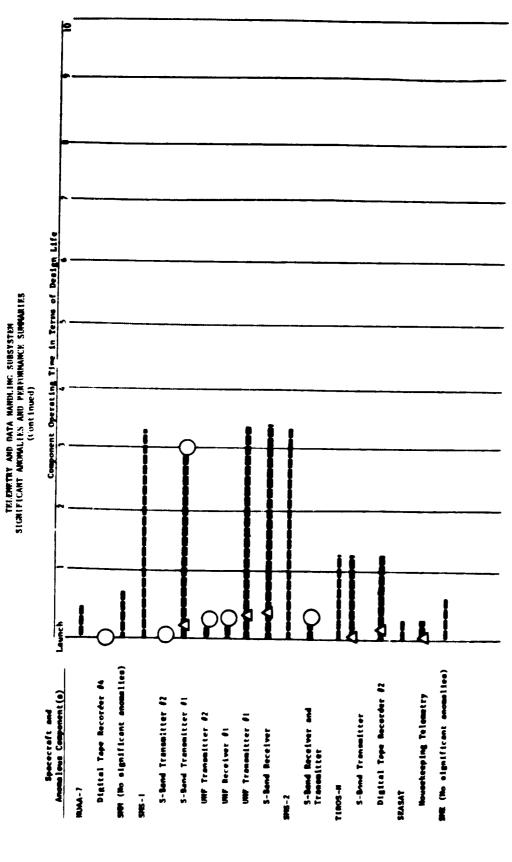
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O indicates that this annualy is a failace, where it defined as the event that renders the subsystem and/or component unusable.

 Δ indicates a significant annually that is not a failure.

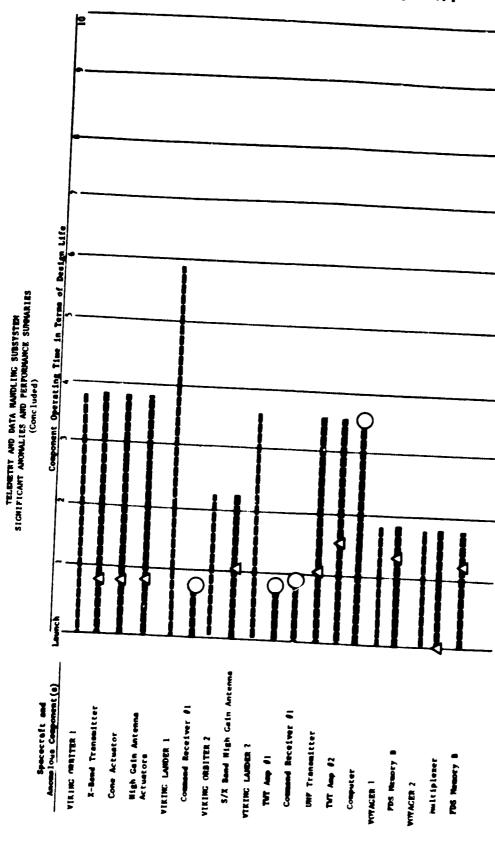
ORIGINAL PAGE IS OF POOR QUALITY



Legend:

Indicates that this enomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

ORIGINAL PAGE 18 OF POOR QUALITY

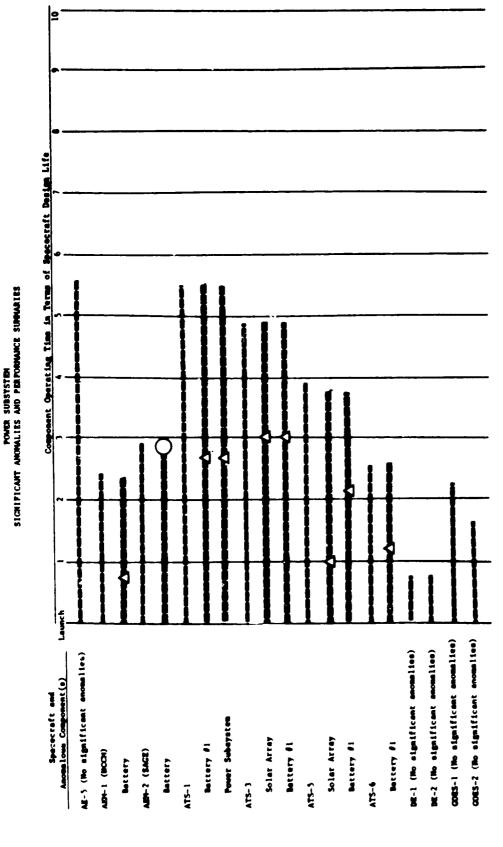


Legend:

O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

A indicates a significant anomaly that is not a failure.

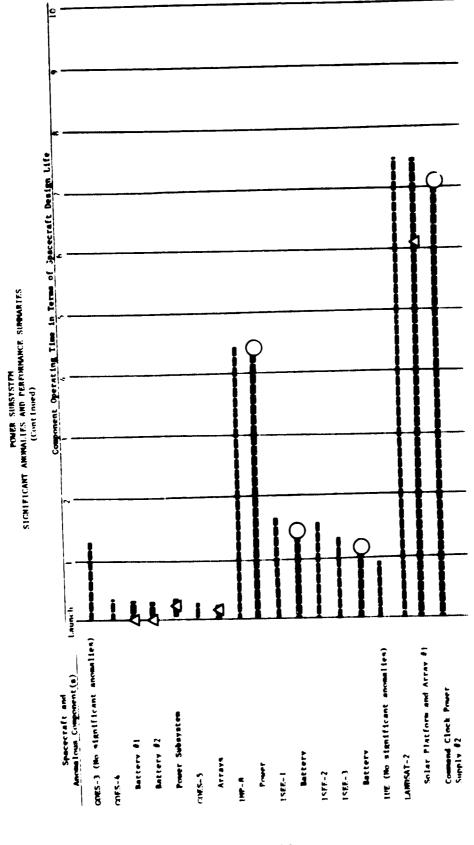
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Oledicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unuable.

A indicates a significant anomaly that is not a failure.

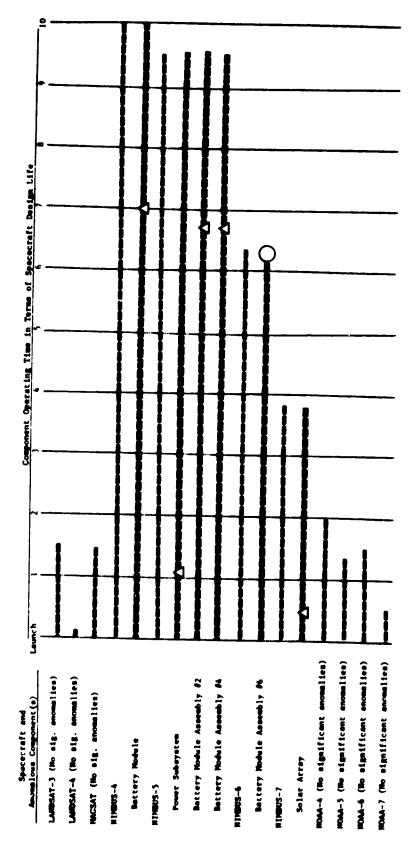
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O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. Legend:

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OF POOR QUALITY

PTHER SUBSYSTEM
SIGNIFICANT ANOMALIES AND PERFONDANCE SUBSARIES
(Continued)



7

O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

 Δ indicates a significant annually that is not a failure.

Component Operating Time in Terms of Spacecraft Design Life POWER SUBSYSTEM
SIGNIFICANT ANGMALIES AND PERFORMANCE SUBMARIES
(Concluded) VIRING ORBITER ! (No sig. enomalies) VIKING LAMBER 1 (No eig. enomalies) VIKING ORBITER 2 (No sig. enomalies) SMS-2 (No significant anomalies) SMS-i (No significant anomalies) SMM (No aignificant anomalies) SWE (No significant enomalies) Slip Ring Brush Assembly Specerraft and Anomalous Component(s) Power Conditioning and Distribution Assembly Battery Pack 2A VIETUE LABOR 2

TIROS-N

SEASAT

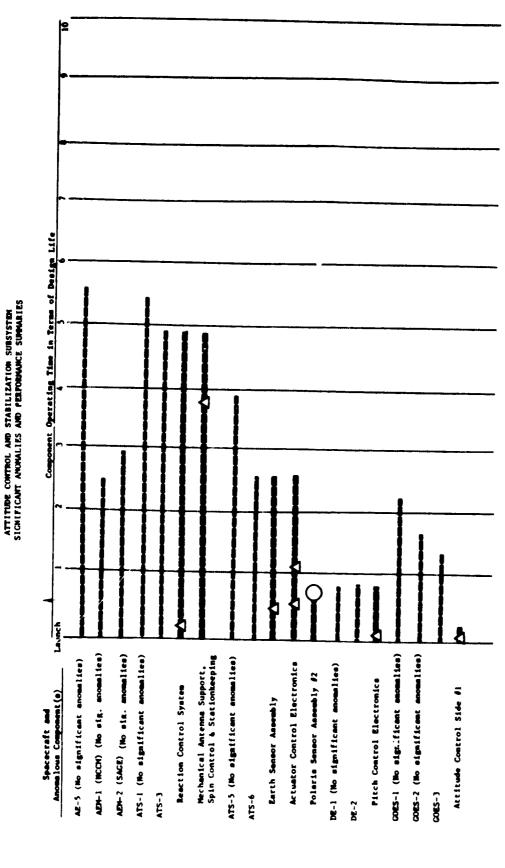
O indicates that that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. Δ indicates a significant anomaly that is not a failure. Legend:

WWAGER 1 (No eig. esceniies)

Pyro Amps 1

VOTACER 2

ORIGINAL PAGE 18 OF POOR QUALITY

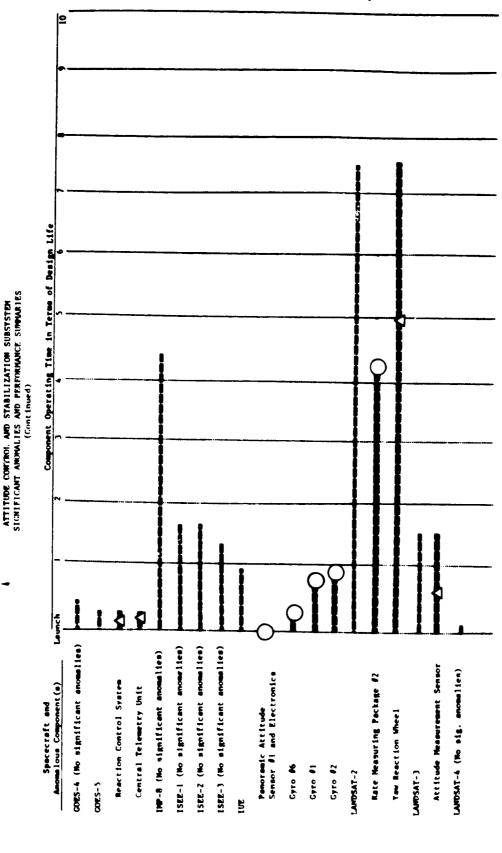


O indicates that this anomaly is a failure, where failure is defined as the ewent that renders the subsystem and/or component umusable.

 Δ indicates a significant anomaly that is not a failure.

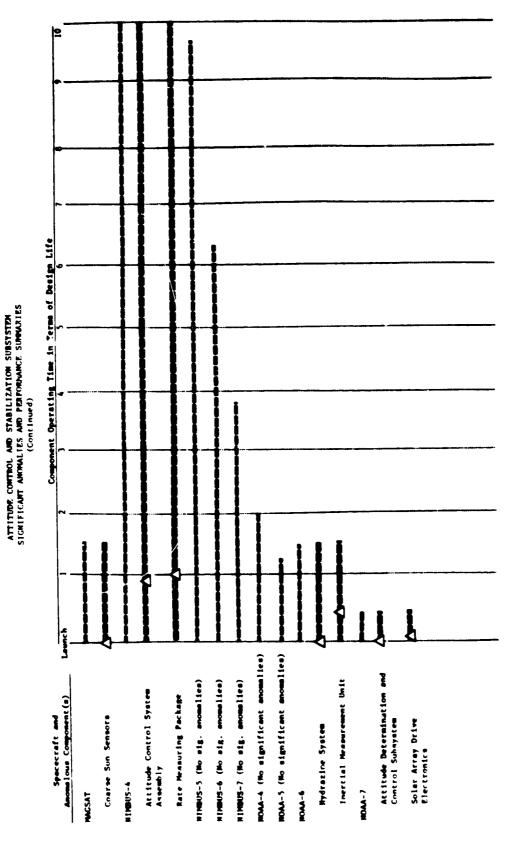
Legend:

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O indicates that this snowely is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

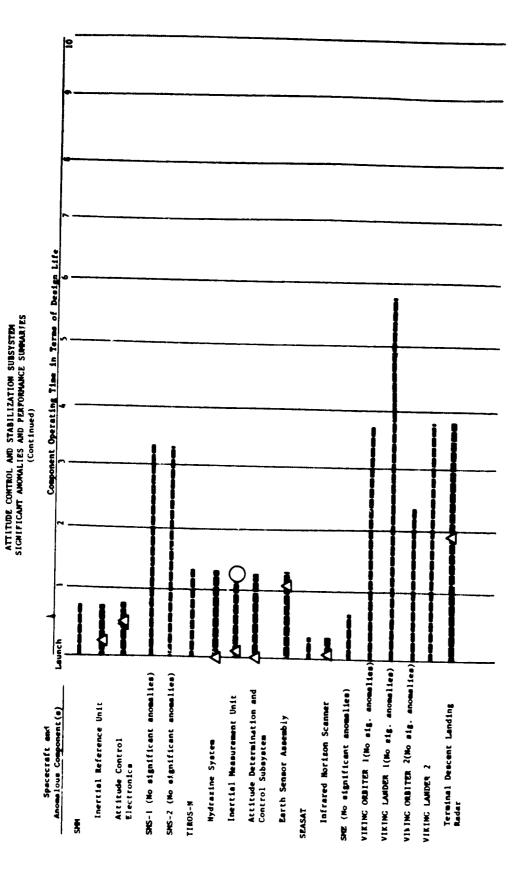
ORIGINAL PAGE 19
OF POOR QUALITY



O indicates that this anomaly is a failure, where failure is defined as the event that renders the aubsystem and/or component unusable. [egend:

ORIGINAL PAGE TO OF POOR QUALITY

15.5



O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. Δ indicates a significant anomaly that is not a failure.

Legend:

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ATTITUDE CONTROL AND STABILIZATION SUBSTSTEM SIGNIFICANT ANOMALIES AND PERFORMANCE SUBMALIES (Concluded)

			Compone	nt Operating	Component Operating Time in Terms of Dealen Life	we of Design	Life			
③	Launch		~	-					2	<u>-</u>
VOTACER 1		i								
Star Tracker #1	\$	i							_	
Star Tracker #2		j						 		
WOTAGER 2 (No sig. anomalies)										

O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

Particular of the second second second

Legend:

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Component Operating Time in Terms of Design Life PROPULSION SUBSYSTEM
ANOMALIES AND PERFORMANCE SUBMARIES Leunch Deorbit Propellant Tank Apogee Boost Motor and Ejection Mechanism Propulsion Electronics Spacecraft $\frac{1}{4}$ and Anomalous Component(s) Spacecraft Propulaton System #1 Pressurant Control Assembly VIKINC ORBITER 1 VIKING LANDER!

2

Legend:

Indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. Δ indicates a significant anomaly that is not a failure.

1/ Only spacecraft with significant anomalies reported in the propulation subsystem are listed.

Thrusters

WY AGER 1

Thrusters

VOYACER 2

Thrusters

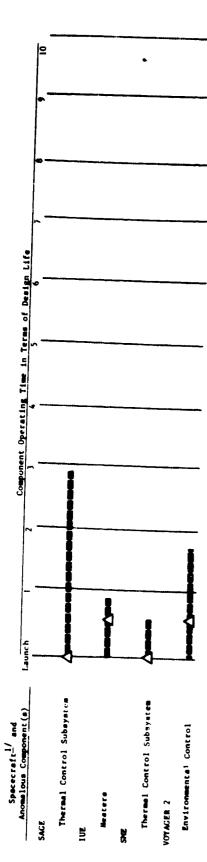
SMS-2

4- S300

ATS-6

ISEE-3

ENVIRONMENTAL CONTROL SUBSYSTEM AMMALIES AND PERFORMANCE SUPERRIES

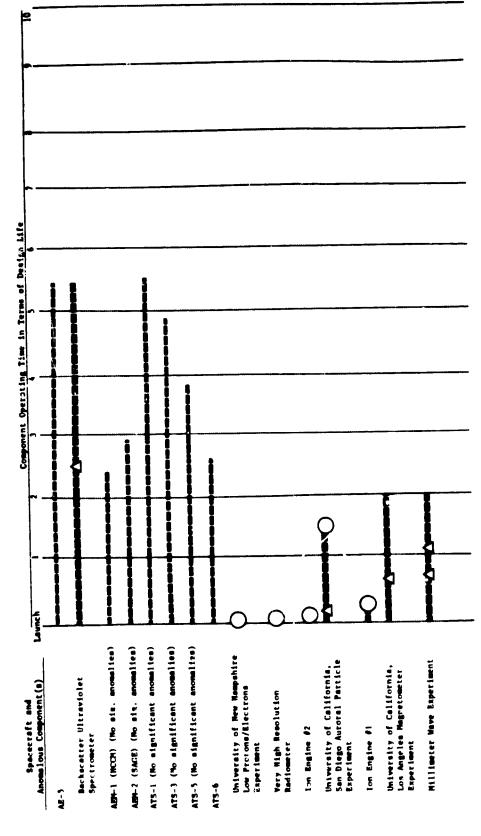


O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. Δ indicates a significant anomaly that is not a failure.

Legend:

1/ Only spacecraft with eignificant anomalies reported in the environmental control subsystem are listed.

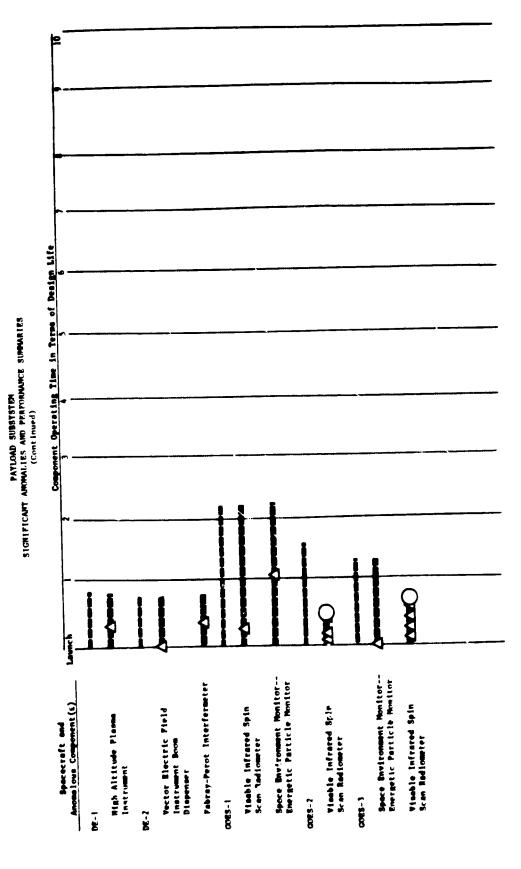
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PATLOAD SUBSTSTEM SIGNIFICANT ANDMALIES AND PERFONMANCE SUMMARIES

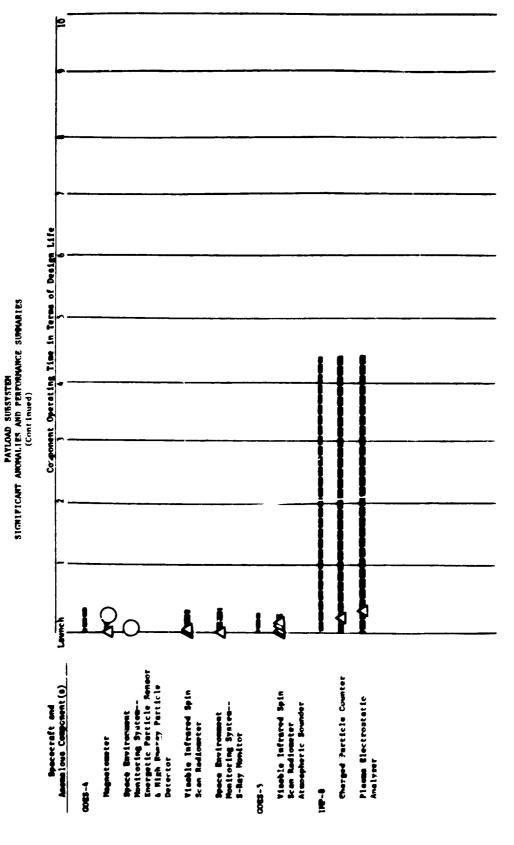
O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. regend:

ORIGINAL PAGE 13 OF POOR QUALITY



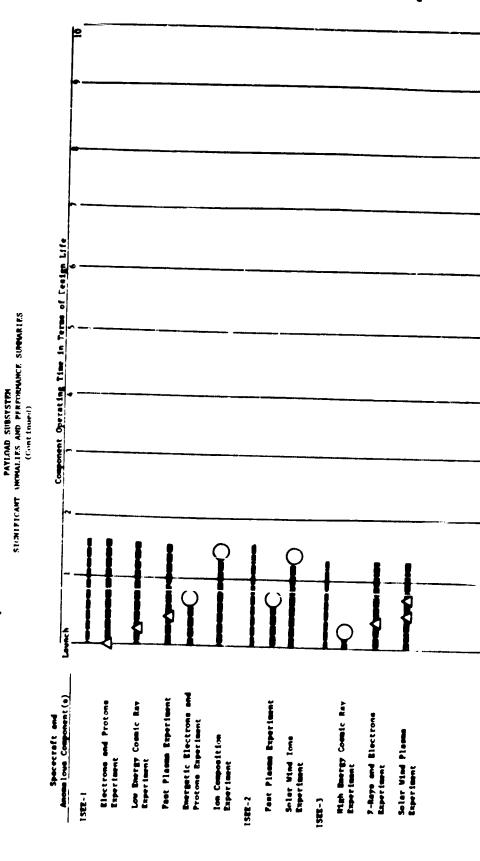
Condicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

ORIGINAL PAGE IS OF POOR QUALITY



O indicates that this anomaly is a failure, where failure is defined as the event that renders the subnyatem and/or component unusable.

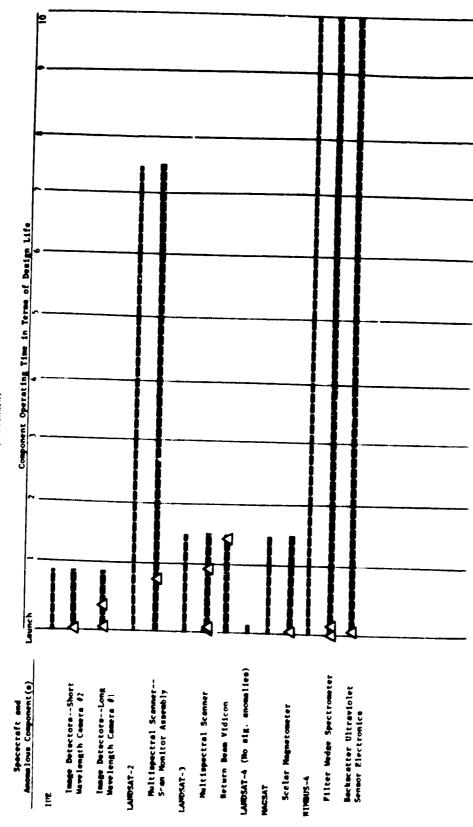
ORIGINAL PAGE 13 OF POOR QUALITY



O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

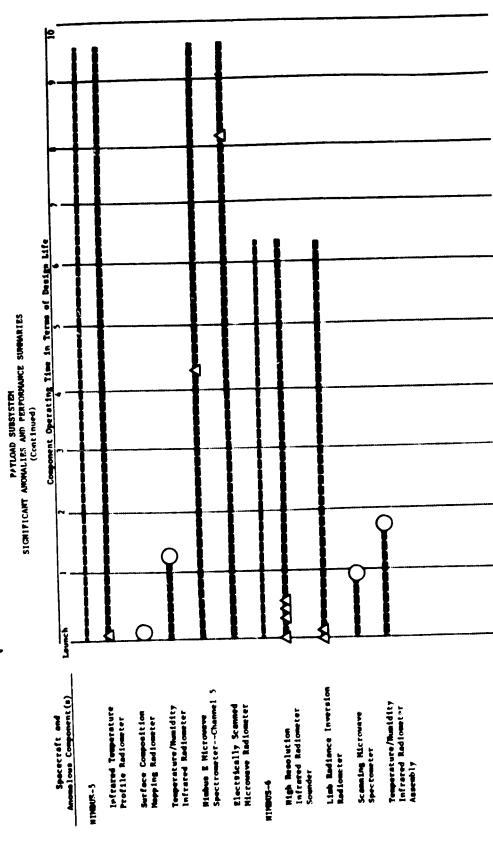
 Δ indicates a significant annually that is not a failure.

PAYLOAD SUBSYSTEN SICHIFICANT ANDMALLES AND PERFUNDANCE SUMMARLES (Continued)



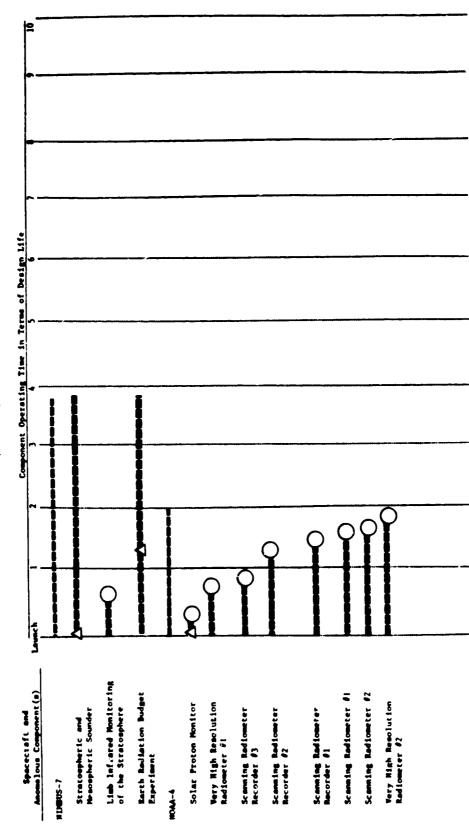
: Fellend: indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

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O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable. : |-|-

PAYLOAD SUBSYSTEM
SIGNIFICANT ANDMALLES AND PERFORMANCE SUPPLABLES
(Continued)



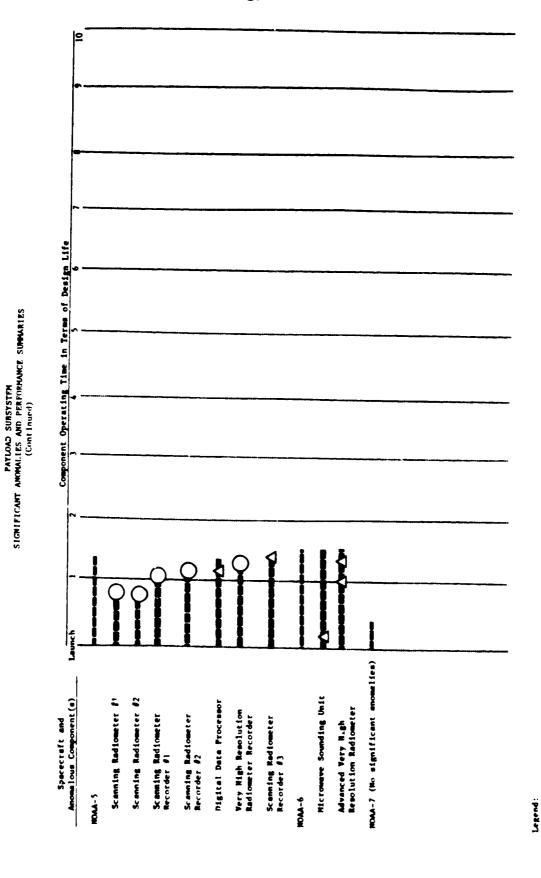
Indicates that this anomaly is a failure, where failure is defined as the event that renders the arbsystem and/or component umusable.

Legend:

A indicates a significant anomaly that is not a failure.

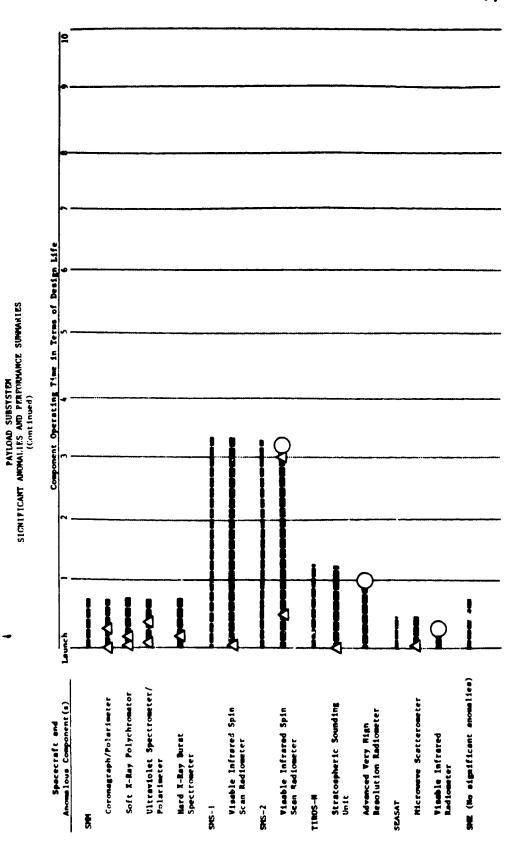
289

ORIGINAL PAGE IS OF POOR QUALITY



O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

ORIGINAL PAGE IS OF POOR QUALITY



O indicates that this anomaly is a failure, where failure is defined as the event that renders the subsystem and/or component wnusable. Δ indicates a significant anomaly that is not a failure.

Legend:

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Component Operating Time in Terms of Design Life PAYLOAD SUBSYSTEM
SICNIFICANT ANOMALIES AND PERFORMANCE SUMMARIES
(Concluded) WIKING ORBITZE 1(No sig. snomslies) Photopolarimeter Analyzer Wheel Spacecraft and Anomalous Component(s) Gas Chromatograph Mass Spectrometer Gas Chromatograph Mass Spectrometer

Mara Atmospheric Mater Detector

VIKING LANDER 2

VIKING ORBITER 1

VIKING LANDER 1

O indicates that this snowsly is a failure, where failure is defined as the event that renders the subsystem and/or component unusable.

Applications and the state of t

 Δ indicates a significant anomaly that is not a failure.

Legend:

WOTACER 2

Photopolarimeter Filter

WOYACER 1

Low Energy Charged Particle Instrument

Scan Plattorm